

BİDGE Yayınları

Advanced Functional Materials for Sustainable Flexible Pavements: Materials, Characterization and Emerging Technologies

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*To our families, colleagues, and students,
whose continuous encouragement and inspiration
have made this work possible.*

PREFACE

The rapid evolution of transportation infrastructure has significantly increased the demand for pavement materials that are not only mechanically durable but also environmentally sustainable and functionally advanced. Conventional pavement technologies are increasingly challenged by heavier traffic loads, climate change, resource depletion, and the growing need to reduce the environmental footprint associated with road construction and maintenance. These challenges have accelerated the development of innovative materials and multidisciplinary approaches aimed at enhancing the long-term performance, resilience, and sustainability of flexible pavements.

Over the past decade, remarkable progress has been achieved through the incorporation of functional materials into asphalt pavements. Nanomaterials, recycled waste products, polymeric modifiers, fibers, bio-based additives, and smart materials have demonstrated considerable potential for improving pavement performance while simultaneously supporting resource efficiency and circular economy principles. At the same time, advances in characterization techniques, performance evaluation methods, and sustainability assessment tools have provided researchers with deeper insights into the complex interactions governing pavement behavior.

This book, *Advanced Functional Materials for Sustainable Flexible Pavements*, has been prepared to provide a comprehensive

and up-to-date overview of this rapidly evolving research field. Rather than focusing on a single modifier or material, the book brings together recent developments in functional materials, pavement engineering, sustainability, and emerging technologies within a unified perspective. It aims to bridge the gap between fundamental scientific concepts and practical engineering applications while highlighting current challenges and future research opportunities.

The book is organized into eight chapters. It begins with the fundamental principles of flexible pavement engineering and introduces the concept of functional materials in pavement applications. Subsequent chapters explore advanced nanomaterials, waste valorization strategies, material characterization techniques, the thermal behaviour of functional pavements, sustainability assessment, and emerging technologies that are shaping the future of pavement engineering. Each chapter has been carefully designed to present both theoretical foundations and recent scientific advances, supported by current literature and practical engineering perspectives.

This book is intended for researchers, graduate students, practicing engineers, and professionals working in pavement engineering, transportation infrastructure, materials science, and sustainable construction. We hope it will serve as a valuable reference for both academic research and engineering practice while encouraging interdisciplinary collaboration and continuous innovation in the development of durable, intelligent, and environmentally responsible pavement systems.

We would like to express our sincere appreciation to the many researchers whose valuable scientific contributions have advanced this rapidly developing field. Their work has laid the foundation upon which this book has been built. We also extend our gratitude to our colleagues and students, whose enthusiasm,

discussions, and continuous support have inspired many of the ideas presented throughout this book.

We believe that the future of flexible pavements will be shaped not by a single material or technology, but by the successful integration of advanced functional materials, sustainable engineering practices, and intelligent infrastructure systems. As transportation networks continue to evolve, interdisciplinary collaboration and continuous innovation will become increasingly essential for developing safer, more durable, and environmentally responsible pavements.

Finally, every scientific advancement begins with curiosity, develops through dedicated research, and reaches its greatest value when transformed into practical solutions that benefit society. It is our sincere hope that this book will not only serve as a comprehensive reference for researchers and practitioners, but also inspire new ideas, encourage scientific collaboration, and contribute to the advancement of sustainable pavement engineering. The journey toward sustainable flexible pavements is far from complete, and we hope this book will become a small but meaningful part of that continuing scientific journey.

Semahat Doruk

Başak Varlı Bingöl

Çankırı, Türkiye

July 2026

HOW TO USE THIS BOOK

This book has been organized to provide both fundamental knowledge and recent developments in the field of sustainable flexible pavements.

Readers who are new to pavement engineering are encouraged to begin with Chapters 1 and 2 before exploring the advanced topics presented in the following chapters. Researchers interested in specific functional materials, characterization techniques, or sustainability assessment may directly refer to the relevant chapters according to their research interests.

Each chapter is designed as a self-contained resource while maintaining a logical progression throughout the book.

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CHAPTER 1

Flexible Pavements And Bituminous Binders: Fundamentals, Composition And Performance Requirements

Flexible pavements are among the most widely constructed civil-engineering assets on Earth, carrying the overwhelming majority of the world's paved road network and forming the physical substrate on which modern freight, commuter, and supply-chain mobility depend. Their designation as "flexible" derives not from any capacity to deform elastically in a colloquial sense but from the characteristic manner in which layered, particulate, bitumen-bound systems distribute wheel loads to the underlying soil: through a comparatively shallow load-spreading action that transmits nonuniform deflections rather than the slab-bridging behaviour of rigid concrete pavements. Understanding the behaviour of these structures, and the emerging generation of advanced functional and sustainable materials designed to improve them, requires first a firm command of the fundamentals: the architecture of the layered system, the chemistry and physical structure of the bituminous

binder that holds it together, the aggregate skeleton and volumetric proportioning that govern mechanical response, and the interlocking performance requirements and distress mechanisms that dictate service life. This chapter establishes that foundation, situating each topic within the contemporary international literature and highlighting the sustainability imperatives that motivate the material innovations examined in later chapters (Styer, Tunstall, Landis, & Grenfell, 2024).

Structure and Classification of Flexible Pavements

A flexible pavement is a multilayer engineered system in which successive courses of progressively higher-quality material are placed over a prepared soil foundation, each layer contributing structural capacity while protecting the layers beneath it from excessive stress. In the conventional description, the system comprises, from the bottom upward, the subgrade (the compacted natural or improved soil), one or more granular subbase and base courses, and the bituminous-bound surface courses that carry traffic directly. The governing structural principle is that a wheel load applied at the surface generates vertical compressive stresses that diminish with depth as the load is spread over an increasing area; the design task is to proportion the layer thicknesses and stiffnesses so that the stresses reaching each layer, and ultimately the subgrade, remain within tolerable limits over the design traffic spectrum. Because the surface asphalt concrete is typically the stiffest layer, as measured by its elastic (resilient) modulus, it contributes disproportionately to the overall load-spreading capacity and, depending on its thickness, may dominate the structural response of the section (Styer et al., 2024). Figure 1.1 illustrates this layered architecture and the way in which the vertical stress diminishes with depth as the wheel load spreads through the successive courses; Figure 1.2 situates the flexible pavement within the broader family

of flexible, rigid and composite systems; and Figure 1.3 contrasts the load-spreading and stress-bulb behaviour of flexible and rigid pavements.

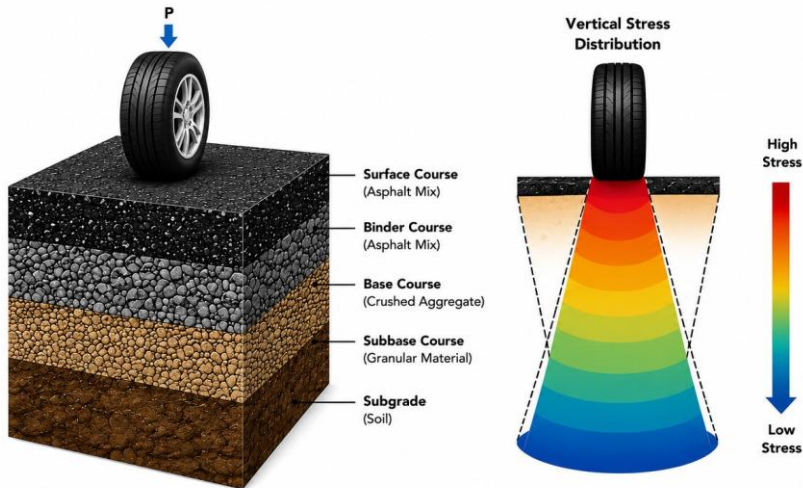


Figure 1.1. Layered structure of a flexible pavement and the vertical stress distribution beneath a wheel load, showing how each course spreads the load so that stress diminishes with depth toward the subgrade.

The broad classification of bound pavements distinguishes three primary families, flexible (asphalt-surfaced), rigid (Portland cement concrete), and composite (combinations of the two), and the essential contrast between the first two lies in the load-transfer mechanism. Rigid pavements possess sufficient flexural rigidity to act as beams or slabs that bridge localized weaknesses in the foundation and distribute loads over a wide area through bending. Flexible pavements, by contrast, lack this slab action; they transmit load through the aggregate interlock and the viscoelastic bituminous matrix, so that the intensity of stress transmitted to the subgrade

depends strongly on the cumulative thickness and stiffness of the overlying bound and unbound layers. This distinction has profound consequences for design philosophy, distress modes, and the way in which material improvements propagate through the structure. Contemporary structural analysis increasingly relies on multiscale numerical simulation, coupling molecular, mesoscale, and full-scale finite-element representations, to predict how layer response and material properties interact under moving wheel loads, reflecting a broader shift from purely empirical toward mechanistic-empirical design frameworks (Wang & Wang, 2024).

Within the flexible-pavement family, several structural configurations are recognized according to how the bound layer thickness is deployed. Conventional multilayer sections use a relatively thin asphalt surface over substantial granular base and subbase courses, relying on the unbound aggregate to provide much of the load-spreading capacity. Full-depth and deep-strength asphalt sections, by contrast, place thick bituminous layers directly on the subgrade or over a thin granular working platform, concentrating structural capacity in the bound material and reducing sensitivity to moisture-induced weakening of granular layers. Perpetual (long-life) pavements represent a further evolution of this concept: they are designed so that the critical tensile strains at the bottom of the asphalt and the compressive strains at the top of the subgrade remain below the endurance limits at which fatigue and structural rutting initiate, confining deterioration to the surface course, which can be periodically milled and replaced without disturbing the structural foundation. The rationale is both economic and environmental, since avoiding full-depth reconstruction conserves virgin materials and reduces the embodied carbon associated with pavement renewal (Styer et al., 2024).

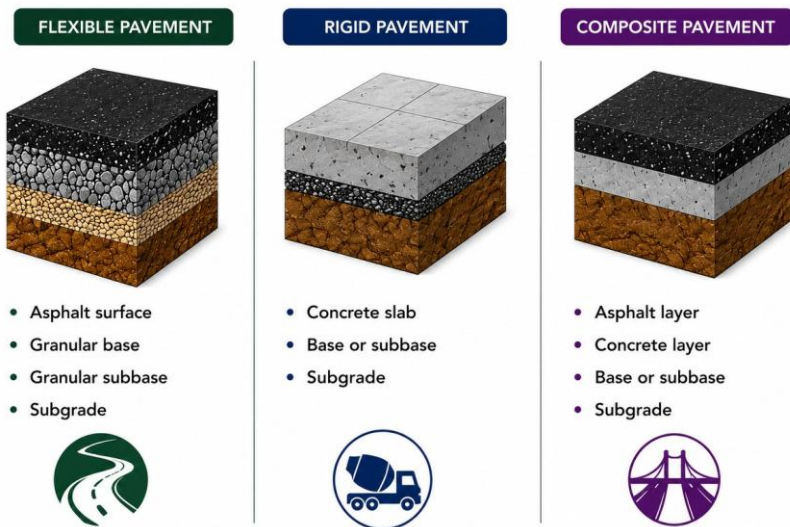


Figure 1.2. *The three principal pavement families, flexible, rigid and composite, compared by their layer make-up and load-carrying concept.*

The functional roles of the individual courses merit explicit statement because they frame the material requirements developed throughout this book. The surface (wearing) course must resist the abrasive and shearing actions of traffic, provide adequate skid resistance and ride quality, seal the structure against water infiltration, and resist rutting and cracking; it is here that the most demanding binder and aggregate specifications apply. The intermediate (binder) course, where present, provides additional load-spreading stiffness and rut resistance while transitioning between the fine surface texture and the coarser base. The asphalt or granular base course is the principal structural layer, distributing load and resisting shear deformation, while the subbase serves as a secondary load-spreading and drainage layer and as a construction platform. The subgrade, finally, provides the ultimate support; its resilient modulus and susceptibility to moisture and frost

fundamentally condition the required thickness of the overlying structure. Effective internal drainage across all of these courses is essential, because the presence of water dramatically accelerates several distress mechanisms, weakening unbound layers and promoting stripping at the bitumen–aggregate interface (Neupane & Wu, 2025).

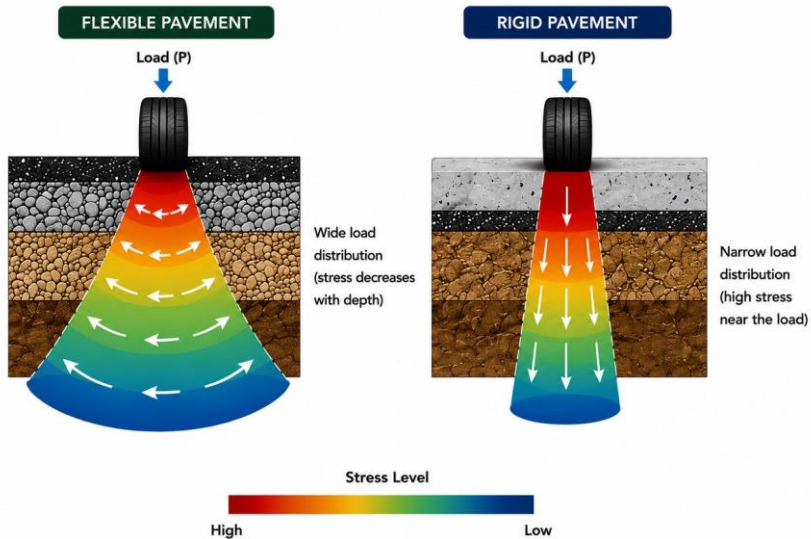


Figure 1.3. *Contrast between flexible and rigid pavements in load spreading, stress-bulb depth and surface deflection, explaining why the two families fail in different ways.*

Modern classification and design increasingly integrate sustainability considerations into the very definition of the pavement structure. The incorporation of reclaimed asphalt pavement (RAP), recycled aggregates, and industrial by-products into base and surface courses is now standard practice in many jurisdictions, and the structural contribution of these recycled layers must be characterized with the same rigour as virgin materials. In the United States alone, tens of millions of tonnes of RAP are reincorporated into new

mixtures each year, and average RAP contents in asphalt mixtures have risen substantially over the past two decades, driven by the dual imperatives of raw-material conservation and cost reduction (Mariyappan, Palammal, & Balu, 2023). Similarly, warm-mix asphalt technologies, which lower production and compaction temperatures, are reshaping how surface and binder courses are manufactured and placed, offering meaningful reductions in energy consumption and greenhouse-gas emissions without necessarily compromising structural function (Milad et al., 2022). These developments mean that the contemporary flexible pavement is not merely a static layered system but an evolving assembly whose classification must accommodate recycled content, functional additives, and life-cycle environmental performance alongside traditional structural criteria.

Chemistry and Physical Structure of Bitumen

Bitumen, the binder that distinguishes flexible from rigid pavements, is a dark, highly viscous residue obtained principally from the distillation of crude oil, and its complex chemistry is the single most important determinant of asphalt-mixture performance. Chemically, bitumen is an extraordinarily heterogeneous mixture of hydrocarbon molecules together with lesser quantities of heteroatoms, sulphur, nitrogen, and oxygen, and trace metals such as vanadium and nickel. Because the number of distinct molecular species is far too large to enumerate individually, bitumen chemistry is conventionally approached through fractionation into four generic families defined by their solubility and polarity: saturates, aromatics, resins, and asphaltenes, collectively known by the acronym SARA (Porto, Angelico, Caputo, Abe, Teltayev, & Oliviero Rossi, 2022). This operational classification, though a simplification, provides a powerful framework for relating composition to physical behaviour and remains the dominant paradigm in binder science. The four

SARA fractions and the principal factors that control their colloidal balance are depicted in Figure 1.4.

The four SARA fractions differ markedly in molecular character and functional role. Saturates are nonpolar, aliphatic and naphthenic hydrocarbons of comparatively low molecular weight; they act as a plasticizing medium and are correlated with the softening behaviour of the binder. Aromatics, the naphthenic-aromatic compounds that constitute the largest fraction by mass in most bitumens, form the principal dispersing medium in which the heavier constituents are suspended. Resins are polar molecules bearing a variety of functional groups and alkyl side chains; they possess strong adsorptive tendencies and act as peptizing agents that keep the heaviest fraction dispersed. The asphaltenes, defined operationally as the fraction insoluble in n-heptane but soluble in toluene, are the highest-molecular-weight, most polar and most aromatic constituents, consisting of polycyclic aromatic cores decorated with heterocyclic functionalities and aliphatic side chains. The asphaltene content exerts a first-order influence on stiffness, viscosity, and the temperature susceptibility of the binder (Lesueur, 2009). A comprehensive contemporary treatment of the properties, separation methods, and reactivity of the asphaltene and maltene (saturate–aromatic–resin) fractions underscores that the boundaries between these families are operationally rather than sharply defined, and that the analytical method chosen strongly affects the measured fractional composition (Primerano, Mirwald, & Hofko, 2024).

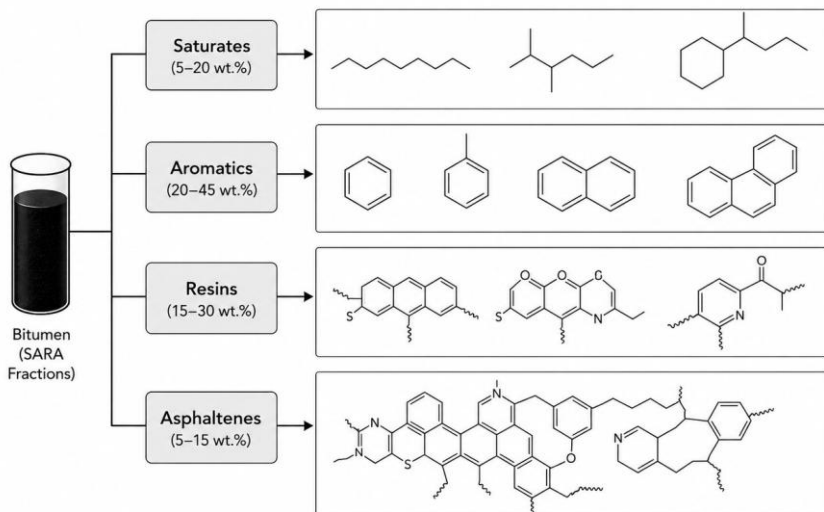


Figure 1.4. Colloidal SARA structure of bitumen, saturates, aromatics, resins and asphaltenes, together with the factors (temperature, ageing, oxidation) that control its stability.

The manner in which these fractions organize themselves in space, the physical or colloidal structure of bitumen, has been the subject of debate for the better part of a century, and it is this structure, rather than bulk composition alone, that governs rheological response. The classical colloidal model, whose origins lie in the mid-twentieth century, envisions asphaltenes aggregating into micelle-like clusters that are peptized by adsorbed resins and dispersed within the lower-polarity maltene medium of aromatics and saturates. In this picture, the balance between asphaltene content and the dissolving power of the maltene phase determines whether the bitumen behaves as a "sol" (a well-dispersed, more viscous-flowing system in which asphaltene micelles move freely) or a "gel" (a structured, more elastic system in which micelles associate into a continuous network). The sol-gel character in turn controls the temperature dependence of stiffness, the elastic recovery, and the

resistance to permanent deformation. Lesueur (2009) synthesized the rheological consequences of this colloidal picture, demonstrating that a solvation parameter capturing the effective volume fraction of the dispersed asphaltene phase can quantitatively account for the influence of asphaltenes on viscosity and modulus.

Modern experimental and computational evidence has both refined and challenged the simplest version of the colloidal model. Advances in microscopy, small-angle scattering, nuclear magnetic resonance, and molecular-dynamics simulation have revealed that the spatial organization of bitumen is more nuanced than a static arrangement of discrete micelles suspended in a solvent, and that a spectrum of interpretations, ranging from genuine colloidal dispersion to near-complete molecular dissolution of asphaltenes in the maltene medium, can be reconciled with different lines of evidence (Porto et al., 2022). At the mesoscale, many bitumens exhibit a characteristic "bee-like" surface microstructure observable by atomic force microscopy, whose origin has been variously attributed to the crystallization of waxy components and to asphaltene-rich domains. Molecular simulations increasingly show that the thermodynamic stability of asphaltene aggregates is actively supported by the surrounding maltene molecules and by resin–asphaltene interactions, and that the interplay among all four fractions, rather than any single component, dictates the aggregation state and hence the bulk mechanical response (Wang & Wang, 2024). The practical upshot is that two bitumens of nominally identical grade but differing crude source and refining history can display materially different structural stability, ageing behaviour, and compatibility with modifiers.

Table 1.1. SARA fractions of bitumen and their role

Fraction	Character	Role in bitumen
Saturates	Non-polar, waxy oils	Plasticiser; lower viscosity

Fraction	Character	Role in bitumen
Aromatics	Low-MW aromatic oils	Dispersion medium for asphaltenes
Resins	Polar, adhesive	Peptise asphaltenes; adhesion, ductility
Asphaltenes	High-MW polar solids	Provide stiffness and structure

The physical structure of bitumen is also intrinsically thermorheologically complex and time-dependent. Bitumen is a viscoelastic material whose response spans from nearly elastic behaviour at low temperatures and short loading times to essentially viscous flow at high temperatures and long loading times, with the transition governed by the glass transition and by the relaxation dynamics of the various molecular populations. This viscoelasticity is the physical basis for the performance-grading systems discussed later in this chapter, and it is the property most directly targeted by the functional modifiers, polymers, crumb rubber, nanomaterials, and rejuvenators, that form the subject of subsequent chapters. Polymer modification, and in particular the incorporation of styrene–butadiene–styrene (SBS) block copolymers, alters the colloidal structure by forming a swollen, elastic polymer network that interpenetrates the maltene phase, thereby broadening the useful temperature range, enhancing elastic recovery, and improving resistance to both permanent deformation and cracking (Alnadish, Katman, Ibrahim, Gamil, & Mashaan, 2023). The efficiency of such modification depends critically on the compatibility between the polymer and the bitumen's chemistry: a maltene phase rich in aromatics promotes swelling and stable dispersion of the polymer, whereas an asphaltene-rich, poorly compatible bitumen may lead to phase separation during storage (Yan et al., 2023). Nanomaterial modifiers, including graphene and graphene-derived platelets,

similarly act by reinforcing the binder microstructure, raising the performance grade, lowering thermal susceptibility, and improving fatigue and rutting resistance, though their effectiveness is likewise governed by dispersion and interfacial interaction with the bituminous matrix (Polo-Mendoza et al., 2023).

Finally, the chemistry of bitumen is not static over the pavement's life but evolves through oxidative ageing, a topic developed more fully in Section 1.4. It suffices here to note that the same functional groups and colloidal balance that define the fresh binder are progressively altered by reaction with atmospheric oxygen, principally through the formation of carbonyl and sulfoxide moieties, which increase polarity, shift material from the maltene toward the asphaltene fraction, and stiffen and embrittle the binder over time (Ahmad, Khedmati, Mensching, Hofko, & Haghshenas, 2024). This inseparability of composition, physical structure, and long-term chemical evolution is a recurring theme: any advanced functional material intended to improve sustainability or durability must be evaluated not only against the properties of the fresh binder but against the entire trajectory of its chemical and rheological change in service.

Aggregates, Mix Design and Volumetric Properties

If bitumen is the binder that gives flexible pavements their name, mineral aggregate is the structural skeleton that carries the great majority of the applied load. Aggregates typically constitute on the order of ninety-four to ninety-six percent of an asphalt mixture by mass, and their properties, gradation, shape, angularity, surface texture, toughness, and mineralogy, exert a controlling influence on the mechanical performance of the mixture. Coarse aggregate provides the interlocking framework that resists shear deformation and rutting, while fine aggregate and mineral filler occupy the interstices, contribute to stiffness, and interact intimately with the

binder to form the mastic. The shape and angularity of aggregate particles are particularly consequential: highly angular, rough-textured crushed particles develop strong particle-to-particle interlock and internal friction, enhancing resistance to permanent deformation, whereas rounded, smooth particles tend to slip past one another under load. Aggregate mineralogy and micro-texture additionally govern the long-term skid resistance of the surface course, since the resistance of the aggregate to polishing under traffic determines whether adequate micro-texture, and hence friction, is retained over the pavement's life (Zhang, Zeng, Wang, & Qu, 2024). The aggregate skeleton, with its load-bearing stone-on-stone contact, the binder–filler mastic and the controlled air voids, is shown in Figure 1.5, and the volumetric composition of the compacted mixture (air voids, voids in the mineral aggregate, voids filled with asphalt and effective binder) in Figure 1.6.

The gradation, or particle-size distribution, of the aggregate blend is arguably the single most influential design variable, because it determines the packing density, the volume of voids available for binder and air, and the load-transfer characteristics of the mineral skeleton. Dense-graded mixtures, in which a continuous distribution of particle sizes produces a tightly packed, low-void structure, are the workhorses of surface and structural courses; gap-graded mixtures, such as stone-mastic asphalt, deliberately omit intermediate sizes to create a coarse-aggregate skeleton with stone-on-stone contact stabilized by a rich mastic; and open-graded friction courses use a preponderance of single-sized coarse aggregate to create an interconnected void structure for surface drainage and noise reduction. Each gradation family responds differently to binder content, modifier type, and compaction, and the selection of gradation is therefore inseparable from the broader mix-design process. The nominal maximum aggregate size, moreover, conditions the volumetric criteria that a mixture must satisfy, with

finer mixtures requiring higher minimum voids in the mineral aggregate to accommodate sufficient binder for durability (Zeiada et al., 2022).

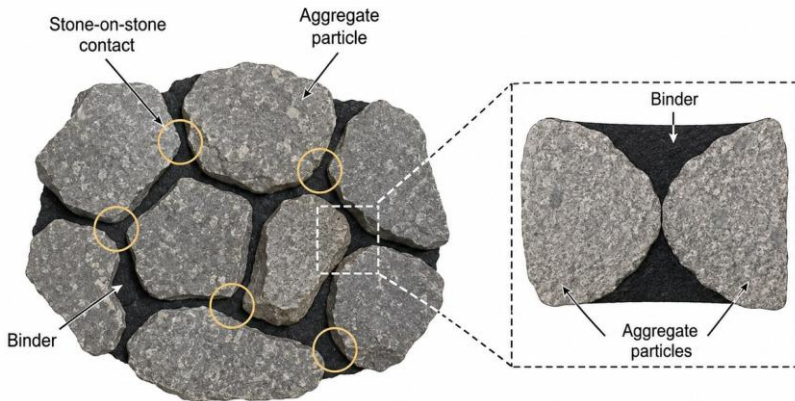


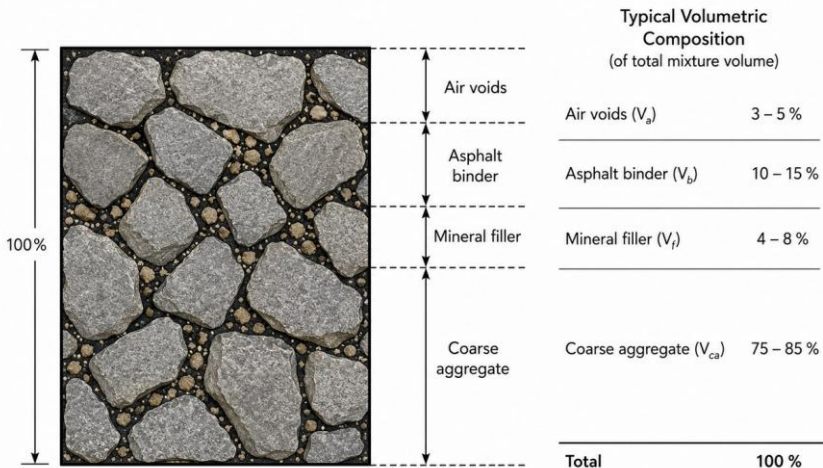
Figure 1.5. *Aggregate skeleton of an asphalt mixture illustrating stone-on-stone load transfer, the binder–filler mastic that coats and bonds the particles, and the controlled air voids that govern durability and permeability.*

The dominant contemporary framework for proportioning dense-graded asphalt mixtures is the Superpave (Superior Performing Asphalt Pavements) volumetric mix-design system, developed under the Strategic Highway Research Program and codified in AASHTO standards. In the Superpave approach, aggregate is compacted with a gyratory compactor that simulates the kneading action of field compaction, and the resulting specimens are evaluated principally through their volumetric properties rather than through empirical stability tests alone. The governing volumetric parameters are the air voids (the volume of interconnected and

isolated voids remaining after compaction), the voids in the mineral aggregate (VMA, the total intergranular void volume that includes both the air voids and the effective binder), and the voids filled with asphalt (VFA, the proportion of the VMA occupied by effective binder). The design binder content is conventionally selected to achieve a target air-void content of approximately four percent at the design gyration level, with VMA and VFA constrained within limits that vary according to nominal maximum aggregate size (Zeiada et al., 2022). VMA occupies a central position in this scheme because it is the primary control on binder film thickness and mixture durability: too little VMA leaves insufficient room for a durable binder film and predisposes the mixture to bleeding and rutting, whereas excessive VMA can yield an unstable, binder-rich mixture prone to permanent deformation.

The rationale for volumetric control rests on the recognition that the interconnected effects of binder content, aggregate packing, and compaction on field performance can be captured, to a first approximation, through the geometry of the compacted mixture. Air-void content is critical because it must be low enough at construction to prevent excessive permeability, which would admit water and oxygen, accelerating stripping and ageing, yet high enough to accommodate the secondary densification that occurs under traffic without the mixture flushing or rutting. Typical target in-place air voids after construction lie in the range associated with a design value near four percent, recognizing that traffic will further compact the mixture toward a lower ultimate void content. The effective binder content, distinguished from the total binder content by the portion absorbed into the surface porosity of the aggregate, governs both durability and the risk of permanent deformation; the mastic formed by the effective binder and mineral filler is the phase in which fatigue and ageing damage predominantly localize. The volumetric approach thus provides an economical and reproducible

means of proportioning mixtures, but it is not without limitations, and its inability to guarantee mechanical performance across all conditions has motivated the evolution toward balanced and performance-based methods discussed below.



Typical Volumetric Composition of Asphalt Mixture

Figure 1.6. *Volumetric composition of a compacted asphalt mixture, air voids (V_a), voids in the mineral aggregate (VMA), voids filled with asphalt (VFA) and effective binder (V_b), the quantities that underpin mix design.*

Beyond the intrinsic properties of the constituents, the mix-design process must ensure adequate resistance to moisture-induced damage, since the durability of a volumetrically sound mixture can be undermined by the loss of adhesion at the bitumen–aggregate interface. Moisture damage manifests as stripping, the physical separation of the binder film from the aggregate surface in the presence of water, and as cohesive weakening of the mastic; it is influenced by aggregate mineralogy, surface chemistry, binder composition, and the void structure that controls water ingress.

Siliceous aggregates such as granite tend to bond less durably with acidic bitumen than do calcareous aggregates such as limestone, and mixtures with marginal or interconnected voids are especially vulnerable. Mitigation strategies incorporated at the design stage include the use of hydrated lime or liquid anti-stripping additives, the selection of compatible aggregate–binder combinations, and the control of void structure, and the moisture susceptibility of a candidate mixture is routinely verified through conditioned mechanical testing (Neupane & Wu, 2025).

The volumetric paradigm is increasingly complemented, and in some jurisdictions supplanted, by balanced mix design (BMD), which augments or replaces purely volumetric acceptance criteria with direct performance tests for the principal distress modes. In a balanced framework, candidate mixtures are subjected to laboratory tests that quantify rutting resistance at high temperature and cracking resistance at intermediate and low temperatures, and the binder content and composition are adjusted to satisfy both simultaneously, recognizing that a mixture optimized against rutting alone tends to become brittle and crack-prone, while a mixture optimized against cracking alone tends to rut. This shift is especially significant for sustainable materials, because mixtures containing high proportions of RAP, recycled shingles, or crumb rubber may meet volumetric targets yet exhibit altered cracking or deformation behaviour that only a performance-based evaluation can reveal (Mariyappan et al., 2023). The mix-design process, in short, is evolving from a primarily geometric exercise toward an integrated optimization that couples volumetrics, mechanical performance, moisture durability, and life-cycle environmental impact, providing the design context within which the advanced functional materials of subsequent chapters must be evaluated.

Performance Requirements and Common Distress Mechanisms (rutting, fatigue, cracking, aging)

The performance requirements imposed on a flexible pavement follow directly from the loading and environmental conditions it must withstand, and they are best understood as a set of frequently competing demands that any successful material or structural solution must reconcile. A pavement surface must simultaneously resist permanent deformation under heavy, slow-moving, or channelized traffic at high summer temperatures; resist fatigue cracking under the millions of repeated load cycles imposed over its design life; resist thermal and reflective cracking at low temperatures and under thermal cycling; retain adequate friction and ride quality; and resist the moisture- and oxygen-driven deterioration that progressively degrades all of these properties. The central difficulty of pavement engineering is that measures which improve one performance attribute often degrade another, stiffening a binder to resist rutting, for example, tends to embrittle it and reduce its resistance to fatigue and thermal cracking, so that performance specification is inherently an exercise in balance (Zeiada et al., 2022). The principal distress mechanisms that these requirements must address are summarized in Figure 1.7, while Figure 1.8 places the whole process within the workflow of flexible-pavement materials engineering, from material selection through to a sustainable pavement. This section surveys the principal distress mechanisms in turn, emphasizing their physical origins, their dependence on material properties, and the way in which they collectively define the requirements that advanced functional materials aim to satisfy.

The performance-grading (PG) system introduced by the Strategic Highway Research Program provides the contemporary framework within which binder-level performance requirements are

specified, and it represents a deliberate attempt to relate measured rheological properties directly to field distress. A binder graded PG 64-22, for instance, is required to possess adequate rutting resistance up to a seven-day maximum pavement temperature of 64 °C and adequate cracking resistance down to a minimum temperature of -22 °C. High-temperature rutting resistance is assessed through the dynamic shear rheometer, historically via the parameter $|G|/\sin \delta$ and, in the current specification, through the multiple-stress creep-recovery (MSCR) test, whose non-recoverable creep compliance provides a more reliable indicator of permanent-deformation resistance for both neat and polymer-modified binders. Intermediate-temperature fatigue resistance is characterized through $|G| \cdot \sin \delta$, and low-temperature cracking resistance through the bending-beam rheometer, which measures creep stiffness and its rate of relaxation. The evolution of these test methods, and their extension to accommodate modified binders whose behaviour was poorly captured by the original neat-binder framework, reflects the continuing refinement of performance-based specification (Zeida et al., 2022).

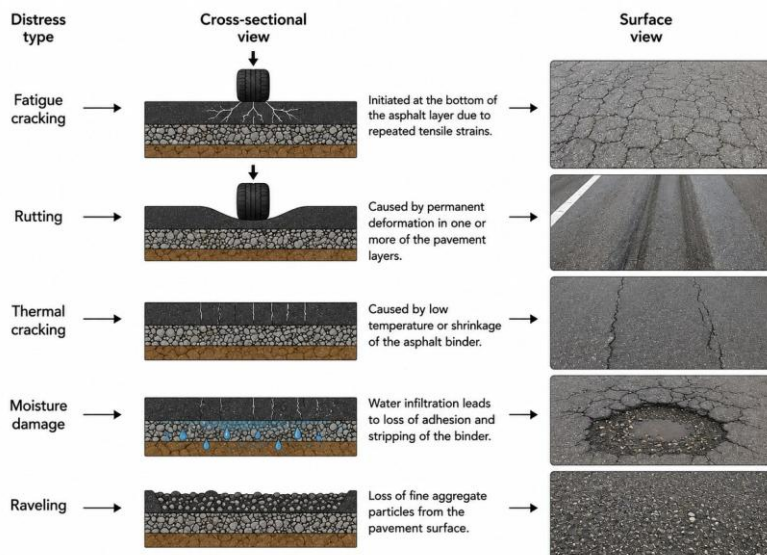


Figure 1.7. *Principal distress mechanisms of flexible pavements, rutting, fatigue and thermal cracking, moisture damage, raveling and ageing, each shown with its characteristic cause.*

Rutting, or permanent deformation, is the accumulation of irrecoverable strain in the wheel paths, manifesting as longitudinal depressions that impair ride quality, promote hydroplaning through water ponding, and ultimately compromise safety. Two distinct mechanisms contribute: structural rutting, in which permanent deformation accumulates in the unbound layers or subgrade owing to inadequate structural capacity, and, more commonly in well-designed structures, instability rutting, in which shear flow occurs within the asphalt layers themselves under the combined action of high temperature and slow or static loading. The latter is governed principally by the high-temperature stiffness and elasticity of the binder, the volumetric proportioning of the mixture, and above all the strength of the aggregate skeleton, since a strong stone-on-stone contact structure resists the shear stresses that drive flow. Elevated summer pavement temperatures and heavy, channelized axle loads

are the dominant field drivers, and modelling of rutting has progressed from empirical regressions toward mechanistic and machine-learning approaches that couple material characterization with traffic and climate inputs (Albayati, 2023; Deng & Shi, 2023). Polymer modification, crumb-rubber modification, and nanomaterial reinforcement are among the principal material strategies for improving rutting resistance, each acting by increasing the elastic component of binder response and the resistance of the mastic to flow (Alnadish et al., 2023; Polo-Mendoza et al., 2023).

Fatigue cracking, historically termed alligator or bottom-up cracking, arises from the repeated tensile strains induced at the bottom of the bituminous layer, or within it, by the flexure of the pavement under passing wheel loads. Under each load cycle the asphalt experiences a small tensile strain; over millions of cycles, microcracks nucleate and coalesce, propagating until an interconnected pattern of cracks resembling the scales of an alligator appears at the surface, admitting water and precipitating further structural deterioration. The phenomenon is fundamentally a manifestation of the viscoelastic and damage behaviour of the binder-rich mastic phase, and its severity depends on the magnitude of the tensile strain (itself a function of layer thickness and stiffness), the stiffness and healing capacity of the binder, the mixture's volumetric composition, and temperature. The prediction of fatigue life has been approached through phenomenological models that correlate cycles to failure with strain amplitude, through mechanistic frameworks grounded in continuum damage mechanics and viscoelastic fracture, and through numerical simulation, with each family of methods offering distinct advantages and limitations (Sudarsanan & Kim, 2022). Because thicker, stiffer bound layers reduce the critical tensile strain, the perpetual-pavement concept exploits the existence of a fatigue endurance limit to design structures in which fatigue cracking is effectively suppressed, a

strategy that also confers sustainability benefits by extending renewal intervals (Alsheyab et al., 2024).

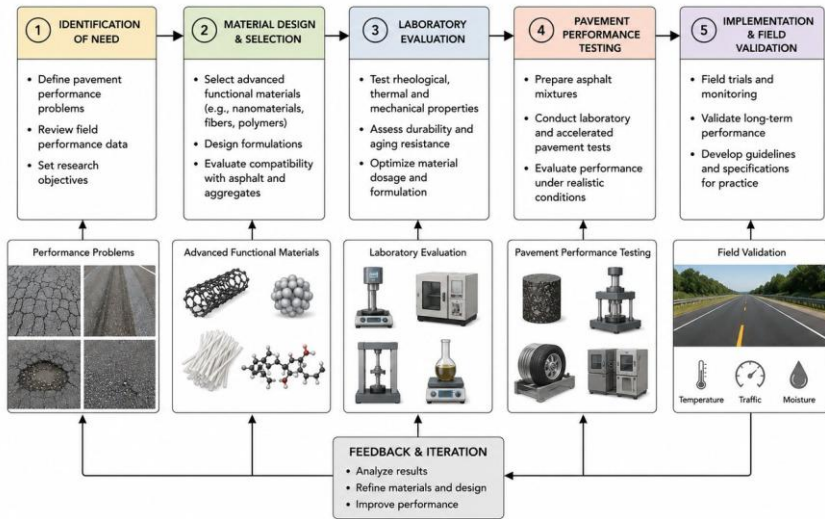


Figure 1.8. Workflow of flexible-pavement materials engineering, from material selection and laboratory characterization through mix design and performance evaluation to a sustainable, field-ready pavement.

Thermal and low-temperature cracking constitute a distinct family of distress driven by environmental rather than traffic loading. When a pavement cools, the bituminous layer contracts, but restraint against contraction generates tensile stress; if this stress exceeds the tensile strength of the mixture, a transverse crack forms across the pavement. Under repeated thermal cycling, an analogous accumulation of damage produces thermal-fatigue cracking even where a single cooling event would not cause failure. The governing material properties are the low-temperature stiffness of the binder and its capacity to relax stress, both captured in the bending-beam rheometer parameters, together with the glass-transition behaviour

and the coefficient of thermal contraction of the mixture. Binders that remain too stiff and relax stress too slowly at low temperature are especially prone to thermal cracking, so that the low-temperature grade limit directly encodes this requirement. Reviews of low-temperature cracking emphasize that binder chemistry, ageing state, and modification all influence the cracking resistance, and that mixture-scale behaviour cannot be inferred from binder properties alone without accounting for aggregate and volumetric effects (Guo, Yao, & Du, 2023). Reflective cracking, in which cracks in an underlying layer propagate upward through an overlay, and top-down cracking, initiating at the surface under the combined influence of tyre contact stresses and ageing, complete the spectrum of crack-related distress and further underscore the need for binders and mixtures that balance stiffness against ductility.

Ageing is the progressive, largely irreversible alteration of binder properties over the pavement's life, and it is both a distress mechanism in its own right and an amplifier of every other mechanism. Ageing proceeds in two broad phases: a short-term phase during hot mixing, storage, and placement, dominated by the loss of volatile components and rapid oxidation at elevated temperature, and a long-term phase in service, dominated by the slow diffusion-limited reaction of the binder with atmospheric oxygen, augmented by ultraviolet radiation at the surface. Chemically, oxidative ageing is characterized by the formation and accumulation of carbonyl and sulfoxide functional groups, tracked through the corresponding infrared absorption bands, and by a shift of material from the maltene toward the asphaltene fraction, which increases polarity, viscosity, and stiffness while reducing ductility and relaxation capacity (Ahmad et al., 2024). The mechanical consequence of this stiffening and embrittlement is a progressive increase in susceptibility to fatigue and thermal cracking and a reduction in the binder's self-healing capacity, so that ageing

effectively shifts the balance of the pavement's performance away from durability over time. Coupled thermal-oxidative and ultraviolet exposure has been shown to intensify these surface changes, contributing to the top-down cracking frequently observed in older pavements (Yang, Li, Xie, Yang, & Liu, 2022). The comprehensive characterization of ageing, chemical, morphological, and rheological, remains an active research frontier, and it is central to the evaluation of any sustainable material, since additives such as recycled binder, rejuvenators, and antioxidants act precisely by modifying the ageing trajectory (Ahmad et al., 2024; Primerano et al., 2024).

Table 1.2. *Principal distress mechanisms of flexible pavements*

Distress	Primary cause	Governing condition	Mitigation
Rutting	Permanent shear, densification	High temperature, heavy load	Stiffer, more elastic binder
Fatigue cracking	Repeated tensile strain	Intermediate temp., traffic	Flexible, self-healing binder
Thermal cracking	Thermal contraction stress	Low temperature	Low stiffness, high m-value
Moisture damage	Loss of adhesion, cohesion	Water, freeze-thaw	Anti-strip, hydrophobic modifiers
Ageing, embrittlement	Oxidation, UV radiation	Time, climate	Antioxidants, barrier fillers

Moisture-induced damage, though introduced in Section 1.3 in the context of mix design, must also be recognized as a performance requirement and distress mechanism in its own right, because it interacts synergistically with the mechanical distresses described above. The ingress of water weakens the adhesive bond

between binder and aggregate and the cohesive strength of the mastic, so that a mixture already stressed by traffic and thermal loading fails more readily when moisture is present; stripping at the bottom of the asphalt layer, for example, dramatically reduces fatigue life, and moisture in unbound layers precipitates structural rutting. The costs of moisture-related deterioration, including pothole formation, are substantial, and the mechanism is governed by the same interfacial chemistry, void structure, and material compatibility that condition the mix-design decisions discussed earlier (Neupane & Wu, 2025). The interconnection of moisture damage with rutting, fatigue, and cracking exemplifies the broader principle that pavement distresses do not occur in isolation but reinforce one another, so that durable performance requires simultaneous resistance across the full spectrum of mechanisms.

Taken together, these performance requirements define the target against which the advanced functional and sustainable materials examined in this book are to be judged. A successful material innovation must improve, or at least not compromise, resistance to rutting, fatigue, thermal cracking, ageing, and moisture damage simultaneously, while advancing the overarching sustainability objectives of reduced virgin-material consumption, lower energy use, and diminished greenhouse-gas emissions (Milad et al., 2022; Styer et al., 2024). Balanced mix design and performance-based binder specification provide the evaluative frameworks within which this multi-objective optimization is conducted, and multiscale modelling increasingly supplies the predictive tools to anticipate long-term behaviour before field deployment (Wang & Wang, 2024). The chapters that follow build upon these fundamentals, examining in detail the classes of functional materials, polymer and rubber modifiers, nanomaterials, bio-based and recycled binders, rejuvenators, and warm-mix and self-healing technologies, through which the enduring challenges of

flexible-pavement performance are being addressed in the pursuit of more durable and more sustainable roads.

AUTHOR'S PERSPECTIVE

In practice, the most under-appreciated fundamental is that the binder film thickness couples to every distress at once: too thin and the mixture is brittle and permeable, too thick and it ruts. Before reaching for any advanced modifier I would insist on sound volumetrics and a balanced-mix-design check, because a functional additive rarely rescues a mixture whose air-void and binder content are wrong to begin with. The fundamentals are not a preface to the innovation; they are the constraint the innovation must respect.

CHAPTER SUMMARY

This chapter established the structural, chemical and mechanical fundamentals on which the book builds: the load-spreading behaviour of the layered system, the colloidal SARA structure of bitumen, the aggregate skeleton and volumetric proportioning, and the five coupled distress mechanisms that any functional material must address.

Key findings

- ▶ Flexible pavements distribute load by shallow spreading, so surface-course stiffness dominates the structural response.
- ▶ Binder behaviour is governed by the SARA colloidal balance, which every modifier ultimately perturbs.
- ▶ Rutting, fatigue, thermal cracking, moisture damage and ageing are coupled, so improving one must not degrade the others.

Design recommendations

- ▶ Fix volumetrics and balanced mix design before adding any functional modifier.
- ▶ Match aggregate mineralogy and binder grade to the governing climate and traffic distress.
- ▶ Treat recycled content, energy and emissions as design constraints from the outset.

Future research

- ▶ Performance-based, multi-distress specifications that reward simultaneous improvement.
- ▶ Multiscale models linking binder chemistry to field distress prediction.

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CHAPTER 2

Advanced Functional Materials in Pavement Engineering: An Overview

Definition and Classification of Functional Materials

The transition from empirical to performance-based pavement design has progressively reframed the way engineers think about the constituents of flexible pavements. Historically, bitumen and mineral aggregate were treated as passive commodities whose principal role was to provide cohesion and load distribution. Contemporary practice, by contrast, increasingly conceives of pavement constituents as *functional* materials, that is, materials selected and engineered not merely to fill a volume but to deliver a defined, often quantifiable, functional response under service conditions. In the context of this book, a functional material is understood as any additive, modifier, filler, fiber, or engineered particle that is deliberately introduced into the bituminous system to modify one or more of its physical, mechanical, rheological, thermal, electrical, or environmental behaviours beyond what conventional binder and aggregate alone can achieve. This definition deliberately

spans a broad spectrum, from long-established polymeric modifiers that improve rutting and cracking resistance to emerging "smart" systems capable of sensing strain, regulating temperature, or autonomously repairing microcracks (Yang et al., 2024; Wang et al., 2023). Figure 2.1 presents the principal families of functional materials together with the performance and sustainability benefits they impart, and Figure 2.2 organises them into a structured classification.

A functional material is distinguished from a conventional constituent by its *intentionality* and its *specificity of effect*. Ordinary mineral filler contributes to the mastic and stiffens the binder, but it is rarely selected to achieve a narrowly defined target such as a prescribed increase in the elastic recovery of the binder or a measured reduction in mixing temperature. Functional materials, in contrast, are chosen precisely because they perturb the bituminous matrix in a targeted and reproducible manner. The polymer styrene–butadiene–styrene (SBS), for instance, is added to establish a continuous elastomeric network that raises the softening point, broadens the useful temperature interval, and enhances elastic recovery of the binder (Wang, Wei, Liu, Ren, & Wang, 2021). Nano-silica is introduced to increase viscosity, stiffness, and ageing resistance through interfacial and adsorption effects at the nanoscale (Cheraghian, Wistuba, Kiani, Barron, & Behnood, 2021). In each case the material is defined by the function it performs rather than by its chemical family alone.

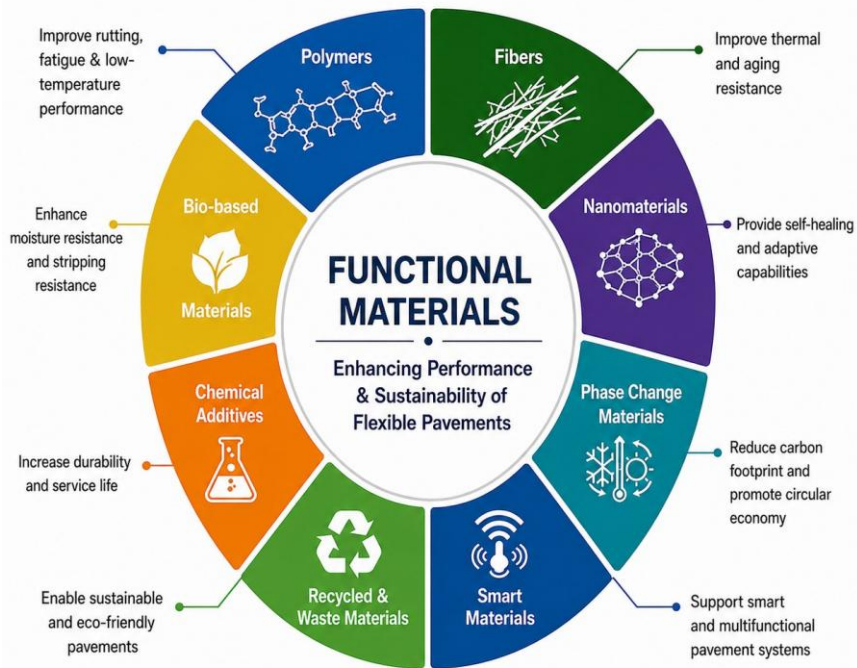


Figure 2.1. The main families of functional materials for flexible pavements and the performance and sustainability benefits that each family contributes.

Classifying the diverse population of functional materials used in flexible pavements is inherently multidimensional, because materials can be grouped according to chemistry, morphology, mechanism of action, or intended performance outcome. A chemistry-based taxonomy distinguishes organic modifiers (thermoplastic elastomers, plastomers, waxes, bio-oils, and rejuvenators), inorganic materials (mineral nanoparticles, layered silicates, metallic oxides), and carbon-based materials (graphene,

carbon nanotubes, carbon fibers). A morphology-based taxonomy separates particulate additives, one-dimensional fibrous reinforcements, two-dimensional nanosheets, and three-dimensional network-forming polymers. Neither scheme, however, captures the *functional* essence that is most relevant to design. For the purposes of this book, therefore, a function-oriented classification is adopted, in which materials are organised according to the primary engineering service they render to the pavement system.

Under a function-oriented scheme, five broad and partly overlapping families can be delineated. The first family comprises *rheology and performance modifiers*, dominated by polymers such as SBS, styrene-butadiene rubber, ethylene-vinyl acetate, and reactive elastomeric terpolymers, together with crumb rubber derived from end-of-life tyres. These materials principally enlarge the temperature interval over which the binder behaves acceptably, simultaneously improving high-temperature rutting resistance and low-temperature or fatigue cracking resistance (Yang et al., 2024; Joohari & Giustozzi, 2022). The second family consists of *processing and sustainability additives*, most prominently the warm-mix asphalt (WMA) technologies, organic waxes, chemical surfactants, and foaming systems, that lower production and compaction temperatures and thereby reduce energy consumption and emissions (Rubio, Martínez, Baena, & Moreno, 2012; Belc, Coleri, Belc, & Costescu, 2021). The third family covers *reinforcing materials*, chiefly discrete fibers such as basalt, aramid, polyolefin, glass, and cellulose fibers, which provide crack bridging, stress dispersion, and enhanced toughness through a three-dimensional network effect within the mixture (Men, Xiao, Tang, Han, Kang, & Wu, 2022; Wu, Meng, Xia, & Xiao, 2022; Khan et al., 2024). The fourth family is that of *nanomaterials*, including nano-silica, nano-clays, metallic oxides, graphene, graphene nanoplatelets, and carbon nanotubes, whose extraordinarily high specific surface area allows

them to influence binder behaviour, ageing, and even electrical conductivity at very low dosages (Huang, Wang, Wu, Zhang, & Huang, 2024; Almashaqbeh et al., 2024). The fifth and most rapidly evolving family encompasses *smart and multifunctional materials*, which impart responsive or active capabilities such as self-healing of microcracks, thermoregulation through latent-heat storage, and self-sensing of mechanical strain (Anupam, Sahoo, & Chandrappa, 2022; Wang et al., 2023; Wang, Faßbender, Dong, Schulze, Oeser, & Liu, 2023).

It is important to emphasise that these families are not mutually exclusive; indeed, the frontier of research lies precisely at their intersections. Carbon nanotubes, for example, simultaneously belong to the nanomaterials family and to the smart-materials family, because they can enhance binder rheology while also rendering the composite electrically conductive and therefore capable of self-sensing (Xin et al., 2020). Steel or carbon fibers can serve as mechanical reinforcement and, when combined with electromagnetic induction, become the enabling medium for self-healing through localized heating. Crumb rubber functions as a performance modifier and simultaneously as a sustainability additive, since it diverts waste tyres from landfill while improving elastic recovery and fatigue life (Joohari & Giustozzi, 2022). This convergence of functions is a defining characteristic of the advanced materials treated in this volume and a central reason why a rigidly compartmentalised classification is of limited practical value.

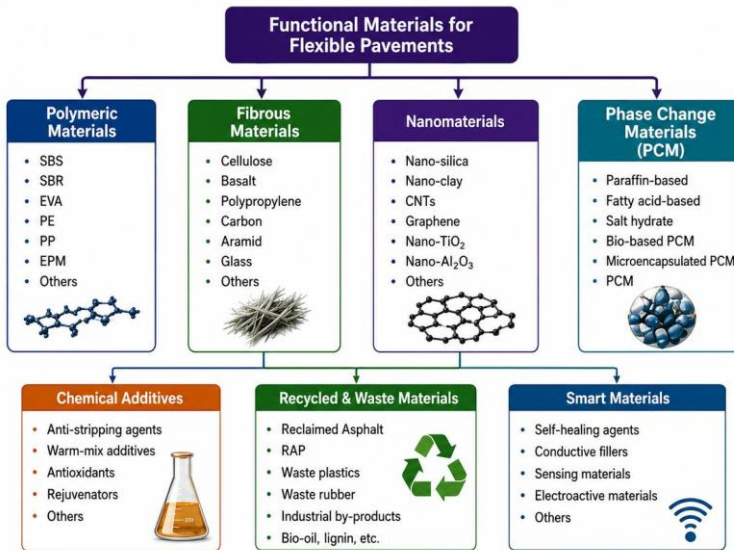


Figure 2.2. Classification of functional materials into polymeric, fibrous, nano, phase-change, chemical, recycled and smart families, with representative examples of each.

A further conceptual distinction underlies the function-oriented taxonomy: the difference between *passive* and *active* functionality. Passive functional materials modify a property once and thereafter behave as static constituents; a polymer network, once formed, continuously provides its elastic contribution but does not respond dynamically to changing stimuli. Active or responsive functional materials, in contrast, react to an external or internal trigger, temperature, an electromagnetic field, mechanical stress, or crack formation, and change their behaviour accordingly. Phase-change materials absorb and release latent heat as the pavement crosses their transition temperature, thereby damping thermal extremes (Wang et al., 2023). Encapsulated rejuvenators release healing agents only when a propagating crack ruptures the capsule wall (Sun et al., 2017). Self-sensing composites alter their electrical resistance in proportion to imposed strain, effectively transforming

the pavement into a distributed sensor (Birgin, D'Alessandro, Laflamme, & Ubertini, 2022). This gradient from passive to active functionality is perhaps the single most useful axis along which to understand the trajectory of the field, and it structures much of the discussion in the sections that follow.

Finally, the classification of functional materials cannot be divorced from the overarching objective of sustainability that motivates this book. A material may be functional in a narrow performance sense yet undesirable if it imposes disproportionate environmental, economic, or health burdens across its life cycle. Increasingly, therefore, "functionality" is understood in an expanded sense that embraces resource efficiency, recyclability, reduced energy demand, and lower emissions alongside mechanical and durability benefits. Warm-mix additives, waste-derived crumb rubber, bio-based rejuvenators, and thermoregulating phase-change systems are valued not only for what they do to the binder but for how they reshape the environmental profile of the pavement (Rubio et al., 2012; Tutu & Tuffour, 2016). This dual imperative, engineering performance coupled with environmental stewardship, frames the definitions and classifications adopted throughout the remainder of the chapter and provides the criteria against which the opportunities and limitations of each material family are ultimately judged.

From Conventional Modifiers to Advanced/Smart Materials

The evolution of functional materials in flexible pavements can be read as a progressive expansion of ambition: from correcting the deficiencies of neat bitumen, to reinforcing the mixture, to reducing environmental impact, and ultimately to endowing the pavement with responsive intelligence. Each stage did not supersede the previous one but rather layered new capabilities upon an increasingly sophisticated understanding of the bituminous system.

Tracing this trajectory clarifies why the "advanced" and "smart" materials that dominate current research are best understood as the continuation of a long-standing engineering logic rather than as a radical departure from it. Figure 2.3 maps the principal functions, from rheological modification and adhesion enhancement to crack resistance and self-healing, that these materials deliver to the binder and the mixture.

The first and most consequential step in this evolution was the advent of polymer modification. Neat bitumen is a thermoplastic material whose consistency is highly temperature dependent; it becomes excessively soft and rut-prone at summer service temperatures and brittle and crack-prone in winter. The introduction of thermoplastic elastomers, above all SBS, addressed both extremes simultaneously by forming a continuous, swollen polymer network throughout the maltene-rich phase of the binder. This network raises the softening point, increases the complex modulus at high temperatures, and restores elasticity through a rubber-like recovery mechanism, while the swollen phase remains flexible enough to resist low-temperature cracking (Yang et al., 2024). Plastomers such as ethylene-vinyl acetate, by contrast, form a rigid crystalline network that principally increases stiffness and rutting resistance. Decades of field experience established polymer-modified bitumen (PMB) as the benchmark high-performance binder, and much of the subsequent literature has been devoted to understanding and mitigating its principal weakness, the tendency toward phase separation and poor storage stability arising from the density and polarity mismatch between polymer and bitumen (Wang et al., 2021). The recognition that compatibility, dispersion, and morphology govern the durability of the modified binder was a decisive intellectual advance, because it reframed modification as a problem of controlled microstructure rather than of simple additive dosing.

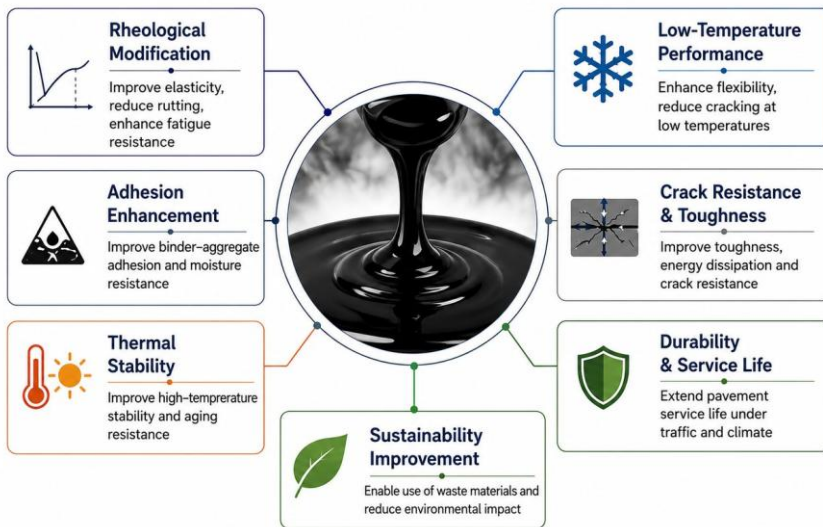


Figure 2.3. *Principal engineering functions delivered by functional materials, from rheological modification and adhesion to crack resistance, thermal stability and sustainability.*

Running parallel to polymer modification was the emergence of waste-derived and reinforcing materials, motivated as much by economics and resource conservation as by performance. Crumb rubber recovered from end-of-life tyres, incorporated by either the wet or the dry process, was found to improve elastic recovery, rutting resistance, fatigue life, and even the acoustic properties of pavements, while providing a sustainable outlet for an enormous global waste stream (Joohari & Giustozzi, 2022). More recent work has pursued hybrid systems that combine crumb rubber with conventional polymers to capture the benefits of both, and has sought to raise the recycled rubber content without sacrificing workability or compatibility. Discrete fibers followed a similar logic in the mixture rather than the binder: basalt, aramid, glass, polyolefin, and cellulose fibers were introduced to bridge microcracks, disperse stress, and inhibit the coalescence of

microcracks into macrocracks, thereby improving cracking, fatigue, and moisture resistance (Men et al., 2022; Wu et al., 2022). The reinforcing mechanism of fibers is fundamentally different from that of polymers: rather than altering the intrinsic rheology of the binder, fibers form a three-dimensional spatial network that mechanically interlocks the mastic and aggregate skeleton and carries tensile stress across incipient fracture planes (Wu et al., 2022).

The third stage in the evolution shifted the emphasis from what materials add to the pavement toward what they allow the industry to avoid, principally energy, emissions, and waste. Warm-mix asphalt technologies epitomise this shift. By employing organic waxes that reduce binder viscosity above their melting point, chemical surfactants that improve aggregate coating and compaction, or foaming processes that transiently expand the binder, WMA additives permit production and compaction at temperatures typically 20 to 40 degrees Celsius below those of conventional hot-mix asphalt (Rubio et al., 2012; Belc et al., 2021). The resulting reductions in fuel consumption, greenhouse-gas emissions, and fume exposure, together with the potential to incorporate higher proportions of reclaimed asphalt pavement, positioned WMA as a foundational sustainability technology (Tutu & Tuffour, 2016; Ahmed & Baig, 2026). Importantly, WMA additives illustrate that a functional material need not improve a mechanical property to be valuable; reducing the process temperature at equivalent performance is itself a functional service of considerable environmental worth.

The fourth stage was defined by the descent to the nanoscale. Nanomaterials, nano-silica, nano-clays, titanium and zinc oxides, graphene, graphene nanoplatelets, and carbon nanotubes, brought a qualitatively new mechanism of action, because their extraordinarily high specific surface area allows extremely small dosages to exert disproportionate effects on binder behaviour (Huang et al., 2024).

Nano-silica increases viscosity, stiffness, and rutting resistance and improves ageing resistance through strong interfacial adsorption of the light bitumen fractions (Cheraghian et al., 2021). Layered nanomaterials such as graphene create tortuous diffusion paths that impede oxygen ingress and thereby retard oxidative ageing, while also increasing stiffness and, at sufficient loadings, imparting electrical conductivity (Almashaqbeh et al., 2024). The nanomaterials era is significant not only for the performance gains achieved but because it forged the conceptual and material bridge to smart pavements: the same conductive carbon nanomaterials that improve rheology and ageing resistance can also transform an electrically insulating asphalt into a piezoresistive, self-sensing composite (Xin et al., 2020).

Table 2.1. *Comparison of principal asphalt modifier families*

Family	Examples	Primary benefit	Limitation
Elastomers	SBS, SBR	Elastic recovery, rutting, fatigue	Storage instability, cost
Plastomers	EVA, PE, PP	High-temperature stiffness	Brittleness at low temperature
Crumb rubber	Waste tyre rubber	Rutting, elasticity, sustainability	Workability, digestion control
Warm-mix additives	Waxes, chemical, foaming	Lower temperature, emissions	Rutting if under-aged
Fibres	Cellulose, glass, basalt	Crack resistance, drainage	Dispersion, mixing
Nanomaterials	Nano-silica, CNT, TiO2	Multi-property, ageing resistance	Dispersion, cost

The current and most advanced stage introduces active functionality, materials and systems that respond to stimuli and perform work within the pavement over its service life. Self-healing

technologies aim to recover the intrinsic crack-healing capacity of bitumen and to amplify it artificially, whether through electromagnetic or microwave induction heating of embedded conductive particles and fibers, or through microencapsulated rejuvenators that are released to soften and reunite crack faces when a capsule is ruptured by a propagating crack (Anupam et al., 2022; Sun et al., 2017). Phase-change materials embedded in the binder or mixture store and release latent heat as they cross their transition temperature, damping the thermal extremes responsible for rutting and thermal cracking and mitigating the urban heat-island effect (Wang et al., 2023; Pinheiro et al., 2023). Self-sensing composites, enabled by conductive carbon additives, convert the pavement itself into a distributed strain and load sensor capable of weigh-in-motion measurement and structural health monitoring (Birgin et al., 2022; Wang, Faßbender, et al., 2023). Collectively, these developments mark the transition from materials that passively endure their environment to materials that actively engage with it.

Viewed as a whole, the progression from conventional modifiers to smart materials exhibits a consistent internal logic. Each successive generation has addressed the limitations exposed by the previous one while broadening the definition of what a pavement material is expected to do. Polymers solved the temperature-susceptibility problem but introduced compatibility challenges; nanomaterials refined performance and unlocked new physical mechanisms but raised questions of dispersion, cost, and safety; smart systems promise autonomous performance recovery and monitoring but confront formidable barriers of durability, scalability, and life-cycle justification. Understanding this lineage is essential, because the interaction mechanisms and selection criteria examined in the remaining sections of this chapter apply, in varying degrees, across the entire continuum from the simplest wax to the most sophisticated self-sensing nanocomposite.

Interaction Mechanisms with the Bituminous Matrix

The performance conferred by any functional material is ultimately governed by how it interacts with the bituminous matrix at the molecular, colloidal, and microstructural scales. Bitumen is a complex colloidal system in which polar, high-molecular-weight asphaltene clusters are peptised and dispersed within a lower-polarity maltene medium comprising saturates, aromatics, and resins. This colloidal architecture, and the mobility of its constituent fractions, dictates the thermorheological behaviour of the binder and, crucially, the manner in which foreign materials integrate with it. Understanding the interaction mechanisms is therefore not an academic nicety but the essential basis for predicting whether a modifier will deliver durable benefits or fail through incompatibility, and it is the connective theme linking every material family discussed in this book. Figure 2.4 summarises the principal interaction mechanisms, physical, mechanical, chemical, hydrogen bonding, network formation and dispersion, through which functional modifiers engage the bituminous matrix.

Polymer modifiers interact with bitumen principally through a swelling-and-network mechanism that is physical rather than chemical in the case of conventional SBS. When SBS is blended into hot bitumen under high shear, the polybutadiene mid-blocks absorb the lighter maltene fractions, particularly the aromatic oils, and swell to several times their original volume, while the polystyrene end-blocks aggregate into rigid physical crosslinks. At sufficient polymer content a continuous, interlocking polymer-rich phase forms and coexists with a bitumen-rich phase, producing a two-phase morphology whose continuity governs the elastic recovery and high-temperature stiffness of the modified binder (Yang et al., 2024). The strength of this interaction is dictated by the compatibility between polymer and bitumen, which depends on the relative density,

molecular weight, polarity, and solubility parameters of the two components. When compatibility is poor, the swollen polymer phase separates and creams under quiescent high-temperature storage, degrading penetration, softening point, ductility, and the anti-rutting factor over a matter of days (Wang et al., 2021). Consequently, the engineering of polymer-modified binders is essentially the engineering of a metastable microstructure, and strategies such as reactive functionalisation, sulphur crosslinking, and hybridisation with crumb rubber are all attempts to stabilise the polymer–bitumen interface against separation (Joohari & Giustozzi, 2022).

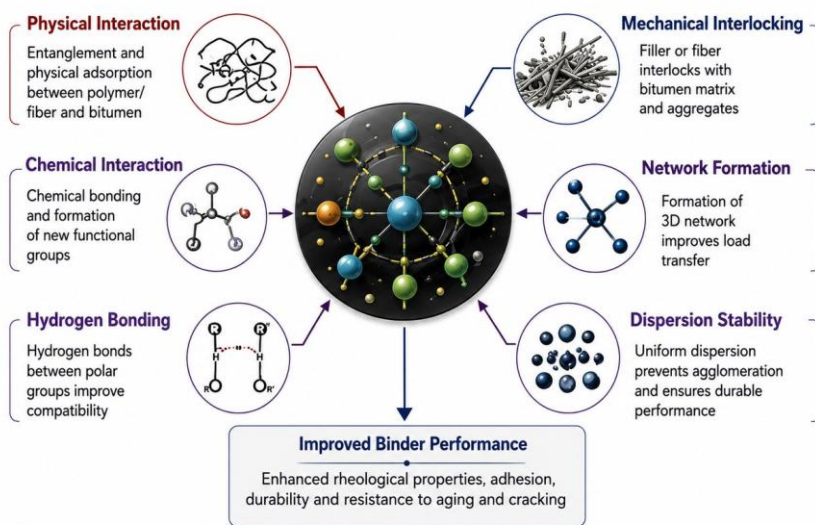


Figure 2.4. Interaction mechanisms between functional modifiers and the bituminous matrix, physical and chemical bonding, mechanical interlocking, network formation, hydrogen bonding and dispersion, that together set binder performance.

Crumb rubber interacts through a related but distinct two-way mechanism of diffusion and partial digestion. In the wet process, rubber particles immersed in hot bitumen absorb aromatic oils and swell, increasing the viscosity and elasticity of the

surrounding binder, while at the same time devulcanised and depolymerised rubber constituents diffuse outward into the bitumen. The resulting binder is a composite of swollen residual rubber particles suspended in an oil-depleted, stiffened bitumen phase. The extent of this interaction depends on temperature, residence time, rubber particle size, and shear, and it directly controls the balance between beneficial elasticity and detrimental phase instability (Joohari & Giustozzi, 2022). This interplay explains why crumb-rubber binders demand careful attention to storage and agitation and why hybridisation with polymers is often adopted to consolidate the network.

Fibers interact with the mixture through an entirely different, mechanical mechanism that operates at the scale of the mastic and aggregate skeleton rather than the binder molecules. Discrete fibers such as basalt disperse within the mixture to form a three-dimensional spatial network that performs three coupled functions: adsorption and stabilisation of the binder, which reduces drain-down and thickens the effective mastic; bridging of microcracks, whereby fibers spanning an incipient crack carry tensile stress across it and dissipate fracture energy; and stress redistribution, which prevents local stress concentrations from nucleating macrocracks (Men et al., 2022; Wu et al., 2022). The effectiveness of this reinforcement depends on fiber length, diameter, dosage, dispersion uniformity, and, critically, the adhesion at the fiber–bitumen interface; surface treatment of fibers to improve this bond is an active area of refinement. Because the mechanism is mechanical and interfacial rather than rheological, fibers improve toughness and crack resistance with comparatively little change to the intrinsic temperature susceptibility of the binder (Wu et al., 2022).

Nanomaterials interact predominantly through interfacial and adsorption phenomena that are amplified by their enormous specific surface area. Because a gram of well-dispersed nanoparticles

presents an interfacial area orders of magnitude greater than that of conventional fillers, even dosages of one to five per cent by binder mass can materially alter behaviour. Nano-silica adsorbs the light maltene fractions onto its surface, restraining their mobility, increasing viscosity and stiffness, and thereby enhancing rutting resistance; the same adsorption reduces the availability of oxidisable light fractions and, together with a physical barrier effect, improves ageing resistance (Cheraghian et al., 2021; Huang et al., 2024). Layered and planar nanomaterials such as graphene and graphene nanoplatelets act partly through this interfacial stiffening and partly through a tortuosity mechanism, in which the impermeable nanosheets lengthen the diffusion path of oxygen and volatiles and so retard oxidative hardening (Almashaqbeh et al., 2024). The decisive variable in all nanomaterial interactions is the state of dispersion: nanoparticles possess a strong thermodynamic tendency to agglomerate, and agglomerates behave as stress-concentrating defects rather than reinforcing phases. Achieving and preserving uniform dispersion, through high-shear mixing, sonication, or surface functionalisation, is therefore the central challenge that determines whether the theoretical promise of nanomodification is realised in practice (Huang et al., 2024).

Table 2.2. *Interaction mechanisms between modifiers and the bituminous matrix*

Mechanism	Description	Typical materials
Physical network	Percolating reinforcing scaffold	Nanomaterials, fibres
Swelling, phase network	Polymer absorbs light maltenes	SBS, SBR
Chemical bonding	Covalent, reactive linkage	Reactive polymers, graphene oxide
Adsorption, H-bonding	Polar surface interaction	Nano-silica, metal oxides

Mechanism	Description	Typical materials
Barrier effect	Tortuous O ₂ , UV diffusion path	Clay, graphene, TiO ₂

Smart and multifunctional materials rely on interaction mechanisms that couple the physical response of an embedded phase to an external or internal stimulus. In induction-based self-healing, electrically conductive particles or fibers embedded in the mastic absorb energy from an alternating electromagnetic field and heat rapidly; the surrounding bitumen softens, its viscosity drops, and capillary flow draws the softened binder into microcracks to reunite the fracture faces, restoring a substantial fraction of the original strength (Anupam et al., 2022). In capsule-based self-healing the interaction is chemomechanical: microcapsules dispersed in the binder remain inert until the stress field at a propagating crack tip ruptures their shells, whereupon an encapsulated rejuvenator is released and diffuses into the aged, crack-adjacent bitumen, restoring maltene balance and mobility so that the crack can close (Sun et al., 2017). Phase-change materials interact thermally rather than mechanically, absorbing latent heat as they melt during heating and releasing it as they solidify during cooling, thereby buffering the pavement temperature within the phase-transition range provided that leakage of the molten phase is prevented by encapsulation or supporting frameworks (Wang et al., 2023). Self-sensing composites interact electromechanically through the piezoresistive effect: a percolating network of conductive carbon nanotubes or fibers within the composite deforms under mechanical load, altering the contact and tunnelling conduction between adjacent particles and producing a measurable change in electrical resistance proportional to strain (Xin et al., 2020; Birgin et al., 2022; Wang, Faßbender, et al., 2023).

Across these diverse mechanisms, several unifying principles emerge that recur throughout the chapter. First, the interface, whether polymer–bitumen, rubber–bitumen, fiber–bitumen, or nanoparticle–bitumen, is almost always the locus that governs both benefit and failure, and interfacial compatibility and adhesion are the pervasive determinants of durability. Second, dispersion and morphological continuity of the introduced phase are as important as its intrinsic properties, because a poorly dispersed or discontinuous modifier delivers a fraction of its potential and may act as a defect. Third, the mobility of the maltene fractions is a shared currency: polymers and rubber compete for it, nanomaterials restrain it, rejuvenators replenish it, and ageing depletes it. Recognising these common threads allows the engineer to reason about unfamiliar materials by analogy and provides the mechanistic foundation for the selection criteria and trade-offs analysed in the final section.

Selection Criteria, Opportunities and Limitations

The selection of a functional material for a flexible pavement is a multi-criteria decision in which technical performance, constructability, cost, environmental impact, and long-term durability must be weighed simultaneously and often against one another. No single material is optimal across all dimensions, and the appropriate choice is invariably contingent on the climate, traffic, materials availability, and sustainability objectives of the specific project. A rational selection framework therefore begins not with the material but with a clear definition of the distress mechanisms and functional requirements the pavement must satisfy, and only then identifies the material family whose interaction mechanism addresses those requirements most efficiently. Figure 2.5 relates the functional materials to the roles they play across the individual pavement layers, and Figure 2.6 sets out the overall development workflow from material selection to a sustainable flexible pavement.

The foremost selection criterion is technical performance across the relevant temperature and loading spectrum. A binder modifier intended for a hot climate with heavy, channelised traffic must demonstrably raise the high-temperature stiffness and elastic recovery to resist permanent deformation, whereas a modifier for a cold region must preserve low-temperature flexibility to resist thermal cracking, and a modifier for a fatigue-critical structure must enhance the binder's capacity to dissipate strain energy without damage. Polymer modification with SBS remains the benchmark precisely because it improves all three simultaneously by broadening the useful temperature interval, and its performance is well documented and specifiable (Yang et al., 2024). Nanomaterials offer a complementary route, delivering stiffening and ageing resistance at low dosage, but their benefits are realised only when dispersion is controlled and are therefore more sensitive to production quality (Cheraghian et al., 2021; Huang et al., 2024). Fibers are selected when cracking, fatigue, and toughness rather than binder rheology are the governing concerns, and are particularly effective in stone-mastic and thin-surfacing applications where drain-down control and crack bridging are valued (Men et al., 2022; Wu et al., 2022).

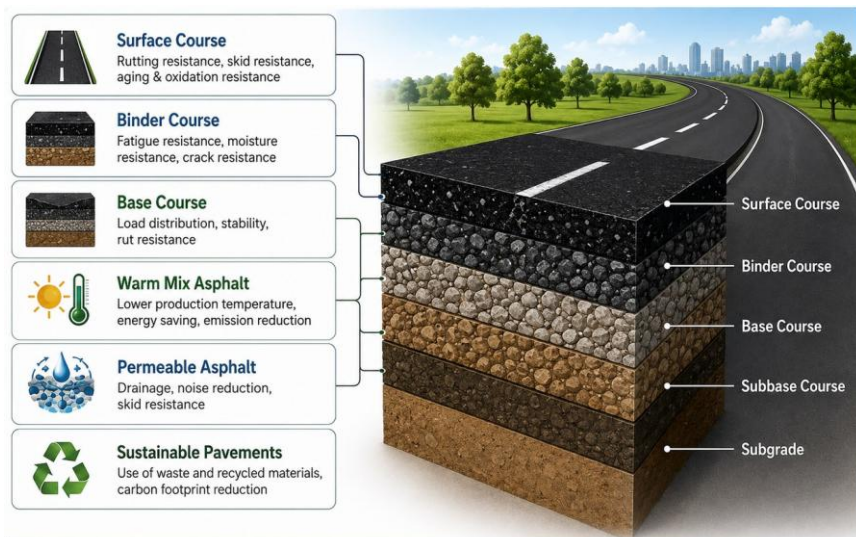


Figure 2.5. *Functional roles of materials across the individual pavement layers, from the wearing surface down to the subgrade, showing where each property is required.*

A second and increasingly decisive criterion is sustainability, assessed over the full life cycle rather than at the point of production alone. Warm-mix additives offer clear and quantifiable opportunities here, lowering production temperatures and the associated energy demand and emissions while improving working conditions and enabling higher recycled-content mixtures; systematic reviews consistently report meaningful reductions in fuel consumption and greenhouse-gas emissions relative to hot-mix asphalt at comparable performance (Rubio et al., 2012; Tutu & Tuffour, 2016; Ahmed & Baig, 2026). Waste-derived materials, above all crumb rubber, provide a dual sustainability benefit by diverting end-of-life tyres from disposal while enhancing binder elasticity and fatigue resistance (Joohari & Giustozzi, 2022). Thermoregulating phase-change materials extend the sustainability rationale to the operational phase, mitigating temperature-induced distress and the urban heat-island effect over the service life of the pavement (Wang

et al., 2023). The opportunity common to these materials is that functionality and environmental benefit reinforce rather than oppose one another, which is a powerful argument for their adoption.

Against these opportunities stand real and material limitations that temper enthusiasm and shape practical deployment. Storage stability and compatibility remain the principal limitation of polymer- and rubber-modified binders, which can undergo phase separation during high-temperature storage and transport, degrading the very properties they were introduced to improve and demanding continuous agitation or compatibilising additives (Wang et al., 2021; Joohari & Giustozzi, 2022). For nanomaterials, the dominant limitations are the strong tendency toward agglomeration, the relatively high cost of well-characterised nanoparticles, uncertainties surrounding occupational and environmental health during handling, and the scarcity of long-term field validation, all of which constrain the translation of impressive laboratory results into routine practice (Huang et al., 2024; Almashaqbeh et al., 2024). Fibers introduce their own constraints, including the risk of clumping and non-uniform dispersion, the need for adequate fiber-bitumen adhesion, and sensitivity of the outcome to dosage and length, since excessive dosing can impair workability and compaction (Men et al., 2022). Warm-mix technologies, for their part, can under some conditions reduce moisture resistance or, in the case of certain organic additives, exhibit variable effects on mechanical performance, so that additive type and dosage must be matched carefully to the mixture and climate (Belc et al., 2021).

The limitations of the smart and multifunctional materials are more fundamental still, reflecting their earlier stage of maturity. Self-healing systems face the challenge of ensuring that induction or microwave heating is applied at appropriate intervals without overheating and ageing the binder, and that microcapsules survive the aggressive mixing and compaction process intact yet rupture

reliably under service cracking; the durability of the capsule shell, the volume fraction that can be incorporated without weakening the mixture, and the repeatability of healing over multiple cycles all remain active research questions (Anupam et al., 2022; Sun et al., 2017). Phase-change materials must overcome leakage of the molten phase, potential softening of the mixture, and limited latent-heat capacity per unit volume, which constrain the magnitude and duration of the thermoregulating effect (Wang et al., 2023). Self-sensing composites require a stable, reproducible percolating conductive network, robust electrode integration, and signal-processing schemes that separate the strain response from confounding effects of temperature and moisture, and their field durability under traffic and environmental cycling is only beginning to be demonstrated (Xin et al., 2020; Birgin et al., 2022; Wang, Faßbender, et al., 2023). Across all smart systems, cost and scalability are recurrent obstacles, and the incremental benefit must be justified against a full life-cycle analysis rather than against first cost alone.

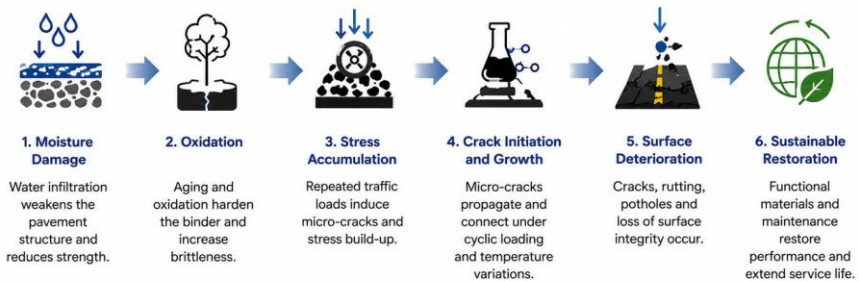


Figure 2.6. Development workflow linking functional-material selection to binder modification, mixture design, performance evaluation and field implementation of a sustainable pavement.

Balancing these opportunities and limitations requires an explicit weighing of trade-offs that is best conducted within a

performance-based and life-cycle-oriented framework. A material that delivers a superior laboratory property but cannot be stored, dispersed, or produced reliably at scale may be inferior in practice to a more modest but robust alternative. Conversely, a material whose first cost is higher may be justified where it extends service life, reduces maintenance frequency, or lowers cumulative energy and emissions. Increasingly, hybrid strategies that combine complementary materials, polymers with crumb rubber for stabilised elasticity, fibers with modified binders for coupled toughness and rheology, or conductive nanomaterials that simultaneously reinforce and sense, offer a route to reconcile competing objectives, though they add complexity to mixture design and quality control (Joohari & Giustozzi, 2022; Xin et al., 2020).

In summary, the selection of functional materials for sustainable flexible pavements is neither a search for a universal solution nor a simple ranking of additives, but a context-dependent optimisation across performance, constructability, cost, durability, and environmental impact. Conventional polymer and rubber modifiers remain indispensable workhorses whose limitations are well understood and increasingly well managed; nanomaterials and fibers offer targeted enhancements whose realisation depends on dispersion and quality control; and smart materials hold transformative promise that is currently constrained by cost, scalability, and the need for long-term field validation. The chapters that follow examine each of these families in greater depth, but the organising principles established here, function-oriented classification, mechanism-based understanding, and multi-criteria, life-cycle-informed selection, provide the framework within which their specific contributions to sustainable pavement engineering should be evaluated.

AUTHOR'S PERSPECTIVE

When I select a functional material I start from the governing distress and the compatibility window, not from the novelty of the additive. An elastomer that separates in storage, or a nanomaterial that will not disperse at plant shear, is worse than no modifier at all. My rule of thumb is to change one property deliberately, verify that the others have not been sacrificed, and only then consider stacking a second additive; multifunctionality earned by careful pairing is durable, multifunctionality assumed from a datasheet is not.

CHAPTER SUMMARY

Chapter 2 mapped the functional-material landscape into five families, traced the evolution from passive fillers to active, responsive systems, and set out the interaction mechanisms and selection criteria that govern their use.

Key findings

- ▶ Functional materials fall into rheology modifiers, processing/sustainability additives, reinforcing fibres, nanomaterials and smart systems.
- ▶ Modifiers act through physical networks, phase swelling, chemical bonding, adsorption and barrier effects.
- ▶ The field is moving from materials that endure the environment to materials that actively engage with it.

Design recommendations

- ▶ Choose the modifier from the governing distress and the compatibility window, not the datasheet.
- ▶ Verify storage stability and dispersibility at plant-representative shear.
- ▶ Justify each added function against a full life-cycle rather than first cost.

Future research

- ▶ Reliable, field-durable smart and self-sensing systems.
- ▶ Design tools that predict multifunctional trade-offs before deployment.

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CHAPTER 3

Nanomaterials for Bitumen Modification: Types, Properties and Mechanisms

Nanoscale Materials: An Introduction

The pursuit of durable, sustainable flexible pavements has increasingly turned attention toward the manipulation of bituminous binders at the nanoscale. Bitumen is a colloidal, viscoelastic material whose field performance is governed by phenomena that originate at molecular and supramolecular length scales: the association of asphaltene aggregates, the mobility of maltene fractions, oxidative bond formation, and the development of interfacial adhesion with mineral aggregate. Because conventional modifiers such as elastomeric and plastomeric polymers act primarily at the micron scale, they cannot fully arrest the sub-micron processes that drive rutting, fatigue cracking, thermal cracking, moisture damage, and age hardening. Nanomaterials, defined broadly as materials possessing at least one external dimension below approximately 100 nm, offer an exceptionally high specific surface area, a large density of reactive surface sites, and the capacity to reinforce the binder

matrix at length scales commensurate with those of the binder's own colloidal architecture (Afshin & Behnood, 2025; Iftikhar et al., 2023). It is this dimensional compatibility, rather than sheer novelty, that motivates their use as functional additives for sustainable pavements, since even small dosages can produce disproportionately large changes in binder behaviour. Figure 3.1 presents the principal nanomaterials used for bitumen modification together with the advantages that motivate their use, and Figure 3.2 organises the field into a classification by dimensionality, composition and origin.

Nano-silica (nano-SiO₂) is among the most widely investigated nanomaterials for bitumen because it is abundant, comparatively inexpensive, chemically stable, and available in both hydrophilic and hydrophobic (surface-treated) grades. Its modification action is dominated by the free silanol (Si–OH) hydroxyl groups distributed across its surface, which are able to form hydrogen bonds with the polar, heteroatom-bearing components of bitumen and thereby knit a three-dimensional spatial network throughout the maltene phase (Dai et al., 2023). Fumed silica, produced by flame hydrolysis, is a particularly effective sub-class: its branched, chain-like aggregate morphology readily develops a percolating network within the binder that enhances elasticity and stiffens the matrix at high service temperatures, while simultaneously screening the binder against thermo-oxidative and ultraviolet degradation (Zhou et al., 2023; Cheraghian & Wistuba, 2021). The economic attractiveness of fumed silica, reported to cost roughly a tenth of conventional precipitated nano-SiO₂, reinforces its relevance to cost-conscious, sustainability-oriented pavement engineering (Zhou et al., 2023).

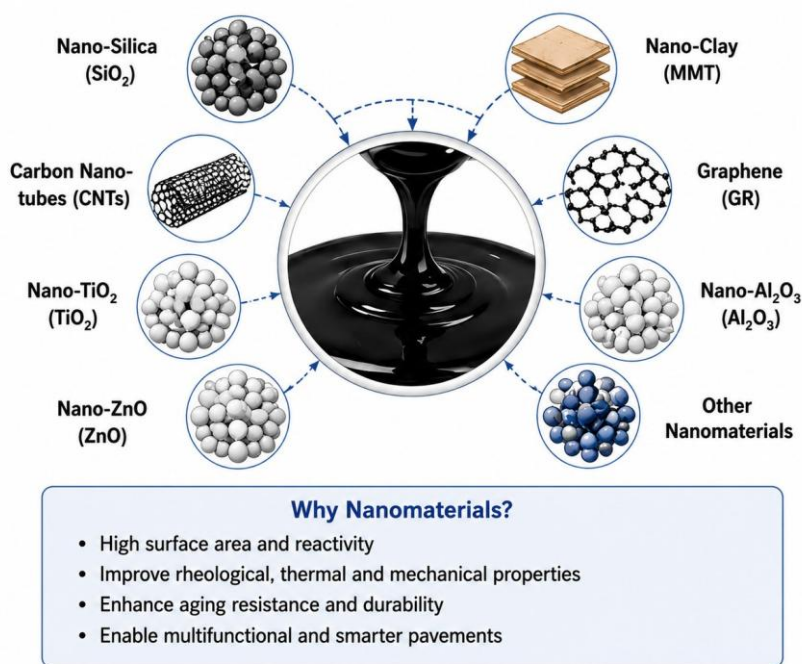
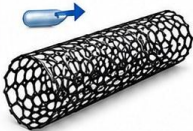
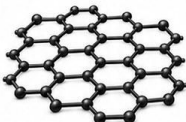
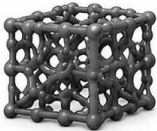


Figure 3.1. *Principal nanomaterials used to modify bitumen, nano-silica, nano-clay, carbon nanotubes, graphene and metal oxides, and the high-surface-area advantages that motivate their use.*

Nano-clays, principally montmorillonite (MMT) and its organically modified derivatives (OMMT), constitute a second major family. These are layered aluminosilicate (phyllosilicate) minerals whose platelets are only about one nanometre thick but hundreds of nanometres across, giving very high aspect ratios. Their effectiveness hinges on how the bitumen fractions interact with the interlayer galleries: when binder molecules diffuse between the silicate sheets, the stacked structure transforms into intercalated or, more favourably, exfoliated morphologies in which individual platelets are dispersed throughout the matrix (Ren et al., 2020; Cheng et al., 2021). Organic surfactant treatment enlarges the

interlayer spacing, improves organophilic compatibility, and promotes the exfoliation that maximises the tortuosity of diffusion paths for oxygen and volatile species. Nano-clays are therefore valued not only for stiffening and rutting resistance but also, importantly, for enhancing the storage stability and ageing resistance of polymer-modified binders (Ren et al., 2020).

By Dimensionality

0D (Zero-Dimensional)	1D (One-Dimensional)	2D (Two-Dimensional)	3D (Three-Dimensional)
- Nano particles - Quantum dots 	- CNTs - Nanofibers - Nanorods 	- Graphene - Graphene oxide - Nanosheets 	- Nanoframes - Nanostructured networks 

By Composition

Oxides	Carbon-based	Layered Silicates	Others
SiO_2 TiO_2 Al_2O_3 ZnO Fe_2O_3 	- Graphene - CNTs - Carbon black - Fullerenes 	- Montmorillonite (MMT) - Halloysite - Sepiolite 	- Metals (Ag, Cu) - Metal oxides - Hybrid nanomaterials 

By Origin

Natural - Nano-clay - Nano-silica 	Engineered - Synthesized nanoparticles - Functionalised nanoparticles 
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Figure 3.2. *Classification of nanomaterials by dimensionality (0D to 3D), chemical composition and origin, providing a map of the available design space.*

Carbon-based nanomaterials represent a third and increasingly prominent category, encompassing carbon nanotubes (CNTs), graphene, and graphene oxide (GO). Carbon nanotubes, cylindrical graphitic structures available as single-walled or multi-walled variants, possess extraordinary tensile strength and stiffness together with very high aspect ratios, enabling them to act as nanoscale fibres that bridge microcracks and reinforce the binder's cohesive strength (Wang et al., 2021; Liang et al., 2020). Graphene, a two-dimensional monolayer of sp²-hybridised carbon, and its industrially convenient forms, graphene nanoplatelets (GNPs) and graphene oxide, provide sheet-like reinforcement with immense specific surface area. Their planar geometry allows them to impede oxygen diffusion, distribute stresses, and improve the performance grade of the binder while lowering its thermal susceptibility (Polo-Mendoza et al., 2023). Graphene oxide is distinguished by oxygen-containing functional groups (hydroxyl, epoxy, carboxyl) that improve its dispersibility and enable stronger chemical interaction with polar binder constituents, whereas pristine graphene and GNPs interact predominantly through physical and π -associative mechanisms (Wang et al., 2021). Collectively, carbon nanomaterials have been shown to enhance complex modulus, elastic recovery, fatigue life, and resistance to permanent deformation, and they are frequently deployed in combination with styrene–butadiene–styrene (SBS) or recycled polyethylene to obtain synergistic composites (Wang et al., 2021; Yu et al., 2021).

Metal-oxide nanoparticles, chiefly nano-titanium dioxide (nano-TiO₂) and nano-zinc oxide (nano-ZnO), form a fourth family whose distinguishing attribute is photoactivity. Both oxides are efficient absorbers of ultraviolet radiation and possess

semiconducting, photocatalytic character, which makes them especially suited to mitigating the UV-driven photo-oxidative ageing that plagues surface courses in high-insolation climates (Lima et al., 2022; Zhang et al., 2021). Nano-TiO₂ exhibits strong absorption near the 365 nm band and has been reported to inhibit the ageing-related increase of asphaltenes and the depletion of lighter fractions, thereby stabilising the binder's chemistry and preserving its rheology (Liao et al., 2021; Yang et al., 2022). Nano-ZnO offers comparable UV-shielding and anti-ageing benefits and can additionally contribute to rutting resistance and elastic recovery (Iftikhar et al., 2023). Beyond durability, both oxides confer functional surface attributes, self-cleaning and pollutant-degrading photocatalysis, that align with the multifunctional aspirations of sustainable pavement design, although optimum dosages are typically low (often below 1% by mass of binder) because excessive loadings promote agglomeration and diminishing returns (Lima et al., 2022).

Table 3.1. *Principal nanomaterial families for bitumen modification*

Material	Dimensionality	Main effect
Nano-silica (SiO ₂)	0D spheres	Stiffening, ageing resistance
Nano-clay (montmorillonite)	2D platelets	Barrier, storage stability
Carbon nanotubes	1D tubes	Crack bridging, fatigue life
Graphene / graphene oxide	2D sheets	Modulus, barrier, PG grade
Nano-TiO ₂ / ZnO	0D oxides	UV shielding, photocatalysis

Across all four families, several unifying themes emerge that frame the remainder of this chapter. First, the benefit of a nanomaterial is realised only if it can be dispersed to a near-primary-

particle state and kept stable against re-agglomeration and settlement during storage, a challenge magnified precisely by the high surface energy that makes nanomaterials attractive (Huang et al., 2024). Second, the mechanisms of modification are simultaneously physical (network formation, reinforcement, barrier effects) and physicochemical (hydrogen bonding, polar adsorption, and, in the case of GO and metal oxides, more specific surface interactions), and they express themselves in measurable microstructural changes (Cheraghian et al., 2022). Third, the ultimate justification lies in field-relevant performance: improved high-temperature stiffness and rutting resistance, preserved or enhanced fatigue and low-temperature behaviour, better moisture resistance, and slower ageing (Alam et al., 2024). The following sections address these dimensions in turn, beginning with the practical prerequisite of dispersion, compatibility, and storage stability.

Dispersion, Compatibility and Storage Stability

The single most decisive factor separating a beneficial nanomodification from a disappointing one is the quality of dispersion. The very attribute that endows nanomaterials with their potency, an enormous surface-area-to-volume ratio, also renders them thermodynamically prone to self-association. Strong van der Waals attraction, and, for hydrophilic surfaces, extensive hydrogen bonding, drive primary nanoparticles to agglomerate into micron-scale clusters that behave essentially as inert filler or, worse, as stress-concentrating flaws. When agglomeration prevails, the reinforcing network cannot percolate, the interfacial contact area with the binder collapses, and much of the anticipated improvement in rutting resistance, fatigue life, and ageing resistance is forfeited (Huang et al., 2024; Liang et al., 2020). Achieving and preserving a fine, homogeneous distribution of nanoparticles is therefore not an incidental processing detail but a central engineering requirement.

Figure 3.3 depicts the dispersion process, the stabilization mechanisms that keep nanoparticles apart, and the key factors that govern their distribution in bitumen, while Figure 3.4 sets out the corresponding laboratory route for preparing a nanomodified binder.

Two broad and complementary strategies are used to promote dispersion: energetic mechanical blending and chemical surface engineering. On the mechanical side, high-shear mixing is the workhorse of laboratory and plant practice, its rotor–stator geometry generating the shear gradients needed to break down agglomerates, while ultrasonication is frequently applied, alone or in combination with shear, to deliver localised cavitation energy that separates strongly bonded clusters (Cheraghian et al., 2022). Processing variables such as shear rate, mixing time, and temperature must be optimised jointly, because insufficient energy leaves agglomerates intact whereas excessive temperature or duration can accelerate binder ageing and degrade heat-sensitive surface treatments. On the chemical side, surface functionalisation modifies the interfacial energetics so that the nanoparticle becomes more compatible, more nearly "wetted", by the organic binder. The organic modification of montmorillonite with quaternary ammonium surfactants is the archetypal example: by exchanging inorganic interlayer cations for bulky organic ions, the gallery spacing is enlarged and the platelet surfaces are rendered organophilic, so that bitumen molecules can penetrate, intercalate, and ultimately exfoliate the clay stacks (Ren et al., 2020; Cheng et al., 2021). Analogous logic applies to silica, where hydrophobic (silane-treated) grades disperse more readily in the non-polar maltene phase than untreated hydrophilic grades, and to carbon nanomaterials, where oxidation to graphene oxide or covalent/non-covalent functionalisation of nanotubes improves both dispersibility and interfacial bonding (Wang et al., 2021; Dai et al., 2023).

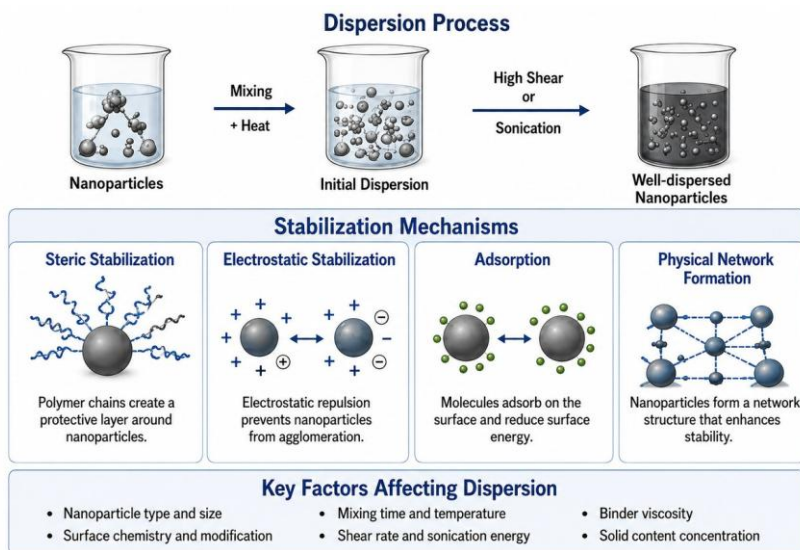


Figure 3.3. Dispersion process for nanoparticles in bitumen, the stabilization mechanisms (steric, electrostatic, adsorption and network formation) that keep them apart, and the key factors controlling the final distribution.

Compatibility, the thermodynamic and kinetic tendency of the nanophase and the binder to remain intimately intermixed rather than to phase-separate, is intimately linked to, but distinct from, initial dispersion quality. A binder may be dispersed well immediately after mixing yet prove incompatible over time if the density mismatch between the nanophase and the surrounding bitumen, together with the low viscosity of the binder at storage temperatures, permits the particles to migrate. Compatibility is enhanced when strong, favourable interfacial interactions, hydrogen bonds between silanol groups and binder heteroatoms, polar adsorption of asphaltenes onto metal-oxide surfaces, or π -associative contacts with graphitic surfaces, anchor the nanoparticles within the matrix and raise the energetic penalty of separation (Dai et al., 2023; Cheraghian et al., 2022). Molecular dynamics simulations have

proved especially valuable in quantifying these interfacial interactions, showing, for example, that carbon nanotubes can strengthen the adhesion between a dispersed polymer phase (such as recycled polyethylene) and the base asphalt by increasing the interfacial binding energy, thereby improving the compatibility of otherwise poorly miscible systems (Yu et al., 2021).



Figure 3.4. Laboratory route for preparing a nanomodified bitumen, from drying and pre-dispersion through high-shear mixing and sonication to curing and storage.

Storage stability is the practical manifestation of compatibility under the conditions the binder actually encounters between production and placement: prolonged holding in hot tanks, typically at temperatures of 160–180 °C, often without continuous agitation. Under these conditions a poorly stabilised system undergoes phase separation, dense nanoparticles settle while lighter polymer-rich phases cream, producing vertical gradients in composition and properties that compromise uniformity and field performance. Stability is conventionally quantified by the hot-storage tube (cigar) test, in which a binder sample is held vertically at elevated temperature for a fixed period and the softening-point (or rheological) difference between the top and bottom segments is

measured; a small differential indicates good stability (Ren et al., 2020). A distinctive and much-cited advantage of nanomaterials is their ability to improve high-temperature storage stability, in contrast to many neat polymer-modified binders whose polymer and asphalt phases tend to separate on standing. Layered nano-montmorillonite is particularly effective in this role: upon intercalation and exfoliation it distributes high-aspect-ratio platelets throughout the binder that physically obstruct the migration and coalescence of polymer domains, markedly reducing the top-to-bottom property differential of crumb-rubber, SBR, and SBS-modified binders (Ren et al., 2020). The magnitude of benefit is system-specific; the same investigations report pronounced stabilisation of crumb-rubber-modified binders but more limited effects for certain SBS systems, underscoring that stabilisation depends on the specific chemistry and morphology of both the nanoclay and the host polymer (Ren et al., 2020).

The verification of dispersion and compatibility relies on a suite of microscopic and spectroscopic techniques. Scanning electron microscopy and transmission electron microscopy visualise agglomerate size and spatial distribution; X-ray diffraction is indispensable for distinguishing intercalated from exfoliated clay morphologies, since the characteristic basal-spacing reflection shifts or disappears as the galleries expand and the platelets delaminate (Cheng et al., 2021). Fluorescence microscopy reveals polymer-phase continuity, and atomic force microscopy (AFM) has become a particularly powerful tool for probing the nanoscale phase structure and micromechanical properties of modified binders, mapping the topographic and mechanical heterogeneity, including the well-known "bee" structures, at resolutions inaccessible to bulk tests (Ouyang et al., 2022). Together these methods allow the engineer to confirm that a chosen combination of mixing protocol and surface chemistry has produced the fine, stable, well-anchored dispersion on

which every subsequent performance benefit ultimately depends (Huang et al., 2024). In practice, the optimisation of dosage is inseparable from dispersion: because agglomeration intensifies as concentration rises, most studies identify a relatively low optimum content, commonly in the range of a few tenths of a percent up to a few percent by mass of binder, beyond which further additions yield diminishing or even negative returns as clustering overtakes reinforcement (Cheraghian et al., 2022; Lima et al., 2022).

Modification Mechanisms and Microstructural Effects

The performance changes wrought by nanomaterials arise from a family of interrelated mechanisms operating on the binder's colloidal and molecular structure. It is useful to organise these into four categories, physical network formation and reinforcement, physicochemical surface interaction, barrier and adsorption effects governing ageing, and modification of the colloidal balance, recognising that in any real system they act in concert and that their relative importance depends on the nanomaterial's geometry, surface chemistry, and dosage (Cheraghian et al., 2022; Afshin & Behnood, 2025). Figure 3.5 illustrates the surface interactions between a nanoparticle and the bitumen fractions and their consequences for the binder microstructure.

The most general mechanism is the formation of a spatial reinforcing network. When well dispersed, high-surface-area nanoparticles establish a percolating, three-dimensional scaffold that pervades the maltene phase and immobilises binder molecules within its interstices. For nano-silica, this network is stabilised by hydrogen bonding between surface silanol groups and the polar functionalities of the binder, producing a structure that increases stiffness and elasticity, especially at high temperatures where the neat binder would otherwise flow (Dai et al., 2023). Fumed silica, by virtue of its branched aggregate morphology, forms such a

network with particular readiness, so that even modest loadings noticeably raise the binder's elastic response and restore it after loading (Zhou et al., 2023). For one- and two-dimensional carbon nanomaterials, the geometry of reinforcement differs but the principle is the same: carbon nanotubes act as nanoscale fibres that bridge incipient microcracks and carry tensile load, while graphene nanoplatelets and graphene oxide act as stiff sheets that distribute stress over large interfacial areas and constrain the mobility of surrounding molecules (Polo-Mendoza et al., 2023; Wang et al., 2021). Layered silicates contribute reinforcement in proportion to their degree of exfoliation, the delaminated high-aspect-ratio platelets providing extensive load-bearing interfaces throughout the matrix (Cheng et al., 2021).

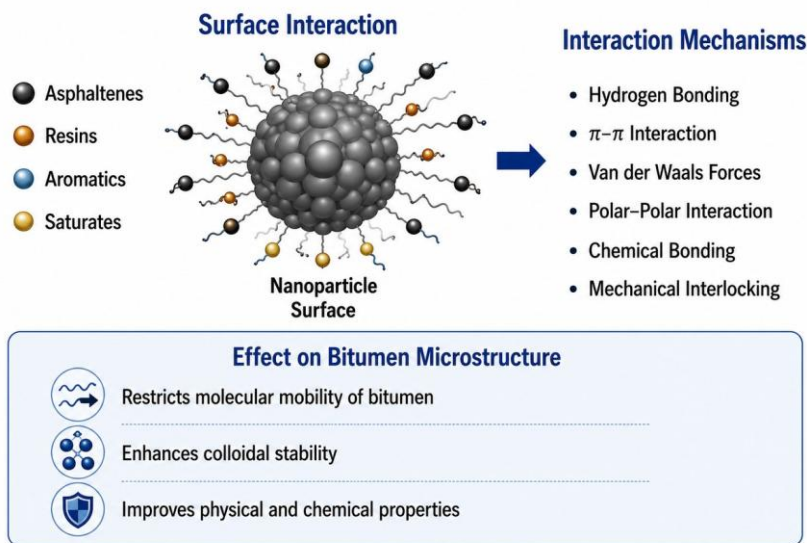


Figure 3.5. Nanoparticle–bitumen surface interactions, hydrogen bonding, π – π and van der Waals forces and chemical bonding, and their consequences for the binder microstructure.

The physicochemical dimension of modification concerns the specific interactions established at the nanoparticle–binder interface, which determine both the strength of the reinforcing network and the compatibility discussed earlier. Spectroscopic evidence, principally from Fourier-transform infrared (FTIR) analysis, indicates that many effective nanomodifications proceed predominantly through physical association, hydrogen bonding, polar adsorption, and van der Waals and π -associative contacts, rather than the formation of new covalent bonds, so that the characteristic functional-group signatures of the binder are broadly preserved while their environment is perturbed (Lima et al., 2022; Wang et al., 2021). Nano-silica's silanol groups interact with the carbonyl, sulfoxide, and aromatic moieties of the binder; graphene oxide's oxygenated groups engage polar asphaltene constituents; and metal-oxide surfaces adsorb polar species onto their high-energy faces. The strength of these interactions can be interrogated at the nanoscale by AFM, which reveals how nanomodification alters adhesion forces, energy dissipation, and the size and distribution of the phase domains that constitute the binder's microstructure (Ouyang et al., 2022).

Table 3.2. Modification mechanisms and their effect on binder behaviour

Mechanism	Effect on binder
Network reinforcement	Higher stiffness, elasticity and rutting resistance
Physicochemical adsorption	Anchoring of particles; improved compatibility
Barrier, UV absorption	Slower oxidative and photo-ageing
Colloidal rebalancing	More structured, gel-like response

A mechanism of special importance for sustainability is the retardation of ageing, which nanomaterials achieve through complementary barrier and adsorption effects. Oxidative ageing, the progressive conversion of maltenes to resins and asphaltenes through the formation of carbonyl and sulfoxide groups, is diffusion-limited, depending on the ingress of atmospheric oxygen into the binder film. Two-dimensional nanomaterials are geometrically ideal oxygen barriers: dispersed graphene and clay platelets create a tortuous, labyrinthine path that lengthens the effective diffusion distance for oxygen and volatile species, slowing the rate of oxidation (Wang et al., 2021; Ren et al., 2020). Metal-oxide nanoparticles combat a different but related pathway. Nano-TiO₂ and nano-ZnO absorb and scatter ultraviolet radiation, shielding the binder from the photochemical energy that initiates photo-oxidation; nano-TiO₂ in particular shows strong absorption in the ultraviolet region and has been shown to suppress the ageing-related build-up of asphaltenes and loss of lighter fractions, keeping the binder chemically and rheologically more stable through rolling-thin-film-oven and pressure-ageing-vessel conditioning (Lima et al., 2022; Yang et al., 2022). Composite systems that couple a UV-absorbing oxide with a barrier-forming clay, such as nano-TiO₂/montmorillonite blends, exploit both effects simultaneously and have been reported to deliver superior resistance to UV ageing than either component alone (Liao et al., 2021). The net microstructural consequence is a binder whose colloidal index and molecular-size distribution drift far less during service, translating directly into extended pavement life and reduced maintenance frequency (Zhang et al., 2021).

Underlying all of these is the mechanism of colloidal rebalancing. Bitumen can be understood as a dispersion whose stability depends on the ratio of peptising resins and aromatics to flocculating asphaltenes and saturates. By adsorbing polar asphaltenes onto their surfaces and by templating the arrangement of

surrounding molecules, nanoparticles alter this balance, in effect increasing the structured, gel-like character of the binder. This restructuring is what AFM observes as changes in phase morphology and what rheometry registers as increased complex modulus and elasticity (Ouyang et al., 2022; Cheraghian et al., 2022). It also explains why the same nanomaterial can improve several ostensibly independent properties at once: a more structured colloid resists permanent deformation at high temperature, recovers elastically under repeated loading, and presents a more oxidation-resistant architecture. The corollary, however, is that over-structuring, driven by excessive dosage or by agglomeration, can embrittle the binder and impair its low-temperature relaxation capacity, which is why mechanism-informed dosage optimisation is essential and why the microstructural techniques described in Section 3.2 are integral to, rather than separate from, the understanding of how nanomaterials work (Huang et al., 2024; Iftikhar et al., 2023).

Effects on Rheological and Mechanical Performance

The mechanisms outlined above express themselves, at the scale of engineering practice, as measurable changes in the rheological and mechanical response of the binder and the mixtures made from it. The most consistently reported effect of nanomodification is an increase in viscosity and complex shear modulus accompanied by a decrease in phase angle, signifying a stiffer, more elastic binder. A comprehensive review of viscosity behaviour concludes that, across the major nanomaterial families, the addition of nanoparticles generally raises the binder's viscosity, enhancing its resistance to high-temperature rutting while remaining, at optimum dosage, within the bounds of workability required for mixing and compaction (Huang et al., 2024). This stiffening is the direct rheological signature of the reinforcing network and colloidal restructuring described in Section 3.3, and it underpins most of the

high-temperature performance benefits that follow. Figure 3.6 summarises the effects of nanomaterial modification on the rheological, thermal, mechanical and ageing properties of the binder and the resulting benefits; Figure 3.7 gathers the principal techniques used to characterise nanomodified binders; and Figure 3.8 sets out the remaining challenges and the future perspectives for nanomaterials in pavement engineering.

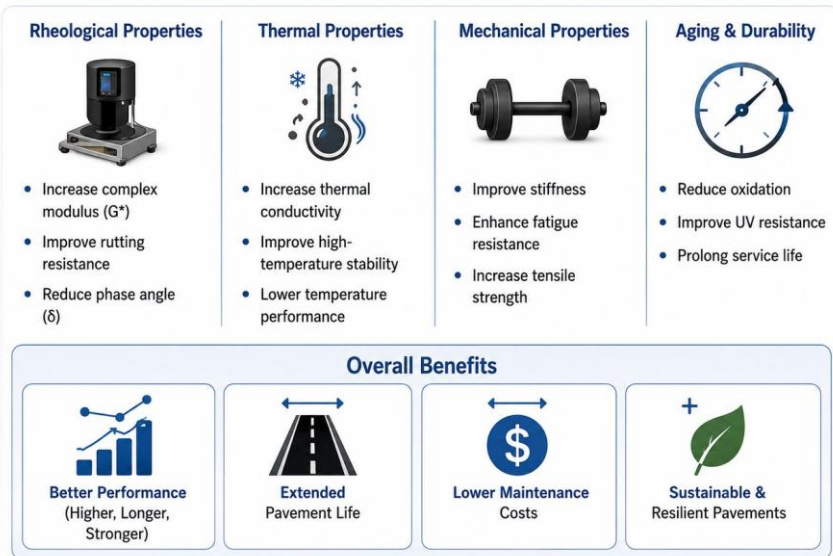


Figure 3.6. *Effects of nanomaterial modification on the rheological, thermal, mechanical and ageing properties of the binder and the performance benefits that follow.*

High-temperature (rutting) performance is the domain in which nanomaterials most reliably excel. In terms of Superpave parameters, nanomodification typically elevates the rutting factor ($G^*/\sin \delta$) and, in the multiple-stress-creep-recovery (MSCR) test, increases the percentage recovery while reducing the non-recoverable creep compliance (J_{nr}), all indicating greater resistance to permanent deformation (Dai et al., 2023; Cheraghian et al., 2022).

At the mixture scale these binder-level improvements are borne out by wheel-tracking and repeated-load tests: graphene nanoplatelets incorporated into SBS-modified binder, for instance, have been shown to raise the rutting resistance of the resulting asphalt mixture by roughly a fifth relative to a reference mixture, while lowering the viscous response at high service temperatures (Polo-Mendoza et al., 2023; Moretti et al., 2021). Metal-oxide and silica nanomaterials similarly improve elastic recovery and high-temperature stiffness, and engineered nano-mineral composites have been reported to maximise rheological resistance, both before and after ageing, at very low optimum contents on the order of a few tenths of a percent by mass (Cheraghian et al., 2022). Because these gains are achieved without the phase-separation liabilities of neat polymer modification, nanomaterials are attractive either as stand-alone modifiers or as stabilising co-additives in polymer-modified systems.

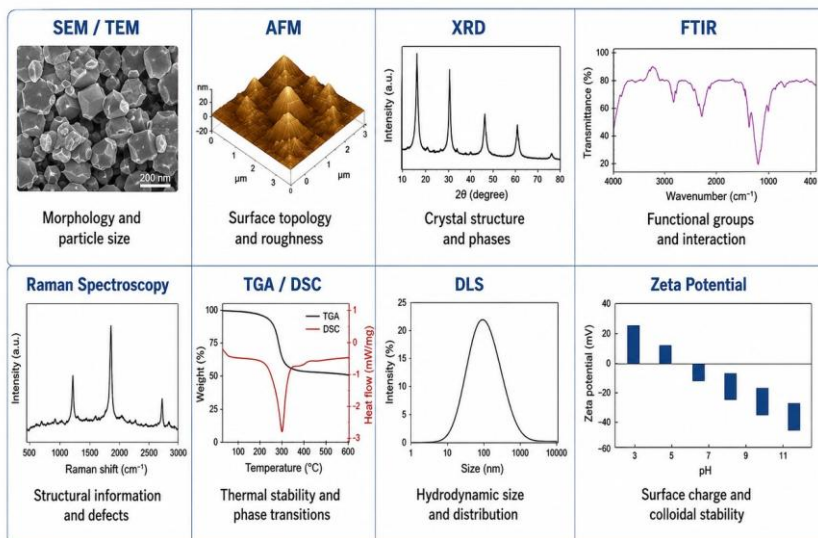


Figure 3.7. *Techniques for characterizing nanomodified binders, from SEM/TEM and AFM to XRD, FTIR, Raman spectroscopy, thermal analysis and zeta-potential measurement.*

The picture at intermediate and low temperatures, governing fatigue and thermal cracking, is more nuanced and dosage-dependent. Fatigue resistance, assessed at the binder scale through time-sweep and linear-amplitude-sweep testing and at the mixture scale through four-point-bending tests, can be either enhanced or diminished by nanomodification depending on the material, the loading, and the degree of dispersion. Well-dispersed reinforcing nanomaterials frequently extend fatigue life: carbon nanomaterials such as graphene oxide and carbon nanotubes have been reported to prolong the fatigue life of SBS-modified binders through their crack-bridging and stress-distributing action (Wang et al., 2021), and graphene nanoplatelets have been shown to increase the fatigue life of asphalt mastics, with the improvement growing as the filler–asphalt ratio increases (Li et al., 2021). Yet the same stiffening that benefits rutting can, if excessive, reduce a binder's capacity to relax stress and dissipate energy, so that some studies report modest reductions in mixture fatigue resistance even where rutting and healing improve, a trade-off documented for industrial graphene nanoplatelets, which raised rutting resistance and healing capacity while slightly lowering fatigue resistance (Polo-Mendoza et al., 2023). Low-temperature cracking behaviour follows a similar logic: appropriate nanomaterial contents can maintain or improve the binder's low-temperature grade and stress-relaxation properties, whereas over-dosing risks embrittlement, reaffirming the primacy of dosage optimisation (Huang et al., 2024; Cheng et al., 2021).



Figure 3.8. *Current challenges and future perspectives for nanomaterials in pavement engineering, spanning cost, dispersion, standardization and multifunctionality.*

Two further performance dimensions of direct relevance to sustainable pavements are moisture resistance and ageing resistance. Moisture-induced damage, driven by the loss of adhesion at the binder–aggregate interface and of cohesion within the binder, is mitigated by nanomaterials that strengthen these bonds. Carbon nanotubes, for example, have been shown to improve the wet and aged adhesion of binder films and to raise the tensile-strength ratio of mixtures well above conventional thresholds, indicating markedly better resistance to moisture damage (Liang et al., 2020). Ageing resistance, already discussed mechanistically, manifests rheologically as a smaller increase in stiffness and a smaller loss of relaxation capacity after laboratory conditioning: fumed-silica-modified binders show improved retention of properties after thermo-oxidative and UV ageing (Cheraghian & Wistuba, 2021; Zhou et al., 2023), nano-TiO₂-modified binders resist UV-driven property change (Lima et al., 2022; Yang et al., 2022), and zinc-oxide modification confers comparable anti-ageing benefits (Iftikhar et al., 2023). The practical value of these effects is amplified in the

context of recycling, where nanomaterials can rejuvenate and reinforce binders containing high proportions of reclaimed asphalt pavement, enabling greater use of recycled material without sacrificing durability (Alam et al., 2024; Afshin & Behnood, 2025).

Table 3.3. *Comparative overview of nanomaterials for bitumen modification*

Nanomaterial	Dim.	Typical dosage	Primary function	Representative study
Nano-silica (SiO ₂)	0D	2-4 wt%	Stiffening, ageing resistance	Dai et al. (2023)
Fumed silica	0D aggregate	2-5 wt%	Elasticity, anti-ageing	Zhou et al. (2023)
Fumed silica (UV)	0D	3-5 wt%	UV ageing resistance	Cheraghian & Wistuba (2021)
Nano-clay (MMT)	2D	2-5 wt%	Barrier, storage stability	Ren et al. (2020)
Organo-montmorillonite	2D	2-4 wt%	Exfoliation, rutting	Cheng et al. (2021)
Carbon nanotubes (CNT)	1D	0.5-1.5 wt%	Crack bridging, fatigue	Liang et al. (2020)
CNT / polymer composite	1D	0.5-1 wt%	Rheology, moisture	Liang et al. (2020)
CNT / recycled PE	hybrid	~1 wt%	Storage stability	Yu et al. (2021)
Graphene / GO	2D	0.5-2 wt%	Modulus, barrier, adhesion	Wang et al. (2021)
Graphene nanoplatelets	2D	1-5 wt%	Rutting, healing, thermal	Polo-Mendoza et al. (2023)
GNP (mastic)	2D	filler-scaled	Fatigue of mastic	Li et al. (2021)

Nanomaterial	Dim.	Typical dosage	Primary function	Representative study
Nano-TiO ₂	0D oxide	3-5 wt%	UV shielding, photocatalysis	Lima et al. (2022)
Nano-TiO ₂ / MMT	hybrid	2-4 wt%	UV plus barrier synergy	Liao et al. (2021)
Nano-ZnO	0D oxide	<1-3 wt%	UV, anti-ageing, rutting	Iftikhar et al. (2023)
Nano-Al ₂ O ₃	0D oxide	2-4 wt%	Rheology, thermal conductivity	Iftikhar et al. (2023)
Engineered nanocomposite	mixed	<0.5 wt%	Rheology before, after ageing	Cheraghian et al. (2022)
Nanomaterials for RAP	mixed	low	Rejuvenation, reinforcement	Alam et al. (2024)

Taken together, the evidence indicates that nanomaterials can deliver a favourable and often synergistic combination of properties: substantially improved high-temperature and rutting performance, enhanced moisture and ageing resistance, and, when dosage and dispersion are properly controlled, maintained or improved fatigue and low-temperature behaviour. The recurring caveat is that these benefits are conditional. They depend on achieving fine, stable dispersion (Section 3.2), on understanding the operative mechanisms (Section 3.3), and above all on identifying the optimum content for each nanomaterial–binder system, beyond which agglomeration and over-stiffening erode the gains (Iftikhar et al., 2023; Huang et al., 2024). Within these constraints, nanomaterials constitute a versatile and powerful toolkit for engineering the advanced functional binders on which durable, sustainable flexible pavements increasingly rely.

AUTHOR'S PERSPECTIVE

Across the nano-silica and metal-oxide work I have followed, the recurring lesson is that dispersion, not dosage, decides the outcome. A well-dispersed nano-silica or nano- Al_2O_3 at a low content, generally below about 3 wt%, usually gives the best balance of rutting improvement and workability, whereas pushing the content higher to chase a larger modulus almost always backfires through agglomeration and embrittlement. I would make a dispersion-verification step (SEM or AFM) a condition of acceptance for any nano-modified binder, because the same material can succeed or fail entirely on how it was mixed.

CHAPTER SUMMARY

Chapter 3 examined the four principal nanomaterial families, the decisive role of dispersion and storage stability, the physical and physicochemical modification mechanisms, and their effects on rheological and mechanical performance.

Key findings

- ▶ Dispersion quality, more than dosage, determines whether a nanomaterial helps or harms.
- ▶ Nanomaterials reinforce, adsorb, form diffusion barriers and rebalance the binder colloid, often simultaneously.
- ▶ Optimum contents are typically low; beyond them agglomeration and over-stiffening erode the gains.

Design recommendations

- ▶ Keep nano-silica and nano-oxide contents low (often below about 3 wt%) and verify dispersion by SEM or AFM.
- ▶ Exploit two-dimensional fillers (clay, graphene) for barrier and ageing resistance.
- ▶ Use nanoclays as co-stabilisers to improve the storage stability of polymer-modified binders.

Future research

- ▶ Scalable, plant-ready dispersion methods and functionalised surfaces.
- ▶ Standardised dosage-performance protocols across nanomaterial families.

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CHAPTER 4

Waste Valorization in Flexible Pavements: Industrial and Post-Consumer Materials

Rationale for Waste Utilization and the Circular Economy

The flexible pavement sector sits at the intersection of two mounting pressures: the escalating demand for durable road infrastructure and the parallel imperative to decouple that demand from the extraction of finite virgin resources. Conventional hot-mix asphalt is, by mass, an overwhelmingly mineral product, typically ninety-four to ninety-six percent aggregate bound by a petroleum-derived bitumen, and both constituents carry substantial environmental burdens across their life cycles. Quarrying of natural aggregate consumes energy, alters landscapes, and depletes locally available stone, while the production and processing of bitumen are energy-intensive and emissions-laden. Against this backdrop, the valorization of industrial by-products and post-consumer wastes has evolved from a marginal, cost-driven expedient into a central strategy of sustainable pavement engineering. The reuse of materials that would otherwise be landfilled or incinerated addresses

simultaneously the supply-side scarcity of quality aggregates and binders and the demand-side accumulation of solid waste, positioning road construction as one of the few high-volume applications capable of absorbing waste streams at a scale commensurate with their generation (Barbhuiya, Qureshi, & Das, 2025). Figure 4.1 summarises the environmental, economic, technical and social benefits that motivate this shift, and Figure 4.2 places waste valorization within the wider circular-economy model for pavements.

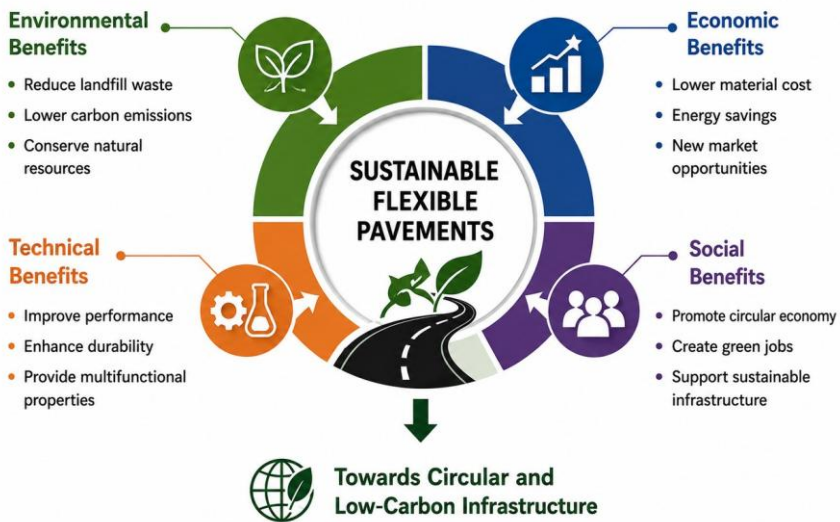


Figure 4.1. *Environmental, economic, technical and social benefits that together motivate the valorization of waste materials in sustainable flexible pavements.*

The conceptual scaffolding for this shift is the circular economy, a framework that reconceives materials not as linear flows from extraction to disposal but as constituents of closed or cascading loops in which value is retained through repeated cycles of use. Within construction and demolition contexts, the circular economy

emphasizes resource efficiency, waste minimization, and the deliberate design of material recovery pathways, and it has increasingly been operationalized through key performance indicators that quantify diversion from landfill and substitution of primary materials (Papamichael, Voukkali, Loizia, & Zorpas, 2023). Construction and demolition waste constitutes one of the largest solid-waste streams globally, and the road sector is uniquely positioned to consume large fractions of it because pavements demand enormous tonnages of granular and bituminous material whose performance requirements, while exacting, can often be met by processed wastes. The circular-economy logic reframes materials such as slags, ashes, glass cullet, reclaimed asphalt, waste tires, and post-consumer plastics not as disposal liabilities but as engineered secondary resources whose incorporation can reduce embodied carbon, conserve virgin stone and binder, and lower the whole-life environmental footprint of the pavement (Barbhuiya et al., 2025).

The environmental case for waste valorization is now supported by a substantial body of life-cycle evidence. Comprehensive reviews of recycled and low-carbon pavement materials consistently report that the substitution of virgin aggregate and binder with appropriately processed wastes reduces energy consumption, greenhouse-gas emissions, and pressure on natural extraction, provided that the additional impacts of collection, sorting, processing, and transport are properly accounted for (Barbhuiya et al., 2025; Mashaan, Oguntayo, & Dassanayake, 2025). Reclaimed asphalt pavement offers perhaps the clearest illustration of a closed material loop within the sector: because it contains both aged binder and sound aggregate, its reincorporation displaces two virgin inputs at once. Industry surveys document the magnitude of the opportunity, with roughly ninety-eight million tons of reclaimed asphalt pavement used in mixtures in the United States in a single recent year and an industry-average recycled content exceeding

twenty percent, alongside recycling rates for reclaimed asphalt that surpass ninety-nine percent (National Asphalt Pavement Association, 2024). These figures demonstrate that waste valorization in flexible pavements is not a speculative aspiration but an established, large-scale practice whose expansion is limited more by technical performance and specification constraints than by material availability.

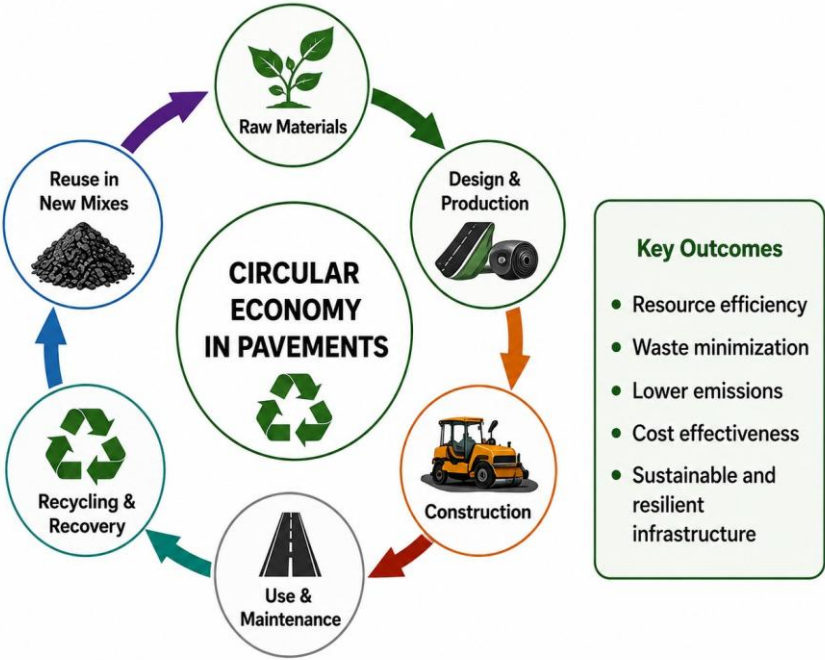


Figure 4.2. Circular-economy model for pavements, in which materials are recovered, reprocessed and returned to new mixtures rather than sent to landfill.

Yet the rationale for waste utilization is not solely environmental; it is also economic and, increasingly, regulatory. The rising cost and diminishing local availability of high-quality natural aggregate in many regions render locally generated by-products such as steel slag or fly ash attractive on strictly economic grounds,

particularly where the alternative involves long-haul transport of virgin stone. Landfill levies, extended-producer-responsibility schemes, and public-procurement policies that reward recycled content further tilt the balance toward valorization. At the same time, the framing of waste incorporation as unambiguously beneficial must be tempered by rigorous engineering and environmental scrutiny. The central thesis of this chapter is that the sustainability benefits of waste valorization are real but conditional: they materialize only when the incorporated material is properly characterized, appropriately processed, and dosed within limits that preserve or enhance mechanical performance and do not introduce unacceptable secondary impacts such as leaching or microplastic release (Enfrin, Myszka, & Giustozzi, 2022; Mashaan et al., 2025). The remainder of the chapter examines the principal waste families in turn, polymeric and rubber wastes, then industrial by-products and mineral wastes, before synthesizing their effects on mixture properties and the practical considerations that govern their responsible deployment.

Polymeric and Rubber Wastes

Among post-consumer and industrial wastes, polymeric plastics and end-of-life tire rubber have attracted the most intense research and public attention, both because of the acute environmental problems their accumulation represents and because of their demonstrable capacity to modify the rheology and mechanical behavior of bituminous binders. The two families share a common logic, repurposing a durable, non-biodegradable polymer as a bitumen modifier or aggregate substitute, but differ substantially in their chemistry, their established histories of use, and the specific concerns they raise. Figure 4.3 traces the processing route by which such wastes are converted into functional pavement materials.

Waste plastics

The incorporation of waste plastics into asphalt has become one of the most rapidly expanding areas of pavement materials research, driven by the sheer volume of plastic waste generated worldwide and the limited capacity of conventional recycling to absorb it. Waste plastics used in asphalt are predominantly polyolefins, low- and high-density polyethylene, polypropylene, and polyethylene terephthalate, sourced from packaging, films, and containers. A comprehensive review synthesizing global research across six major plastic types and both processing routes concluded that plastic modification, when properly executed, enhances the stiffness, rutting resistance, fatigue life, and moisture durability of asphalt while offering a high-volume outlet for a problematic waste stream (Shah, Gao, & Abdelfatah, 2025). The mechanisms underlying these improvements are well established: the addition of a stiff thermoplastic increases the viscosity and elastic recovery of the binder, raises its high-temperature stiffness and rutting resistance, and can strengthen the adhesion between binder and aggregate.



Figure 4.3. Processing route that converts collected waste streams, through sorting, cleaning and treatment, into functional pavement materials and modified asphalt.

Two principal technologies govern how plastics are introduced. In the wet process, the plastic is blended into the hot bitumen at elevated temperature to form a modified binder, yielding a more homogeneous product with improved and controllable rheology but demanding higher energy input and careful management of storage stability. In the dry process, shredded plastic is added directly to the heated aggregate before the binder is introduced, so that the plastic acts partly as a binder modifier and partly as an aggregate or filler substitute; this route is simpler and more cost-effective and permits higher plastic loadings, but it can produce uneven dispersion and less predictable binder interaction (Shah et al., 2025). The choice between processes is therefore a trade-off between the homogeneity and controllability of wet blending and the operational simplicity and higher waste-absorption capacity of the dry method.

The mechanical benefits reported in the literature are frequently substantial. Laboratory evaluations of low-density polyethylene waste as a binder modifier have documented pronounced increases in mixture stiffness, on the order of well over one hundred percent at service temperatures relative to an unmodified base binder, together with meaningful gains in indirect tensile strength and rutting resistance, and these mechanical improvements have been shown to translate into favorable economic outcomes for road construction (Singh & Gupta, 2024). Comparable enhancements in rutting and fatigue performance have been reported across a wide range of plastic types and dosages, and the incorporation of plastics can also reduce the emission of certain harmful volatile and semi-volatile compounds during production and service (Enfrin & Giustozzi, 2022; Shah et al., 2025). Recent work has further explored composite strategies in which recycled plastics are combined with rejuvenating or softening agents, such as waste engine oil, to balance the stiffening effect of the plastic against the need to restore ductility and cracking resistance, demonstrating that plastic modification can be tuned rather than applied as a single-effect additive (El-Sherbeni, Gabr, El-Badawy, & Awed, 2025).

These advantages are counterbalanced by persistent technical and environmental concerns. The foremost technical challenge is compatibility: many waste plastics exhibit poor thermodynamic compatibility with bitumen, and this incompatibility manifests as phase separation during hot storage, transport, and construction, threatening the homogeneity of the modified binder and, consequently, the uniformity of field performance (Shah et al., 2025). Storage stability is therefore a recurrent limiting factor, and much of the current research effort is directed toward compatibilizers, cross-linking agents, and process controls that suppress separation. The environmental concerns are equally consequential and are examined more fully in Section 4.4; they

center on the potential for plastic-modified pavements to shed microplastics through surface abrasion and material ageing, and on the leaching of residual additives, stabilizers, and pigments contained in the waste plastic (Enfrin et al., 2022; Shah et al., 2025). The prevailing scholarly assessment is that plastic-modified asphalt offers clear advantages over conventional and even polymer-modified mixes in terms of carbon and energy, but that a defensible sustainability judgment requires a holistic accounting that includes these end-of-life impacts.

Crumb rubber

Table 4.1. Principal waste streams valorized in flexible pavements

Waste	Source	Role in mixture	Key effect
Crumb rubber	End-of-life tyres	Binder modifier	Higher rutting resistance, elasticity
Waste plastics	Packaging (PE, PET)	Binder, dry additive	Higher stiffness, moisture resistance
Steel, blast-furnace slag	Steelmaking by-product	Aggregate replacement	High skid, durability
Fly ash	Coal combustion	Mineral filler	Stiffening, stability
Waste glass	Container glass	Fine aggregate	Resource saving (skid limit)
RAP	Reclaimed pavement	Aggregate plus binder	Resource and CO2 saving

Crumb rubber derived from end-of-life tires occupies a more mature position in the spectrum of waste modifiers, with a history of field application extending back several decades and a correspondingly deeper base of long-term performance evidence. Crumb rubber is produced by mechanically grinding scrap tires into

granulated particles, and, like plastics, it may be introduced through a wet process, in which the rubber is digested into the hot bitumen to produce an asphalt-rubber binder, or a dry process, in which the rubber is added to the aggregate as a partial substitute. The wet process yields a modified binder with markedly enhanced elasticity and high-temperature stiffness, while the dry process is technologically simpler and can accommodate larger rubber quantities, giving it particular appeal as a high-volume disposal route for scrap tires (Duan et al., 2023).

The mechanistic effects of crumb rubber on binder behavior are well characterized. The rubber particles swell as they absorb the lighter fractions of the bitumen, increasing the viscosity and stiffness of the binder and enhancing its elastic recovery. At the mixture scale, these changes reduce the rate of rut formation and improve high-temperature deformation resistance, with rubberized specimens exhibiting substantially shallower ruts than unmodified controls under repeated loading (Duan et al., 2023). A synthesis of research progress on crumb-rubber-modified asphalts and their mixtures confirms that the basic and rheological properties of the binder improve appreciably with increasing rubber content, but it also cautions that excessive rubber dosages can impair certain properties, underscoring the existence of an optimum content beyond which returns diminish or reverse (Duan et al., 2023). This non-monotonic behavior, improvement up to a threshold followed by degradation, is a recurring motif across essentially all waste modifiers and is central to the practical guidance developed in Section 4.4.

The durability and field performance of crumb-rubber-modified mixtures have been validated under real service conditions in a manner that few other waste modifiers can claim. A field investigation that constructed multiple road sections under differing climatic conditions and monitored cored specimens over service periods extending to more than five years found that asphalt mixtures

manufactured with crumb-rubber-modified bitumen offered ageing and mechanical performance very similar to that of mixtures produced with conventional styrene–butadiene–styrene polymer-modified binders, subject to severe traffic and climate (Sierra-Carrillo de Albornoz, Moreno-Navarro, & Rubio-Gómez, 2022). This equivalence is significant because it positions crumb rubber not merely as a waste-disposal expedient but as a technically credible substitute for a premium virgin polymer modifier. Indeed, hybrid strategies that combine modest quantities of crumb rubber with reduced dosages of styrene–butadiene–styrene have shown that a small rubber addition can halve the required amount of the virgin polymer while preserving the principal binder properties, offering both cost and sustainability benefits (Duan et al., 2023). Taken together, the plastics and rubber literatures indicate that polymeric wastes can deliver genuine performance enhancements to flexible pavements, but that their benefits are contingent on dosage optimization, compatibility management, and, especially in the case of plastics, careful attention to potential secondary environmental impacts.

Industrial By-products and Mineral Wastes

Whereas polymeric and rubber wastes chiefly modify the binder phase, the second broad family of valorized materials acts principally within the mineral skeleton of the pavement, substituting for virgin aggregate, mineral filler, or, in the case of reclaimed asphalt, for both aggregate and binder. These industrial by-products and mineral wastes are generated in enormous tonnages by the metallurgical, power-generation, and glass industries, and their compositional similarity to natural minerals often makes them technically well suited to pavement incorporation. A recent review of waste by-products in asphalt concrete construction surveys steel slag, fly ash, and related mineral residues, concluding that many of

these materials confer performance benefits as sustainable aggregate and filler substitutes while cautioning that their use is bounded by material-specific limitations that must be managed through characterization and dosage control (Mashaan et al., 2025). Figure 4.4 gathers the principal waste streams together with their functions in the mixture, and Figure 4.5 shows the roles these materials play across the pavement structure.

Steel and blast-furnace slags

Steel slag, a by-product of steelmaking, is among the most extensively studied mineral wastes for asphalt applications, and its physical characteristics make it in several respects superior to conventional natural aggregate. Steel slag aggregates typically exhibit high hardness, angular texture, rough surfaces, and strong affinity for bituminous binder, properties that promote excellent skid resistance, mechanical interlock, and adhesion. A performance evaluation of steel slag asphalt mixtures incorporating the material at rates of twenty and thirty-five percent found that the inclusion of steel slag aggregate did not impair mixture behavior and in several respects improved it, with gains in resistance to permanent deformation, stability, flow, and water sensitivity relative to control mixtures (Neves & Crucho, 2023). Complementary laboratory work on electric-arc-furnace and basic-oxygen-furnace slags used as partial replacements for conventional aggregate, at levels of ten, thirty, and fifty percent, reported that mix-design properties remained within specification and that abrasion loss was reduced irrespective of replacement level, with an optimum around thirty percent; electric-arc-furnace slag in particular outperformed both basic-oxygen-furnace slag and conventional mixtures in moisture sensitivity, rutting resistance, fatigue behavior, and resilient modulus (Chandrashekar Gowda & Naveen, 2023). These findings are consistent with the higher adhesion energy and superior hardness

commonly attributed to steel slag relative to natural aggregates such as limestone (Mashaan et al., 2025).

The principal technical caveat attaching to steel slag is volumetric instability. Steel slags frequently contain free lime and free magnesium oxide, which hydrate and expand upon prolonged exposure to moisture, potentially inducing swelling, cracking, and disintegration in the pavement. This hydration potential is the dominant limiting factor governing the safe use of steel slag, and the literature is consistent in recommending that the material be weathered or aged to allow expansive phases to react before incorporation, and that expansion be controlled through appropriate volumetric limits and quality assurance (Mashaan et al., 2025; Neves & Crucho, 2023). Its higher density relative to natural aggregate also raises the mass of material required per unit volume of pavement, a consideration for haulage and mix design. Blast-furnace slag, generated in iron production and distinct in composition from steelmaking slags, has likewise been used successfully as coarse and fine aggregate; air-cooled blast-furnace slag is more absorptive than conventional aggregate and therefore increases binder demand, but pavements containing it exhibit good skid resistance and satisfactory durability. The overall picture that emerges is that metallurgical slags are among the most technically promising of all mineral wastes for asphalt, capable of matching or exceeding the performance of natural aggregate provided that their expansive potential and absorptivity are properly managed.

Reclaimed Asphalt Pavement (RAP)	Crumb Rubber	Waste Plastic	Waste Glass	Fly Ash / GGBS	Biochar / Bio-based Material
					
• Reuse bitumen layers • Reduce virgin materials demand • Up to 20–30% RAP in many applications	• Asphalt rubber modifier (CRM) • SMA and OGFC improvement • Improved crack and fatigue performance	• Binder modification • Improved moisture resistance • Lower temperature performance	• Filler replacement • Enhanced skid resistance • Improved polishing resistance	• Filler replacement • Improve workability • Enhance durability and permeability	• Binder modification • UV and aging resistance • Carbon sequestration potential

Figure 4.4. *Principal waste streams used in flexible pavements, reclaimed asphalt, crumb rubber, waste plastic, glass, fly ash and biochar, together with their functions in the mixture.*

The synergy between slag and other recycled streams has attracted growing attention. Stone mastic asphalt designed with coarse steel slag aggregate in combination with fine reclaimed asphalt pavement has been evaluated through wheel-tracking, low-temperature bending, freeze–thaw, and fatigue testing, demonstrating that two waste streams can be co-valorized within a single high-performance surfacing without sacrificing pavement performance (Wu et al., 2025). Such combinations exemplify the circular-economy aspiration of stacking multiple recovered materials in one mixture, though they also compound the characterization and quality-control demands placed on the mix designer.

Fly ash

Fly ash, the fine particulate residue captured from the flue gases of coal-fired power generation, represents one of the largest single industrial waste streams globally, and its fine, largely

spherical particles make it a natural candidate for use as mineral filler in asphalt. Although fly ash has long been employed in cement and concrete, its use in asphalt pavement has been comparatively limited, and recent research has sought to establish it more firmly as a filler substitute. Studies incorporating coal fly ash as a filler in hot-mix asphalt report improvements in rutting and fatigue performance relative to conventional mixtures, attributable to the ash's contribution to mastic stiffness and its favorable particle characteristics (Mashaan et al., 2025). Because fly ash can be hydrophilic and variable in composition, processing strategies such as hydrophobic surface modification have been investigated to render it a free-flowing, moisture-resistant powder suitable as a mineral filler, with reported gains in compressive strength and adhesion relative to reference fillers. The chief considerations governing fly ash use are its inherent compositional variability, which depends on the source coal and combustion conditions, and the need to verify that trace-element content does not present a leaching hazard, concerns that place a premium on consistent sourcing and characterization.

Waste glass

Waste glass, generated in large quantities from packaging and container disposal and only partially absorbed by conventional bottle-to-bottle recycling, has been investigated as a fine-aggregate substitute in asphalt for several decades under the informal designation "glasphalt." Crushed glass shares a siliceous composition and angular fracture with natural sand, and moderate replacement levels can be accommodated without detriment to mixture properties. An assessment of waste glass incorporation in asphalt concrete for surface-layer construction, using both monolithic and tempered glass at ten and fifteen percent replacement, evaluated stiffness, resistance to permanent deformation, indirect tensile strength, and moisture susceptibility

and found the material technically viable for surface applications (Kalampokis, Kalama, Kesikidou, Stefanidou, & Manthos, 2023). Work on waste glass as an aggregate in asphalt micro-surfacing similarly demonstrated acceptable resistance to water action, wear, rutting, and skidding, extending the material's applicability to thin surface treatments (Cheng et al., 2021). More specialized formulations have explored borosilicate glass, whose low coefficient of thermal expansion, high shock resistance, and chemical durability make it an attractive engineered variant, with feasibility studies confirming its potential as a replacement material in asphalt concrete (Hamid et al., 2023).

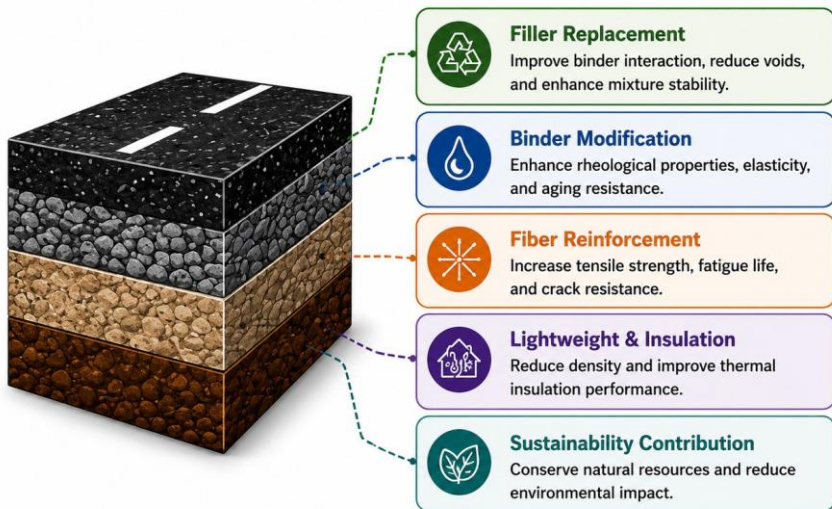


Figure 4.5. Roles that waste-derived materials play across the pavement structure, as filler replacement, binder modifier, fibre reinforcement and sustainability contributor.

The recurring technical limitations of waste glass are twofold. First, the smooth surfaces and low porosity of glass particles weaken the adhesion between binder and aggregate,

promoting moisture-induced stripping; this is conventionally mitigated by limiting glass content, restricting particle size, and adding anti-stripping agents or hydrated lime. Second, larger glass particles are prone to fracture under compaction and traffic and can create safety concerns, so the literature converges on the use of finer glass fractions, commonly with a maximum size on the order of a few millimeters, and modest replacement ratios, frequently in the range of ten to twenty percent, as the practical envelope within which glass can be used reliably (Cheng et al., 2021; Kalampokis et al., 2023). Within these bounds, waste glass constitutes a locally available fine-aggregate substitute whose incorporation diverts a persistent waste stream from landfill.

Reclaimed asphalt pavement

Reclaimed asphalt pavement stands apart from the other mineral wastes discussed here because it is not an external industrial by-product but the milled or excavated product of the pavement's own end of life, containing both aged binder and sound mineral aggregate. Its reincorporation therefore closes the most direct material loop available to the sector, displacing virgin aggregate and virgin binder simultaneously, and it is by far the highest-volume recycled material in flexible-pavement construction (National Asphalt Pavement Association, 2024). The central technical challenge of reclaimed asphalt is that its binder has been oxidatively aged and hardened, becoming stiffer and more brittle than virgin bitumen; consequently, mixtures containing high fractions of reclaimed asphalt tend to exhibit improved high-temperature and rutting performance but reduced resistance to low- and intermediate-temperature cracking unless the aged binder is remobilized and its properties restored (Bilema & Yuen, 2025).

Two complementary strategies address this challenge. The first exploits the very stiffness of the aged binder by designing high-

modulus asphalt mixtures for which a stiff binder is desirable; experimental work adopting this approach for high reclaimed-asphalt contents found that as the reclaimed-asphalt fraction increased, high-temperature performance improved substantially and low-frequency dynamic modulus rose severalfold, with only a moderate decline in low- and intermediate-temperature crack resistance (Wang, Wu, Wu, & Li, 2025). The second strategy employs rejuvenators, recycling agents engineered to restore the functional properties of the aged binder. A comprehensive state-of-the-art review of rejuvenators explains that effective agents do more than merely soften the binder; they chemically compatibilize the aged asphalt's gel structure, restoring ductility, workability, and cracking resistance and enabling high reclaimed-asphalt contents to be used while achieving performance equivalent to virgin mixtures (Bhatt & Wu, 2025). With effective rejuvenation, reclaimed-asphalt contents well in excess of fifty percent become feasible. A systematic review of high reclaimed-asphalt contents, particularly in combination with other waste materials, confirms both the strong environmental and economic rationale for maximizing reclaimed-asphalt use and the centrality of binder compatibility as the governing constraint on how much can be incorporated (Bilema & Yuen, 2025). Reclaimed asphalt thus epitomizes the promise and the discipline of waste valorization: enormous availability and a genuinely closed loop, tempered by the exacting requirement to manage an aged and hardened binder.

Effects on Mixture Properties and Practical Considerations

The preceding sections surveyed individual waste families largely in isolation; this concluding section synthesizes their collective effects on mixture properties and distills the practical considerations that determine whether waste valorization succeeds or fails in the field. Across the entire spectrum of wastes, a set of

common principles emerges, cutting across the distinction between binder modifiers and aggregate substitutes. Figure 4.6 summarises the effects of the various waste materials on the principal performance aspects of asphalt mixtures, while Figure 4.7 sets out the remaining challenges, the future perspectives and the long-term vision for waste valorization in pavements.

The most consistent finding is the existence of an optimum dosage for essentially every waste material. Whether the material is crumb rubber, waste plastic, steel slag, fly ash, waste glass, or reclaimed asphalt, mechanical performance tends to improve as the waste is added up to a characteristic threshold and then to plateau or degrade beyond it. Excessive crumb rubber damages certain binder properties despite improving others (Duan et al., 2023); high replacement levels of steel slag beyond the optimum reduce performance relative to control mixtures (Chandrashekar Gowda & Naveen, 2023); glass content must be capped to preserve adhesion and safety (Kalampokis et al., 2023); and reclaimed-asphalt fractions are bounded by the brittleness of the aged binder (Bilema & Yuen, 2025). The corollary for practice is that no waste should be dosed to the maximum the process can physically accommodate; rather, mixtures must be designed around a performance-optimized content established through laboratory testing. This is a decisive shift away from the historical framing of wastes as materials to be disposed of in the largest possible quantity and toward their treatment as engineered constituents subject to the same optimization discipline as any virgin material.

Performance Aspect	Potential Improvement	Typical Waste Materials	Reference Effects
 Rutting Resistance	Increase high-temperature stability and stiffness	Crumb rubber, Waste plastic, Fly ash	↑
 Fatigue Resistance	Enhance fatigue life and crack resistance	Rubber, Fibers, Glass powder, RAP	↑
 Moisture Resistance	Improve moisture susceptibility	Lime-treated fly ash, Glass powder	↑
 Low Temperature Performance	Improve flexibility and crack resistance	Rubber, Waste plastic modifiers	↑
 Durability	Reduce aging and oxidation	Nanomaterials, Biochar, GGBS	↑
 Environmental Impact	Reduce CO ₂ emissions and energy consumption	All waste materials, RAP	↑↑

Figure 4.6. *Effect of the main waste materials on the principal performance aspects of asphalt mixtures, rutting, fatigue, moisture and low-temperature resistance, durability and environmental impact.*

A second cross-cutting theme is the frequent trade-off between resistance to permanent deformation at high temperatures and resistance to cracking at low and intermediate temperatures. Stiffening modifiers and stiff recovered materials, waste plastics, crumb rubber in the wet process, and aged reclaimed-asphalt binder, reliably enhance rutting resistance but can compromise fatigue and thermal-cracking performance if applied without countermeasures (Shah et al., 2025; Wang et al., 2025). The engineering response is to balance the mixture deliberately: pairing stiffening wastes with rejuvenators, softer base binders, or ductility-restoring co-additives such as waste engine oil so that high-temperature and low-temperature performance are simultaneously satisfied (Bhatt & Wu, 2025; El-Sherbeni et al., 2025). The concept of a balanced mix design, in which rutting and cracking are optimized jointly rather

than sequentially, is therefore especially pertinent to waste-modified pavements.

Moisture susceptibility constitutes a third recurring practical concern. Several wastes introduce or exacerbate the risk of moisture-induced damage: waste glass through its smooth, low-adhesion surfaces, and, more subtly, any material that alters the binder–aggregate interface. Conversely, some wastes improve moisture resistance, steel slag through its strong binder affinity, and hydrophobically modified fly ash through its engineered water repellency. The practical implication is that moisture sensitivity must be verified experimentally for each waste-modified mixture, and that mitigation measures such as anti-stripping agents or hydrated lime should be deployed where the incorporated waste is known to weaken adhesion (Cheng et al., 2021; Kalampokis et al., 2023). Steel slag introduces the additional and distinctive requirement of volumetric-stability control, given the expansive hydration of free lime and magnesium oxide; weathering of the slag prior to use and strict volumetric limits are the accepted safeguards (Mashaan et al., 2025; Neves & Crucho, 2023).

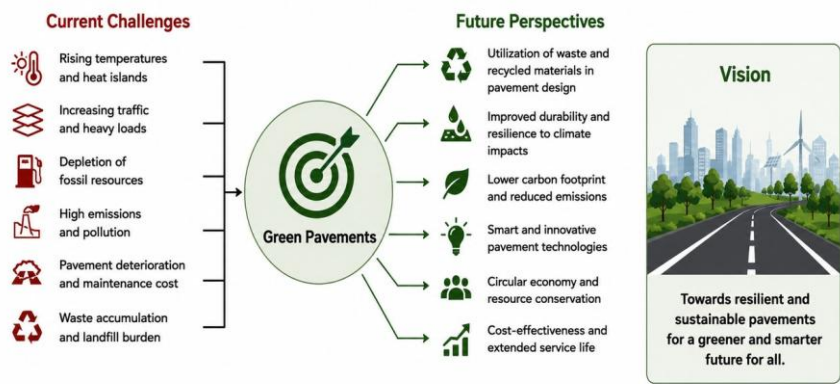


Figure 4.7. *Current challenges, future perspectives and the long-term net-zero vision for waste valorization in flexible pavements.*

Beyond mechanical performance, waste valorization raises questions of homogeneity, workability, and construction practice. Storage stability is a preeminent concern for plastic-modified binders, whose tendency toward phase separation during storage, pumping, transport, and paving threatens the uniformity of the delivered product and must be managed through compatibilizers and process control (Shah et al., 2025). Absorptive wastes such as blast-furnace slag increase binder demand and therefore affect mixture economics and volumetrics. Reclaimed asphalt and other recovered streams are inherently variable in composition, and their reliable use depends on frequent characterization and quality assurance to manage that variability. These realities mean that the successful field deployment of waste-modified mixtures depends as much on robust materials management, consistent sourcing, processing, sampling, and testing, as on the intrinsic properties of the waste itself.

Table 4.2. *Typical dosage and practical considerations for key wastes*

Material	Typical dosage	Benefit	Caution
Crumb rubber	10-20 % of binder	Rutting, noise, sustainability	Workability, storage stability
Waste plastic	4-10 % of binder	Stiffness, moisture resistance	Dispersion, microplastics
Steel slag	up to 100 % coarse agg.	Skid, strength	Volumetric expansion
RAP	20-50 % (up to 100 %)	Cost and CO2 saving	Aged binder needs rejuvenator

The environmental dimension, finally, must be integrated into any responsible assessment rather than assumed. The strongest case study is that of plastic-modified asphalt, whose demonstrable advantages in carbon, energy, and waste diversion are qualified by two distinct end-of-life concerns: the shedding of microplastic particles through the mechanical wear of the pavement surface under the combined action of traffic, ultraviolet radiation, and oxidative ageing, and the leaching of residual additives, stabilizers, and pigments carried in the waste plastic (Enfrin et al., 2022; Shah et al., 2025). Investigations into microplastic release from recycled-plastic-modified asphalt have shown that such release, while real, can be comparable to that from conventional polymer-modified pavements and is strongly influenced by environmental conditions, indicating that the issue is one to be quantified and managed rather than a categorical disqualification (Enfrin et al., 2022). Analogous scrutiny applies to the potential leaching of trace elements from fly ash and slags. The unifying lesson is that the sustainability of a waste-modified pavement cannot be inferred from waste diversion alone; it must be established through life-cycle assessment that captures processing burdens and end-of-life impacts, and it must be weighed against the material's demonstrated performance and durability (Barbhuiya et al., 2025; Mashaan et al., 2025).

In synthesis, the valorization of industrial by-products and post-consumer materials in flexible pavements has matured into a technically robust and environmentally motivated practice, but one whose benefits are conditional rather than automatic. Polymeric and rubber wastes can substantially enhance binder rheology and mixture performance; metallurgical slags can match or exceed natural aggregate; fly ash and waste glass provide serviceable filler and fine-aggregate substitutes; and reclaimed asphalt offers an unrivaled closed material loop. Realizing these benefits, however, requires disciplined dosage optimization, deliberate balancing of high- and

low-temperature performance, verification and mitigation of moisture and volumetric risks, rigorous materials management to control variability and ensure homogeneity, and honest accounting of end-of-life environmental impacts. Approached with this discipline, waste valorization is not a compromise of pavement quality in the name of sustainability but a convergence of the two, advancing the circular-economy vision of roads that consume waste, conserve virgin resources, and perform to the demands placed upon them.

AUTHOR'S PERSPECTIVE

Waste valorization succeeds or fails on process control rather than on the waste itself. Crumb rubber must be given time to digest, waste plastic must be introduced by a route that actually disperses it, and high-RAP mixtures live or die by the rejuvenator and the assumed degree of binder blending. I treat every waste stream as a variable feedstock: I would specify incoming-material characterisation and a moisture-and-dosage protocol before I would trust a headline performance number from a single laboratory batch.

CHAPTER SUMMARY

Chapter 4 set waste valorization within the circular economy and reviewed polymeric and rubber wastes, industrial by-products and mineral wastes, and their effects on mixture properties and practical implementation.

Key findings

- ▶ Road construction can absorb large waste streams at a scale commensurate with their generation.
- ▶ Crumb rubber, waste plastics, slag, fly ash, glass and RAP each bring distinct benefits and cautions.
- ▶ Benefits are conditional on processing route, dosage and, for RAP, rejuvenation and blending assumptions.

Design recommendations

- ▶ Characterise incoming waste and control moisture and dosage before production.

- ▶ Give crumb rubber adequate digestion and disperse waste plastics by an appropriate route.
- ▶ Pair high-RAP mixtures with a validated rejuvenator and realistic blending assumptions.

Future research

- ▶ Life-cycle and ecotoxicity assessment of waste-modified mixtures, including microplastic release.
- ▶ Specifications that credit durability, not only diverted-waste tonnage.

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CHAPTER 5

Performance Characterization of Modified Asphalt Mixtures

The transition from empirical, recipe-based specifications to performance-related characterization has been the single most consequential development in flexible-pavement materials engineering over the past three decades. Modification of asphalt binders with polymers, crumb rubber, nanomaterials, and an increasingly diverse family of functional additives has expanded the attainable property envelope of bituminous materials far beyond that of neat binders, but it has simultaneously exposed the limitations of the classical grading framework. A styrene–butadiene–styrene (SBS)-modified binder, a rubberized binder, and a nanoclay-modified binder may share an identical penetration grade yet behave in profoundly different ways under repeated load, at low temperature, and after years of oxidative aging. Meaningful characterization of modified asphalt mixtures therefore requires a multiscale, multi-property approach that couples fundamental

rheology of the binder, mechanical and durability testing of the compacted mixture, microstructural and chemical interrogation of the modified phase, and an explicit accounting for the evolution of all of these properties over the pavement's service life. This chapter surveys the principal experimental tools used for that purpose, emphasizing their physical basis, their sensitivity to the mechanisms introduced by functional modifiers, and their interpretation in the context of sustainable pavement design.

Rheological Characterization of Modified Binders (DSR, BBR, MSCR)

Rheological characterization occupies the foundational tier of performance evaluation because the viscoelastic response of the binder governs, to first order, the high-temperature stability, intermediate-temperature fatigue tolerance, and low-temperature cracking resistance of the mixture it binds. As summarized in Figure 5.1, rigorous characterization spans the chemical, microstructural, rheological, thermal, physical, and performance-testing domains of the modified binder and mixture, and the discussion that follows moves systematically through these tiers. The dynamic shear rheometer (DSR) is the central instrument of modern binder rheology, and the principal rheological tests, together with the parameters and properties they assess, are compared in Figure 5.2. In an oscillatory shear test, a thin binder film sandwiched between parallel plates is subjected to a sinusoidal strain, and the resulting stress is resolved into the complex shear modulus, G , and the phase angle, δ . *The complex modulus quantifies the total resistance to deformation, while the phase angle expresses the balance between the stored elastic and dissipated viscous components of that resistance, ranging from 0° for a purely elastic solid to 90° for a purely viscous liquid. The Superpave high-temperature rutting parameter, $G/\sin \delta$, and the intermediate-temperature fatigue*

parameter, $G^* \cdot \sin \delta$, were derived from this framework. For neat binders these parameters remain serviceable, but for modified binders they are widely acknowledged to be inadequate because they are measured deep within the linear viscoelastic region, whereas the field distresses they are meant to predict are non-linear, accumulative phenomena. The delayed elastic recovery imparted by a continuous polymer network, for instance, is poorly captured by a single-frequency, small-strain measurement, and the rutting parameter has repeatedly failed to rank polymer-modified binders in agreement with field performance (D'Angelo, 2009).

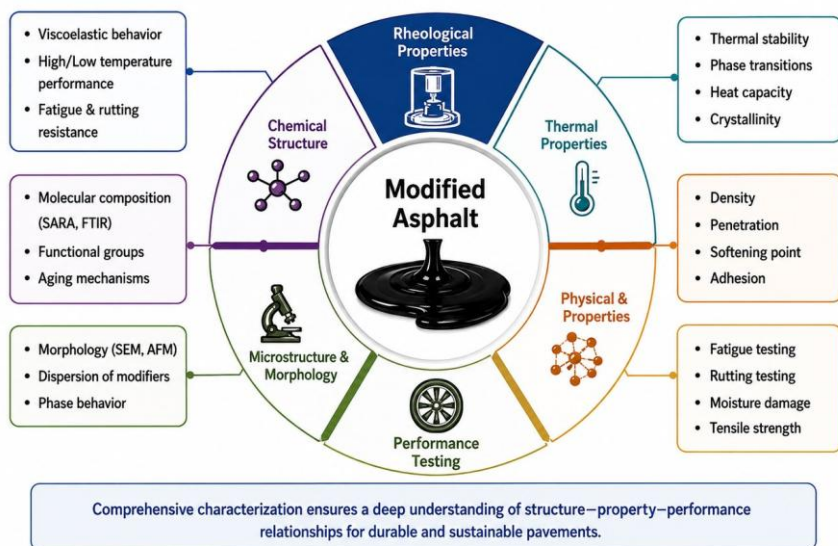


Figure 5.1. Comprehensive characterization framework for modified asphalt, linking the chemical, microstructural, rheological, thermal and physical domains to field performance.

The multiple stress creep recovery (MSCR) test was developed specifically to remedy these shortcomings and now represents the state of practice for high-temperature grading of modified binders. In the MSCR procedure, the binder is subjected in

the DSR to repeated cycles of one second of constant creep stress followed by nine seconds of recovery, first at a low stress of 0.1 kPa and then at a high stress of 3.2 kPa. Two parameters are extracted: the non-recoverable creep compliance, J_{nr} , which correlates strongly with the mixture's resistance to permanent deformation, and the percent recovery, R , which quantifies the delayed elastic response and hence the effectiveness of the polymer network. The stress-sensitivity index, $J_{nr,diff}$, computed from the difference in compliance between the two stress levels, flags binders whose response degrades under heavier loading. Because the test applies a genuinely non-linear stress and separates the recoverable from the non-recoverable strain, it discriminates among neat, SBS, crumb-rubber, and chemically modified binders far more effectively than $G^*/\sin \delta$, and it does so without any prior knowledge of the modification type (D'Angelo, 2009). The MSCR framework has been shown to correlate with the delayed elastic behaviour of polymer-modified systems and with the compatibility and phase structure of the binder, both of which are functions of the polymer/asphalt interaction discussed later in this chapter (Polacco, Filippi, Merusi, & Stastna, 2015).

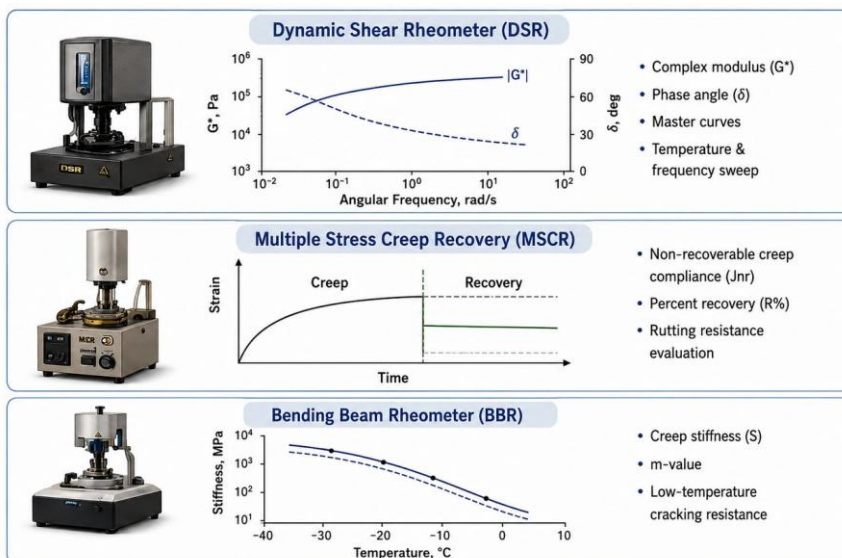


Figure 5.2. Rheological characterization of bituminous binders by dynamic shear rheometer, multiple-stress creep recovery and bending-beam rheometer, and the property each test assesses.

At the opposite end of the temperature spectrum, the resistance of a binder to thermal and fatigue cracking depends on its stiffness and its ability to relax stress at low temperatures. The bending beam rheometer (BBR) is the standard tool for this regime. A small prismatic beam of binder is conditioned at the design low temperature and loaded at its midspan, and the creep stiffness, $S(t)$, and the rate of change of stiffness with time, the m -value, are recorded, typically at a loading time of 60 seconds. A binder with low creep stiffness and a high m -value relaxes thermally induced stresses efficiently and resists low-temperature cracking. Modification strategies that toughen the binder at high temperature can inadvertently stiffen it at low temperature, so the BBR provides an essential counterbalance in the evaluation of any functional additive. The BBR is nonetheless labour-intensive, requires a comparatively large specimen, and imposes long conditioning times,

which has motivated the development of DSR-based surrogates. Using 4-mm parallel-plate geometry, the DSR can be operated at sub-zero temperatures to obtain a complex modulus and phase angle that are convertible, through mechanistic time–temperature relationships, into BBR-equivalent stiffness and m-value, thereby recovering the low-temperature grade from a much smaller specimen and a faster protocol (Kim et al., 2022). An alternative implementation adapts the DSR into a three-point bending configuration, allowing a beam test to be performed within the rheometer itself as a direct surrogate for the BBR (Kim et al., 2022). Studies on SBS-modified systems have confirmed that DSR-derived low-temperature parameters track the polymer's contribution to stress relaxation and can reproduce the ranking obtained from conventional BBR grading (Wang, Wei, Zhang, Shi, & Cheng, 2021).

Table 5.1. Rheological tests for modified asphalt binders

Test	Parameter	Property assessed
DSR (oscillation)	G^* , δ , $G^*/\sin \delta$	High-temperature stiffness
MSCR	J _{nr} , % recovery	Rutting, elastic recovery
BBR	S(t), m-value	Low-temperature cracking
LAS	Nf (VECD)	Fatigue resistance
Frequency sweep	Master curve, Glover-Rowe	Viscoelasticity, cracking risk

Beyond the specification parameters, oscillatory rheology in the DSR yields master curves of complex modulus and phase angle over wide ranges of frequency and temperature, constructed through the time–temperature superposition principle. These master curves, together with black-space and Cole–Cole representations, reveal the structural fingerprints of modification: the extended rubbery plateau

of a well-dispersed SBS network, the increased low-frequency modulus of a nano-reinforced binder, and the elevated phase angles that signal incompatibility or phase separation. The colloidal model of bitumen, in which asphaltene micelles are peptized within a maltene medium, provides the conceptual basis for interpreting these responses, because modification alters the balance of the colloidal system and hence the temperature dependence of the modulus (Lesueur, 2009). Frequency-sweep and temperature-sweep data are also used to quantify the softening effect of warm-mix additives and rejuvenators, which reduce viscosity at production temperatures to lower energy consumption and emissions while ideally preserving in-service stiffness (Behnood, 2020). Finally, the DSR is increasingly used to probe intrinsic self-healing, wherein a fatigue-damaged binder is allowed to rest and the recovery of modulus is monitored; such measurements have demonstrated that pure and modified bitumens recover a measurable fraction of their stiffness during rest periods, a capacity that functional modifiers can be designed to enhance (Qiu, van de Ven, Wu, Yu, & Molenaar, 2011). A further class of rheological descriptors derived from the master curve addresses the coupled problem of stiffness and relaxation capacity that governs non-load-associated cracking. Parameters constructed from the complex modulus and phase angle at an intermediate reference condition, most notably the Glover–Rowe parameter, locate a binder within black space and define damage thresholds beyond which block and surface cracking become likely. Because these parameters respond simultaneously to increases in modulus and to reductions in phase angle, they are especially informative for tracking the embrittlement that modification is intended to postpone and that ageing inevitably advances, and they connect the fresh-state rheology of the binder to its future durability. The interpretation of all such parameters, however, remains contingent on the compositional state of the binder, for the same

value of complex modulus can arise from very different colloidal structures and thus imply very different cracking susceptibilities, which is why rheological grading is most powerful when read together with the chemical and microstructural evidence developed later in this chapter (Polacco et al., 2015). Collectively, DSR, BBR, and MSCR testing furnish a coherent, physically grounded description of the binder across the full service-temperature range and form the indispensable first stage in the characterization of any modified asphalt system.

Mechanical and Durability Testing (rutting, fatigue, moisture damage)

While binder rheology establishes the intrinsic viscoelastic character of the modified material, the performance of a pavement is ultimately governed by the compacted mixture, in which the binder acts in concert with the aggregate skeleton, the mastic, and the air-void structure. Mechanical and durability testing at the mixture scale therefore closes the gap between fundamental binder properties and field behaviour, and it addresses the three dominant load- and environment-related distresses of flexible pavements: permanent deformation (rutting), fatigue cracking, and moisture-induced damage. The empirical and physical binder tests that complement the fundamental rheological methods are summarized in Figure 5.3, while the principal mixture-scale performance tests, their purpose, and their key outputs are compared in Figure 5.4.



Figure 5.3. *Physical and empirical binder tests, penetration, softening point, viscosity, density and adhesion, alongside the ageing tests that complement fundamental rheology.*

Rutting, the accumulation of unrecoverable shear and densification strain under repeated wheel loads at elevated temperature, is the distress most directly connected to the high-temperature binder parameters discussed above. At the mixture scale, the Hamburg wheel-tracking test has become the benchmark: a steel wheel is tracked repeatedly over a compacted specimen submerged in heated water, and the rut depth is recorded as a function of load cycles. Because the specimen is immersed, the test evaluates rutting and moisture susceptibility simultaneously, and the characteristic inflection point in the deformation curve, the stripping inflection point, marks the transition from load-driven deformation to moisture-driven degradation. Complementary triaxial and uniaxial repeated-load tests, along with the dynamic modulus test that generates the stiffness master curve used in mechanistic–empirical pavement design, provide the constitutive information needed to predict rutting analytically. The connection between

binder and mixture is well documented: functional modifiers that reduce the non-recoverable creep compliance (J_{nr}) of the binder generally translate into shallower ruts in the mixture, and nanomaterial modification in particular has been shown to increase mixture stiffness and rutting resistance by reinforcing the mastic and improving binder–aggregate adhesion (Cheraghian, Wistuba, Kiani, Barron, & Behnood, 2021). Warm-mix technologies must be scrutinized in this respect because the reduced production temperature can leave the binder incompletely aged and the mixture more rut-susceptible unless the modifier system compensates (Behnood, 2020). Beyond rut depth, the flow number obtained from repeated-load permanent-deformation testing and the phase-specific stiffness captured in the dynamic modulus master curve provide continuous, mechanistically interpretable measures of deformation resistance that can be embedded directly in pavement-response models, and they discriminate among modifier families more finely than a single terminal rut depth. Crumb-rubber modification illustrates the value of this multi-index approach: the swollen rubber particles both stiffen the mastic and impart elasticity, producing shallower ruts and improved high-temperature grades, yet the same particles influence workability, fatigue, and moisture response in ways that only a broad testing programme can resolve, and their benefit is contingent on the interaction between rubber and bitumen developing fully during digestion (Behnood, 2020; Cheraghian et al., 2021).

Test Type	Purpose	Typical Equipment	Key Output
Rutting Test (Wheel Tracking)	Evaluate rutting resistance under repeated loading		• Rut depth (mm) • PRDair / WTSair
Fatigue Test (4PB / SCB / IDEAL-CT)	Assess fatigue life and cracking resistance		• Fatigue life (cycles) • Strain at failure
Moisture Susceptibility (TSR / Lottman)	Determine moisture damage resistance		• Tensile Strength Ratio (TSR) • Retained strength
Low-Temperature Cracking Test (Thermal Stress)	Evaluate low-temperature cracking performance of mixtures		• Fracture temperature • Stiffness • m-value

Figure 5.4. Mixture-scale performance tests for rutting, fatigue, moisture susceptibility and low-temperature cracking, with their purpose and key outputs.

Fatigue cracking arises from the repeated application of tensile strains well below the material's monotonic strength, producing microcracks that coalesce over millions of load cycles. At the mixture scale, fatigue resistance is characterized through repeated flexural bending beam tests, direct or indirect tension cyclic tests, and, increasingly, fracture-mechanics-based approaches that quantify the energy required to propagate a crack. At the binder scale, the linear amplitude sweep (LAS) test has become the principal accelerated fatigue characterization method. In the LAS procedure, the binder is subjected in the DSR to a systematically increasing oscillatory strain amplitude, and the resulting damage accumulation is analysed within the viscoelastic continuum damage framework to predict fatigue life as a function of strain level (Hintz & Bahia, 2013). The LAS is especially valuable for modified binders because the polymer or rubber network can dramatically extend fatigue life in a manner that time-sweep testing captures only slowly

and that the classical $G^* \cdot \sin \delta$ parameter fails to represent. Fatigue tolerance is intimately linked to the binder's capacity for self-healing during rest periods; healing recovers a portion of the damage introduced during loading, and both the healing potential and its dependence on temperature and rest duration are measurable properties of the binder that modifiers can be engineered to improve (Tan, Shan, Kim, & Underwood, 2012). It is important to recognize, however, that ageing and physical hardening progressively embrittle the binder and diminish this favourable behaviour, so that the fracture characteristics of a polymer-modified binder measured shortly after production may overstate its long-term cracking resistance (Zhang, Shan, Xing, & Cui, 2023).

Table 5.2. *Mapping of distresses to characterization tests*

Distress	Binder-scale test	Mixture-scale test
Rutting	MSCR (Jnr)	Hamburg WTT, flow number
Fatigue	LAS	Four-point bending
Thermal cracking	BBR	TSRST / IDT
Moisture damage	N/A	TSR (AASHTO T 283)
Ageing	FTIR indices, DSR	RTFO / PAV plus performance

Moisture-induced damage, the loss of integrity that occurs when water infiltrates the mixture and disrupts the adhesive bond between binder and aggregate or the cohesive strength of the mastic, is the third principal durability concern and is often the mechanism that limits the field life of otherwise well-designed mixtures. The most widely used index is the tensile strength ratio (TSR), obtained by comparing the indirect tensile strength of moisture-conditioned specimens, subjected to vacuum saturation and freeze–thaw cycling,

with that of companion dry specimens; a low ratio signals a mixture prone to stripping. The TSR framework, standardized in the AASHTO T 283 protocol, remains the reference method against which modification strategies are judged, although its variability and its sensitivity to the conditioning regime have prompted continued refinement and the introduction of complementary parameters such as cohesion, dynamic modulus, and resilient modulus ratios (Movilla-Quesada, Raposeiras, Guíñez, & Frechilla-Alonso, 2023). Functional modifiers combat moisture damage through several mechanisms. Polymeric and recycled-plastic modifiers, when introduced through an appropriate process, can raise the TSR by stiffening the mastic and improving the binder's resistance to displacement by water, though the processing route strongly influences the outcome (Movilla-Quesada et al., 2023). Nanomaterials are particularly effective moisture-resistance enhancers because their high specific surface area promotes stronger, more hydrophobic binder–aggregate interfaces, and their incorporation has been shown to raise tensile strength ratios while simultaneously improving stiffness and thermal stability (Atiyah & Albayati, 2026). Environmental severity compounds the problem: in cold or de-icing environments, the combination of moisture, salt, and freeze–thaw action accelerates the deterioration of the binder–aggregate system and demands modifiers specifically formulated for such exposure (Zhang, Li, & Han, 2019). Because moisture, temperature, and ultraviolet exposure act simultaneously in the field, laboratory durability protocols increasingly attempt to reproduce combined climatic deterioration rather than isolated conditioning, which yields a more realistic ranking of modified mixtures under service-representative conditions (Sol-Sánchez, Moreno-Navarro, García-Travé, & Rubio-Gámez, 2015).

Microstructural and Chemical Analysis (SEM, FTIR, AFM)

Macroscopic rheological and mechanical performance is ultimately the emergent expression of phenomena occurring at the micrometre and nanometre scales: the dispersion and swelling of a polymer within the maltene phase, the distribution of nanoparticles across the mastic, the chemistry of oxidation, and the topography of the binder surface. Microstructural and chemical characterization techniques provide the mechanistic explanations that mechanical testing alone cannot, and they are indispensable for the rational design of functional modifiers because they reveal why a given additive succeeds or fails. Three techniques dominate contemporary practice: scanning electron microscopy (SEM) for morphology, Fourier-transform infrared spectroscopy (FTIR) for chemistry, and atomic force microscopy (AFM) for nanoscale topography and mechanics. These microstructural and chemical methods, together with X-ray diffraction, are summarized in Figure 5.5, and the complementary thermal-analysis techniques (DSC, TGA, and TMA) that probe transitions, stability, and dimensional behaviour are shown in Figure 5.6.

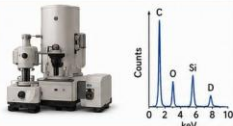
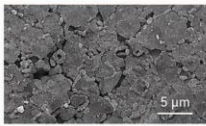
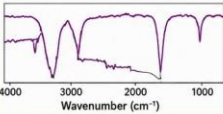
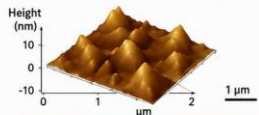
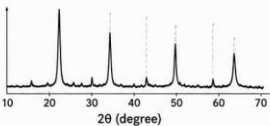
Technique	Instrument / Principle	Typical Output	Information Provided
SEM / EDS			- Morphology & dispersion of modifiers - Elemental composition - Filler–binder interaction
FTIR			- Functional groups - Chemical interactions - Aging indicators
AFM			- Surface topography - Phase separation - Nanostructure analysis
XRD			- Crystalline structure - Modifier crystallinity - Intercalation in clay

Figure 5.5. Microstructural and chemical characterization techniques, SEM/EDS, FTIR, AFM and XRD, that reveal the mechanisms behind bulk performance.

Scanning electron microscopy resolves the spatial organization of the modified binder and, in the case of polymer modification, the continuity and uniformity of the polymer network. In a compatible SBS-modified system, the polymer swells by absorbing the light aromatic fractions of the bitumen and forms a continuous, interpenetrating network that carries load in parallel with the asphalt phase; in an incompatible or poorly processed system, the polymer segregates into isolated domains that provide little reinforcement and are prone to storage instability. These morphologies, imaged by SEM or by fluorescence microscopy, correlate directly with the delayed elastic recovery measured in the MSCR test and with the extended rubbery plateau seen in the rheological master curves, thereby linking microstructure to performance. The theoretical basis for interpreting these images is the colloidal and thermodynamic understanding of asphalt/polymer

interaction, in which compatibility is governed by the relative solubility of the polymer in the maltene medium and by the tendency of the system toward phase separation (Polacco et al., 2015; Lesueur, 2009). This understanding has been extended through modelling of the phase-separation process itself: phase-field simulations reproduce the coarsening of polymer-rich domains during storage and the influence of processing conditions on the final morphology, providing a predictive complement to microscopy (Zhu, Lu, Balieu, & Kringos, 2016). More recent microscale investigations, integrating phase-field theory with experimental imaging, have clarified the kinetics by which a modifier develops its equilibrium structure within the binder and how that structure responds to thermal history (Liang, Chen, Jiao, & Wang, 2024). For nanomaterial-modified systems, electron microscopy is the primary means of confirming that the nanoparticles are exfoliated and homogeneously dispersed rather than agglomerated, because the reinforcing benefit of high specific surface area is realized only when dispersion is achieved (Cheraghian et al., 2021).

Fourier-transform infrared spectroscopy interrogates the chemical composition of the binder by measuring the absorption of infrared radiation at wavenumbers characteristic of specific molecular bonds. In the study of modified asphalt, FTIR serves two complementary purposes. First, it confirms and quantifies the presence of the modifier: SBS, for example, produces diagnostic absorption bands associated with the polybutadiene and polystyrene segments of the copolymer, and the intensity of these bands can be used to estimate polymer content and to detect the scission of the butadiene phase that accompanies degradation. Second, and more importantly for durability assessment, FTIR tracks the chemical evolution of the binder under ageing through the growth of the carbonyl band, near 1700 cm^{-1} , and the sulfoxide band, near 1030 cm^{-1} , which arise from the oxidation of the bitumen. The carbonyl

and sulfoxide indices, computed by normalizing these band areas against a stable reference, have become standard quantitative descriptors of oxidative ageing, and their evolution can be correlated with the loss of ductility and the increase in stiffness that accompany embrittlement. For composite-modified systems such as SBS/rubber binders, the simultaneous use of rheological indices and FTIR-derived chemical indices provides a robust, multi-parameter description of the ageing state that neither approach achieves alone, and the correspondence between the two classes of index strengthens the mechanistic interpretation of long-term behaviour (Chen et al., 2024). FTIR is likewise employed to verify the action of functional additives designed to alter binder chemistry, such as antioxidants that suppress carbonyl formation and phase-change or self-healing systems whose active constituents carry identifiable spectral signatures (Almutairi & Baaj, 2023).

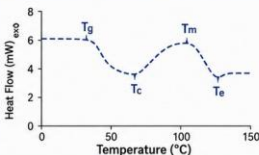
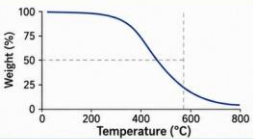
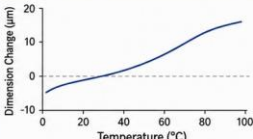
Technique	Instrument / Principle	Typical Output	Information Provided
DSC			• Glass transition (T_g) • Melting / crystallization • Degree of crystallinity • Compatibility
TGA			• Thermal stability • Degradation profile • Oxidative stability
TMA			• Thermal expansion • Softening behavior • Dimensional stability

Figure 5.6. Thermal analysis of modified binders by DSC, TGA and TMA, probing glass transition, thermal stability and dimensional behaviour.

Atomic force microscopy probes the binder at the nanometre scale, mapping surface topography and, in advanced modes, local mechanical properties such as adhesion, modulus, and energy dissipation. The most celebrated feature revealed by AFM in bituminous materials is the so-called bee structure, a pattern of alternating ridges and valleys on the binder surface whose chemical origin, variously attributed to the crystallization of waxes and to the segregation of asphaltenes, has been the subject of sustained debate. Beyond its intrinsic scientific interest, the bee structure is a sensitive marker of compositional change: in modified and aged binders, the size, number, and distribution of these features evolve in ways that reflect the underlying microstructure and the progress of oxidation. Peak-force quantitative nanomechanical mapping extends AFM from pure topography to the direct measurement of phase-specific stiffness, allowing the polymer-rich, asphaltene-rich, and maltene-rich domains to be distinguished by their mechanical response and enabling the reinforcing action of a modifier to be localized within the binder microstructure. When coupled with the chemical information from FTIR and the morphological information from SEM, AFM completes a multiscale characterization in which the nanoscale organization of the binder is connected to its bulk rheology and, through it, to the field performance of the mixture. The colloidal framework again provides the interpretive backbone, since the micellar organization of asphaltenes within the maltene medium is the structural feature that AFM ultimately visualizes and that modification perturbs (Lesueur, 2009). Together, SEM, FTIR, and AFM transform performance characterization from a purely phenomenological exercise into a mechanistic science, furnishing the cause-and-effect understanding required to engineer the next generation of functional, sustainable modifiers.

Aging and Long-Term Performance

Every property discussed in the preceding sections is time-dependent, because asphalt binders age. Ageing is the progressive, largely irreversible change in the physical and chemical state of the binder driven principally by oxidation, by the volatilization and migration of light components, and by physical hardening, and it proceeds throughout the material's life, from the moment of production through decades of service. Because ageing systematically stiffens and embrittles the binder, the durability and long-term performance of a modified asphalt mixture cannot be assessed from its properties in the fresh condition; it must be evaluated after representative ageing, and the effectiveness of any functional modifier must ultimately be judged by how well it preserves performance over time rather than by how it performs on the day it is placed. The systematic workflow that links material selection to laboratory characterization, mix design, and field application is outlined in Figure 5.7, and the multiscale structure–property–performance relationships that this workflow is designed to exploit are synthesized in Figure 5.8.

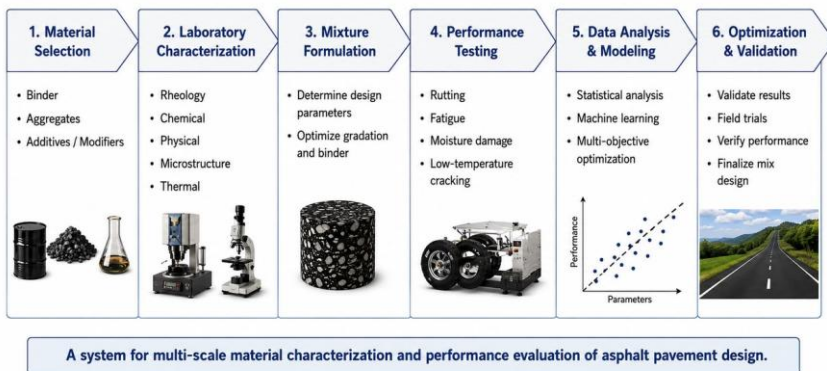


Figure 5.7. *Systematic characterization workflow that links material selection to laboratory testing, mix design and field application.*

Ageing is conventionally divided into two regimes that are reproduced by distinct laboratory protocols. Short-term ageing represents the intense but brief oxidation and volatilization that occur during hot mixing, transport, and compaction, and it is simulated by the rolling thin-film oven, which exposes a moving film of binder to heat and air for a controlled interval. Long-term ageing represents the slow oxidation that accumulates over years in service, and it is simulated by the pressure ageing vessel, which subjects short-term-aged binder to elevated temperature and pressure to compress years of field ageing into a matter of hours. The mechanistic driver in both regimes is the reaction of atmospheric oxygen with the binder to form polar, carbonyl- and sulfoxide-bearing functional groups, a process that can be followed at the level of the saturate, aromatic, resin, and asphaltene fractions and that shifts the colloidal balance toward a more asphaltene-dominated, more elastic, and more brittle state (Hu, Zhang, Wang, & Xu, 2020). Superimposed on thermal oxidation is photo-oxidation driven by ultraviolet radiation, which is particularly aggressive at the pavement surface and which conventional oven and pressure-vessel protocols do not reproduce; the ultraviolet ageing of bituminous materials is now recognized as a distinct and important degradation pathway that merits dedicated conditioning and that can dominate the deterioration of the uppermost binder film (Polo-Mendoza, Martinez-Arguelles, Walubita, & Moreno-Navarro, 2022).

The consequences of ageing pervade every performance dimension. As the carbonyl and sulfoxide indices rise, the creep stiffness measured in the BBR increases and the m-value falls, so that the low-temperature grade worsens and the risk of thermal cracking grows; the fatigue life inferred from the LAS test shortens

as the binder loses its capacity to relax and dissipate stress; and the intrinsic self-healing potential diminishes, because the mobility of the binder molecules that underlies healing is progressively lost (Sun, Ma, Sun, & Li, 2020). Modification interacts with these processes in ways that are not always favourable. Polymers themselves degrade under thermo-oxidative and photo-oxidative attack, with the butadiene phase of SBS being especially vulnerable to scission, so that the reinforcing network that confers rutting resistance and elastic recovery in the fresh state can be partially dismantled over time. The rational evaluation of a modified binder therefore requires ageing indices that are sensitive to both the bitumen and the modifier, and the combined use of rheological ageing indices and FTIR-based chemical indices has proven effective for tracking the deterioration of composite SBS/rubber systems across short- and long-term ageing (Chen et al., 2024). Physical hardening, a reversible stiffening that occurs at low temperature independent of oxidation, adds a further complication by transiently embrittling the binder and altering its fracture behaviour in ways that must be distinguished from true oxidative ageing (Zhang et al., 2023).

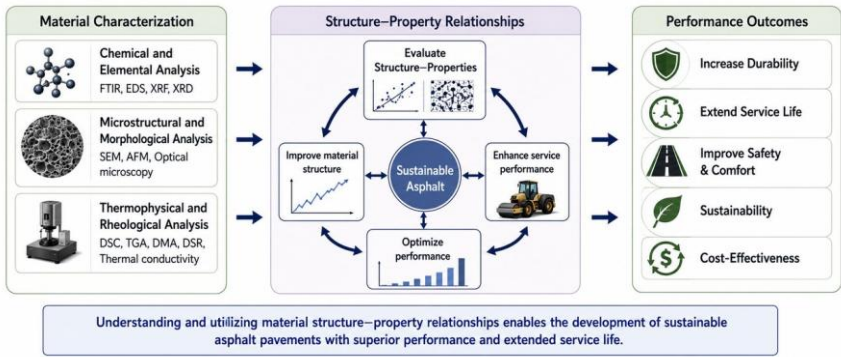


Figure 5.8. *Multiscale structure–property–performance relationships that connect binder chemistry and microstructure to the engineering behaviour of modified asphalt.*

These challenges have motivated two broad strategies for extending long-term performance. The first is chemical stabilization, in which antioxidant and stabilizing additives are incorporated to scavenge the free radicals that propagate oxidation and thereby to suppress the growth of the carbonyl and sulfoxide indices; when effective, such additives can multiply the ageing life of the binder and delay the onset of embrittlement, and their action is directly verifiable through the reduced rate of chemical index growth measured by FTIR. The second strategy is functional design for damage tolerance and recovery, exemplified by self-healing technologies that seek to reverse fatigue and thermal damage during rest periods rather than merely to resist its accumulation. The scientific literature on self-healing asphalt has grown rapidly and now encompasses intrinsic healing driven by molecular diffusion, extrinsic healing based on encapsulated rejuvenators, induction and microwave heating of magnetically susceptible fillers, and, most recently, the incorporation of dynamic covalent bonds whose reversible chemistry allows repeated crack closure and even material recyclability (Nalbandian, Carpio, & González, 2021; Chen & Zhang, 2024). Phase-change materials, polymers, and recycled mineral powders have been evaluated for their combined contribution to fatigue resistance and self-healing, illustrating the convergence of durability enhancement with the sustainability imperative of reusing waste streams (Almutairi & Baaj, 2023). Crucially, the durability benefit of any such technology must be demonstrated on aged material and under combined climatic exposure, because a modifier that performs admirably in the fresh, laboratory condition may lose its efficacy once the binder has oxidized and hardened in the field (Sol-Sánchez et al., 2015). Long-

term performance characterization thus unifies the preceding themes of this chapter: the rheological, mechanical, and microstructural tools described in Sections 5.1 through 5.3 acquire their full engineering value only when they are applied across the ageing continuum, tracing the evolution of the modified binder from production to the end of service life and providing the evidence base on which durable, sustainable flexible pavements are designed.

AUTHOR'S PERSPECTIVE

I trust a modified binder only after I have aged it. The Superpave rutting and fatigue parameters were built for neat binders and routinely mis-rank modified ones, so I lean on MSCR and the linear amplitude sweep, and I read them alongside FTIR ageing indices rather than in isolation. A material that shines on fresh, unaged specimens has told me almost nothing about how the pavement will behave in year eight; the honest question is always how well performance is preserved, not how high it starts.

CHAPTER SUMMARY

Chapter 5 surveyed the multiscale characterization of modified mixtures, from binder rheology (DSR, BBR, MSCR, LAS) through mixture mechanics and durability to microstructural and chemical analysis, all read across the ageing continuum.

Key findings

- ▶ Superpave parameters mis-rank modified binders; MSCR and LAS discriminate them far better.
- ▶ SEM, FTIR and AFM link microstructure and chemistry to bulk performance.
- ▶ Ageing and physical hardening progressively erode fresh-state benefits, so evaluation must be on aged material.

Design recommendations

- ▶ Grade modified binders with MSCR (Jnr, %R) and assess fatigue with the LAS.

- ▶ Track oxidation with the FTIR carbonyl and sulfoxide indices.
- ▶ Demonstrate durability on RTFO- and PAV-aged specimens, ideally under combined climatic exposure.

Future research

- ▶ Standardised performance-related tests tuned to modified and multifunctional binders.
- ▶ Test protocols that reproduce coupled moisture, thermal and UV ageing.

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CHAPTER 6

Thermal Behaviour of Functional Pavements: Conductivity, Heat Transfer and Nano-Enhancement

Flexible pavements are, in a very real sense, thermal machines. Every day they absorb solar radiation, store it, conduct it downward into the structure and the subgrade, and release it back to the atmosphere at night. The rate at which these exchanges occur, and the temperatures that develop within the bituminous layers as a result, govern much of what practising engineers care about: the rutting that appears when the mixture is soft and hot, the thermal cracking that opens when it is cold and brittle, the ageing of the binder, and increasingly the capacity of the pavement to perform additional "functions" such as harvesting energy, melting snow, or cooling the city around it. This chapter treats the pavement as a thermal system. It begins with the fundamental thermal properties of bituminous materials and how they are measured, moves to the heat transfer processes that produce temperature fields in the road, then examines how nanomaterials can be used to deliberately engineer

thermal conductivity, and closes with the functional applications that this thermal understanding makes possible.

Thermal Properties of Bituminous Materials and Their Measurement

Four intertwined properties describe how a bituminous material stores and transports heat. Thermal conductivity (k , in $\text{W/m}\cdot\text{K}$) is the rate at which heat is conducted through the material under a temperature gradient. Specific heat capacity (c , in $\text{J/kg}\cdot\text{K}$) is the energy required to raise the temperature of a unit mass by one degree, while volumetric heat capacity (ρc , in $\text{J/m}^3\cdot\text{K}$) expresses the same quantity per unit volume and is often the more useful form for a composite such as asphalt. Thermal diffusivity (α , in m^2/s) links the three through the relation $\alpha = k/(\rho c)$ and measures how quickly a temperature disturbance propagates rather than how much energy is stored; a high-diffusivity material reaches thermal equilibrium rapidly, whereas a high-heat-capacity material resists temperature change. These properties are not independent constants of "asphalt" in the abstract. They depend on the proportions and properties of the constituent phases, the mixture microstructure, temperature, and moisture state, and it is this dependence that makes the thermal characterisation of pavements both interesting and non-trivial (Bai, Park, Vo, Dessouky, & Im, 2015). Figure 6.1 summarises the principal factors, aggregate mineralogy, binder characteristics, porosity and air voids, temperature, moisture and additives, that govern the thermal conductivity of an asphalt mixture.

Consider the phases first. Bitumen itself is a poor conductor, with thermal conductivity of the order of $0.15\text{--}0.17 \text{ W/m}\cdot\text{K}$, and it has a relatively high specific heat. Mineral aggregate, which occupies the majority of the mixture volume, conducts far better, but the value depends strongly on mineralogy. Quartz-rich aggregates such as siliceous gravels are markedly more conductive than

carbonate rocks; crystalline quartz has an intrinsic conductivity many times that of limestone, so that mixtures built from quartzitic material tend to conduct heat more readily than otherwise similar mixtures built from limestone. Indeed, when the influence of composition on the effective conductivity of asphalt concrete is examined systematically using transient measurements, the aggregate source emerges as the single most influential variable, exceeding the effects of maximum aggregate size and air-void content (Demirtürk, Ozturk, & Guler, 2024). Air, the third phase, is an excellent insulator, and its presence as voids therefore lowers conductivity and volumetric heat capacity while altering the balance of storage and transport. Reported volumetric heat capacities illustrate the contrast between phases: air contributes on the order of only $1 \text{ kJ/m}^3\cdot\text{K}$, whereas bitumen and mineral matter contribute roughly 1.7 and $2.1 \text{ MJ/m}^3\cdot\text{K}$ respectively, so replacing solid with void has a pronounced diluting effect (Hassn, Aboufoul, Wu, Dawson, & Garcia, 2016).

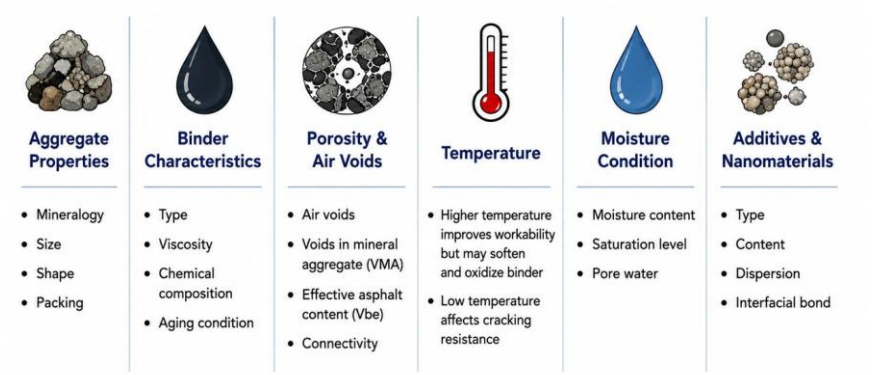


Figure 6.1. Factors that govern the thermal conductivity of an asphalt mixture, aggregate mineralogy, binder characteristics, porosity and air voids, temperature, moisture and additives.

The role of air voids has been studied in detail because it is one of the few thermal levers a mix designer can adjust indirectly. Denser mixtures store and conduct heat more effectively than porous ones; a porous asphalt slab, having lower specific heat capacity and lower conductivity, heats and cools more quickly and reaches higher peak temperatures than a dense-graded slab under the same radiant load (Hassn et al., 2016). The sensitivity is not uniform across the whole range, however. Within the compaction window typical of dense mixtures, roughly 4% to 6.5% air voids, the effect on conductivity is minor, so that ordinary construction variability does not swing thermal behaviour dramatically, whereas the large void contents of porous and open-graded materials do (Byzyka, Rahman, & Chamberlain, 2021). Moisture complicates the picture further: when voids fill with water, which itself conducts far better than air, both conductivity and heat capacity rise, so a wet pavement is thermally quite different from a dry one and simple dry-state values can mislead.

Temperature and ageing also matter. Thermal conductivity and diffusivity of asphalt mixtures vary appreciably with temperature, and the direction and magnitude of the change interact with the ageing state of the binder, so that laboratory values obtained at one temperature cannot be transferred uncritically to service conditions. Importantly, ageing has been shown to alter conductivity and diffusivity while leaving the specific heat capacity essentially unchanged, a decoupling that reflects the fact that heat storage is dominated by the mineral skeleton whereas conduction paths are sensitive to the binder film and microstructure (Byzyka et al., 2021).

Measurement is where much of the practical difficulty lies, and it deserves emphasis. Thermal-property methods divide broadly into steady-state and transient families. Steady-state techniques, of which the guarded hot plate is the classic example, impose a constant temperature gradient across a specimen and infer conductivity from

the equilibrium heat flux; they are accurate but slow, require large flat specimens, and are ill-suited to moist or heterogeneous materials because prolonged heating drives moisture migration. Transient techniques instead apply a controlled heat pulse and follow the temperature response in time, extracting several properties at once and in minutes rather than hours. The transient line-source (needle-probe) method energises a thin heated needle inserted into the specimen and fits the resulting temperature-time curve to obtain conductivity and diffusivity; thermal conductivity is commonly measured this way using portable transient line-source analysers such as the KD2 Pro, and it is against this background that nano- Al_2O_3 and graphene are of interest as effective conductivity enhancers, a theme developed in Section 6.3. The transient plane-source (hot-disk) method uses a flat spiral sensor sandwiched between two specimen faces and yields conductivity, diffusivity and volumetric heat capacity simultaneously; it has been applied successfully to laboratory-produced asphalt concrete and confirms the dominant role of aggregate source (Demirtürk et al., 2024). The laser flash method, used mainly for diffusivity of small homogeneous samples, fires a light pulse at one face and measures the temperature rise at the opposite face.

Table 6.1. *Thermal conductivity of pavement phases and mixtures*

Phase / material	k (W/m·K)	Thermal role
Bitumen	0.15-0.17	Poor conductor, high heat capacity
Air (voids)	~0.026	Insulator, lowers k and heat capacity
Water (saturated voids)	~0.6	Raises k and heat capacity when wet
Limestone aggregate	1.3-3	Carbonate, moderate conductivity
Quartz / siliceous aggregate	5-8	High; raises mixture conductivity

Phase / material	k (W/m·K)	Thermal role
Dense-graded asphalt	0.7-2.0	Depends on voids, aggregate, moisture
Porous asphalt	< dense-graded	High voids, higher peak temperature

None of these methods is free of artefacts when applied to a coarse, heterogeneous material like asphalt. Comparative studies show that steady-state and transient measurements on nominally identical asphalt concrete do not always agree, because the two approaches sample the microstructure differently and respond differently to contact resistance and specimen geometry (Demirtürk, Ozturk, & Guler, 2026). Transient probes are also sensitive to boundary effects: measurements taken near the edge of a slab specimen can differ substantially from those taken at the centre, so that probe placement and specimen size become part of the measured result rather than incidental to it. Because dedicated standards for the thermal testing of road materials remain sparse, careful attention to specimen preparation, probe contact, temperature control and measurement location is essential for reproducible data.

Taken together, these considerations explain why the thermal conductivity of asphalt mixtures is usually reported as a range rather than a single figure. Typical dense-graded asphalt falls in the region of about 0.7–2.0 W/m·K, with the lower end associated with high void contents, limestone aggregate and dry conditions, and the upper end with dense, quartz-rich, moist or conductively modified mixtures (Bai et al., 2015). Specific heat capacities of asphalt mixtures cluster around 0.8–1.0 kJ/kg·K and are comparatively stable, while diffusivity tracks the ratio of a variable conductivity to a relatively steady heat capacity. These baseline values are the input to every temperature-field calculation and every thermal-functional

design discussed in the remainder of the chapter, which is why their measurement warrants the care described here.

Heat Transfer and Temperature Fields in Flexible Pavements

The thermal properties of Section 6.1 acquire their engineering meaning only when they are placed inside the heat-transfer problem that defines the pavement temperature field. That field is the solution of a transient heat-conduction equation within the layered structure, driven by a boundary condition at the surface that couples the pavement to the atmosphere. Three transport mechanisms operate at that boundary, and all three must be represented to obtain realistic temperatures. Conduction carries heat downward through the asphalt, base and subgrade according to Fourier's law, so the depth profile of temperature depends directly on the conductivity and diffusivity discussed earlier. Convection exchanges heat between the surface and the moving air above it, at a rate that grows with wind speed and with the temperature difference between surface and air. Radiation acts in two directions: the pavement absorbs short-wave solar radiation in proportion to (one minus) its albedo, and it emits and receives long-wave radiation according to its emissivity and the temperature of the sky and surroundings. Figure 6.2 depicts these heat-exchange processes and the surface energy balance of the pavement, Figure 6.3 distinguishes the conduction, convection and radiation mechanisms at the scale of the asphalt microstructure, and Figure 6.4 shows how the resulting temperature field varies with depth over a daily cycle.

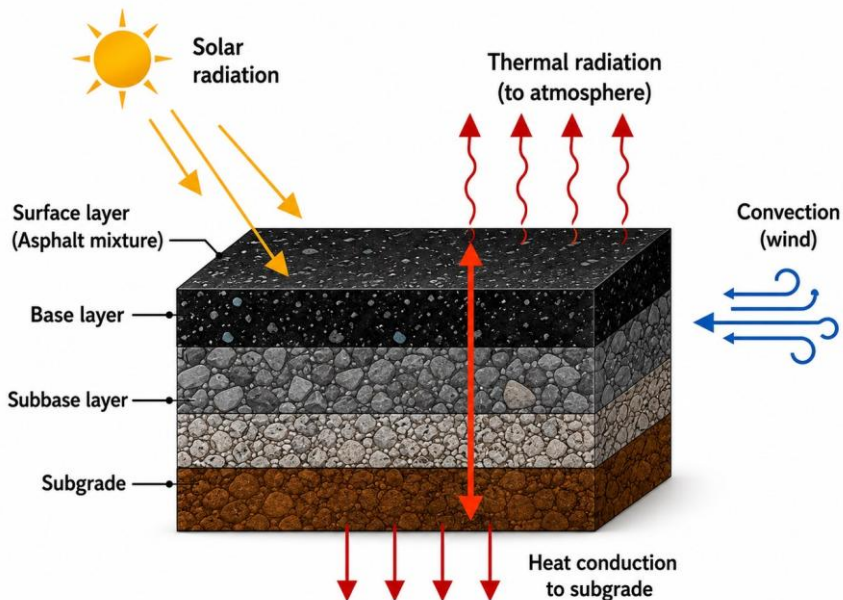


Figure 6.2. Heat-exchange processes and the surface energy balance of a flexible pavement, solar and thermal radiation, convective exchange with the wind, and conduction downward into the subgrade.

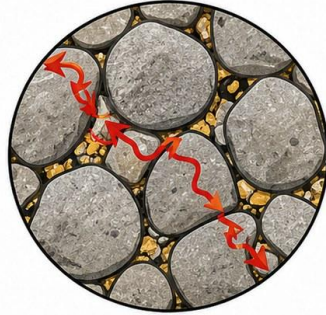
The surface energy balance ties these together. At any instant the net absorbed solar radiation, less the net long-wave emission, less convective loss, less the heat conducted into the body of the pavement, must sum to zero (or, more precisely, to the rate of change of stored surface energy). This balance is what makes surface temperature so responsive to material thermal properties. Because a pavement's surface temperature fluctuation scales inversely with the square root of the product of conductivity, volumetric heat capacity and density, raising any of these quantities lowers the daytime peak and raises the night-time minimum, flattening the diurnal swing. A dark, low-conductivity, low-heat-capacity surface therefore reaches the highest peak temperatures, whereas a denser or conductively

enhanced surface buffers the extremes (Hassn et al., 2016). Albedo enters the same balance through the absorbed solar term and is the principal lever behind the "cool pavement" strategies of Section 6.4 (Wong, Lim, Mohd Hasan, Sougui, Milad, & Qu, 2024).

The temperature field is inherently unsteady. On the diurnal scale, the surface leads a warming and cooling cycle whose amplitude decays and whose phase lags with depth, so that the bottom of a thick asphalt layer experiences a smaller, delayed version of the surface swing. On the seasonal scale, a slower thermal wave superimposes summer and winter envelopes on the daily cycle, and the subgrade a few tens of centimetres down remains far more stable than the surface, a gradient that will prove useful for energy harvesting. The lateral dimension is usually secondary but not always negligible; where the cross-section changes, as at part-cut, part-fill roadbeds in mountainous terrain, measurable lateral temperature differences develop across the width of the pavement and interact with the subgrade type (Han, Li, Wei, Yang, Wu, & Ouyang, 2024).

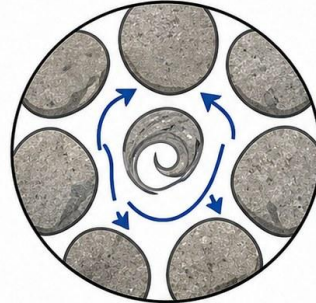
● Conduction

Heat transfer through solid particles and binder matrix.



● Convection

Heat transfer by the movement of air or fluid within the voids.



● Radiation

Heat transfer through electromagnetic waves emitted by the surface.

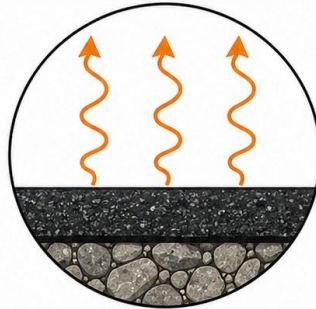


Figure 6.3. *Conduction, convection and radiation illustrated at the scale of the asphalt microstructure, the three modes by which heat moves through the pavement.*

Predicting this field has been approached both analytically and numerically. Closed-form analytical solutions, obtained by solving the conduction equation for a semi-infinite or layered medium under harmonic boundary forcing, are attractive because they expose the governing groups directly and can be evaluated

quickly; they have been derived, for example, for open-graded friction-course structures to give the temperature at any depth and time from the daily temperature and radiation inputs (Qi, Yu, Zhao, Zhang, & Zhang, 2023). Their limitation is that they demand idealised geometry and constant properties. Numerical methods relax these restrictions. Finite-difference schemes discretise the conduction equation in depth and time and are the traditional workhorse for one-dimensional temperature prediction. Finite-element models handle layered, temperature-dependent and multi-dimensional problems and are readily coupled to a subsequent stress analysis, so that a transient thermal solution feeds a quasi-static mechanical solution at each time step. Computational fluid dynamics extends the treatment to the convective and radiative boundary and to embedded fluid systems, resolving the air flow or the pipe flow explicitly rather than through a lumped coefficient; two-dimensional transient models that include conduction, convection and radiation together are now routinely used to design snow-melting and heated-pavement systems (Xu, Chen, Xiao, Zhu, & Wang, 2025). Across these approaches the required inputs are the same meteorological drivers, air temperature, solar radiation and wind speed, together with the layer thermal properties, and the fidelity of the prediction is limited as much by the accuracy of those property values as by the numerical scheme (Han et al., 2024).

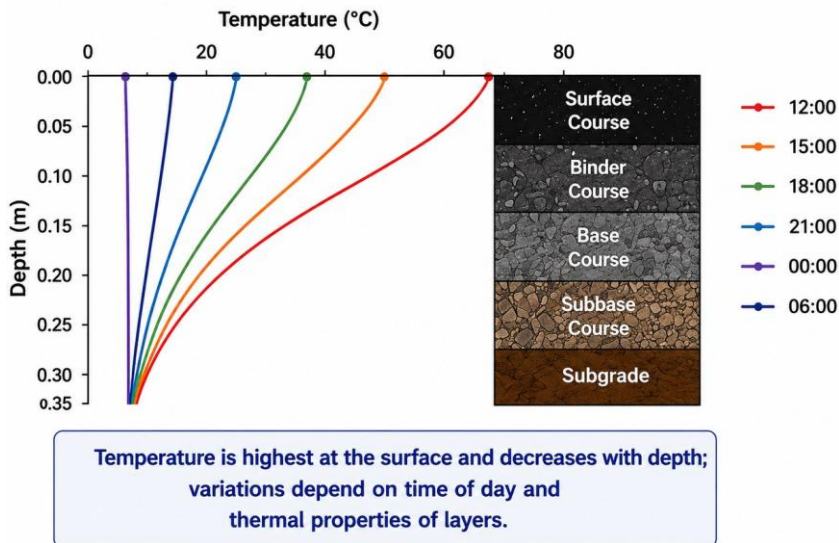


Figure 6.4. Temperature field with depth in a flexible pavement over a daily cycle, showing that the surface heats and cools far more strongly than the deeper layers.

The reason all of this effort is justified is that the temperature field is a direct cause of the two dominant thermally driven distresses. At the hot end of the range, high pavement temperatures soften the binder and lower the mixture's resistance to shear, so that repeated heavy, slow-moving loads accumulate permanent deformation; the equivalent stresses in the upper asphalt layer that drive rutting rise sharply as surface temperature increases, which is why rutting prediction is now commonly performed on a transient temperature field rather than a single design temperature. At the cold end, rapid cooling generates tensile thermal stresses in the surface layer that, when the mixture is stiff and its relaxation capacity exhausted, exceed the tensile strength and open low-temperature transverse cracks. A pavement that can be engineered to flatten its temperature swings, whether by adjusting albedo, conductivity or heat capacity, therefore attacks both distresses at once, and the tools

for doing so are the subject of the following sections. Accurate thermal characterisation and heat-transfer modelling are thus not academic exercises but the quantitative foundation on which durable, and increasingly multifunctional, pavement design rests.

Nano-Enhancement of Thermal Conductivity

Because bitumen is such a poor conductor, the effective conductivity of an ordinary mixture is limited by the binder-rich phase that separates the aggregate particles. The rationale for nano-enhancement is to build, within that binder phase, a continuous network of highly conductive inclusions that bridges the insulating gaps and provides preferential paths for heat flow. The candidate fillers span several families. Carbon nanomaterials, principally graphene, graphene nanoplatelets (GNPs), and carbon nanotubes (CNTs), combine extraordinarily high intrinsic thermal conductivity with high aspect ratio, which makes them efficient at forming conductive networks at low loadings (Li, Yu, Liang, & Wu, 2021). Metal-oxide and ceramic nanoparticles such as nano- Al_2O_3 raise conductivity more modestly but bring processing stability and rheological benefits. Coarser conductive additives, graphite powder, carbon fibres, steel fibres and conductive aggregates such as steel slag, are cheaper and can be dosed at high volume fractions, and they are frequently used in combination with the nanoscale fillers. Figure 6.5 illustrates the resulting gains, showing how the addition of nanomaterials such as silica, alumina, carbon nanotubes and graphene progressively raises the thermal conductivity of the mixture above that of the reference.

The efficiency of these fillers differs markedly, and the comparison is instructive. Reviewing the carbon-nanomaterial literature, graphene has been reported to be far more effective than carbon nanotubes on a like-for-like basis: an addition of about 5% graphene by volume of the matrix bitumen has produced increases

of roughly 300% in both thermal conductivity and thermal diffusivity at 20 °C, whereas the same volume of carbon nanotubes yielded increases of only about 72% (Li et al., 2021). The disparity reflects the two-dimensional, high-contact-area geometry of graphene platelets, which form thermal bridges more readily than the one-dimensional tubes. Studies that vary the platelet geometry directly confirm this, showing that larger-diameter, thicker platelets both raise conductivity more and lower the loading at which the network forms (Li et al., 2021). Metal oxides operate in a different regime; for nano-Al₂O₃ dispersed in bitumen, thermal conductivity has been found to increase almost linearly at a rate near 0.004 W/m·K per percent of nano-content, a smaller but reliable gain that comes together with improved high-temperature rheology (Broering, de Melo, & Manfro, 2024).

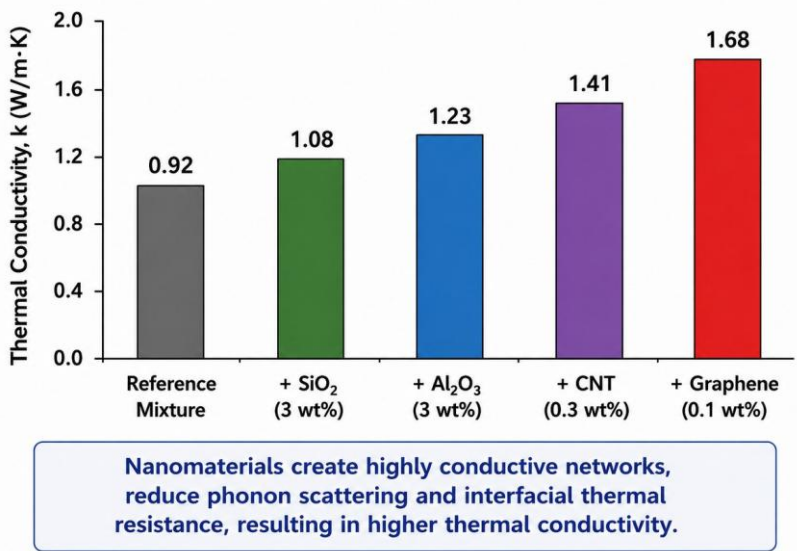


Figure 6.5. *Effect of nano-enhancement on the thermal conductivity of asphalt mixtures, with nano-oxides, carbon nanotubes and graphene progressively raising conductivity above the reference mixture.*

Central to all of this is the concept of a percolation threshold. Below a critical filler concentration the conductive inclusions remain isolated islands within the binder, and conductivity rises only gradually; once the concentration reaches the threshold at which the inclusions touch and form a continuous, sample-spanning network, conductivity climbs steeply before saturating. This thermal percolation behaviour has been demonstrated explicitly for graphene-nanoplatelet composites, where a rapid rise in conductivity accompanies the formation of a connected GNP network at the critical loading, and where larger platelets shift that threshold to lower concentrations (Jang, Nam, So, Lee, Kim, Kim, & Kim, 2022). The practical consequence is that dosage-conductivity relationships are strongly non-linear: adding filler below threshold buys little, adding it near threshold buys a great deal, and adding it well beyond threshold gives diminishing returns while imposing growing penalties. For coarser conductive fillers the same logic yields characteristic optimum contents, for example on the order of 15% graphite alone, or the far more economical combination of roughly 10% graphite with about 1% carbon fibres, where the fibres link otherwise isolated conductive regions and complete the network at low added cost (Bai et al., 2015). Combinations of graphene with carbon fibres similarly construct a more complete conductive network in asphalt mortar than either component alone (Wang, Tan, Liu, & Xu, 2021).

Table 6.2. *Conductive fillers and fluids for thermal enhancement*

Filler / fluid	Type	Typical content	Reported effect	Study
Graphene	2D carbon	~5 vol%	~+300 % k and diffusivity	Li et al. (2021)
Carbon nanotubes	1D carbon	~5 vol%	~+72 % k	Li et al. (2021)

Filler / fluid	Type	Typical content	Reported effect	Study
Graphene nanoplatelets	2D carbon	1-5 wt%	Steep rise past percolation	Jang et al. (2022)
Nano-Al ₂ O ₃	0D oxide	2-6 wt%	~+0.004 W/m·K per %	Broering et al. (2024)
Graphite powder	micro carbon	~15 wt%	Optimum standalone content	Bai et al. (2015)
Graphite + carbon fibre	hybrid	~10 % + 1 %	Economical percolating network	Bai et al. (2015)
Steel slag	conductive agg.	high vol%	Induction heating, self-healing	Yang et al. (2022)
Graphene nanofluid	pipe fluid	vol% in base	Leading heat-transfer fluid	Pavia et al. (2021)

These conductivity gains are not free of trade-offs, and honest design accounts for them. The same fillers that stiffen the binder and raise its rutting resistance tend to reduce its low-temperature relaxation capacity, so that thermal-cracking resistance can be degraded; conductive graphite and carbon black, for instance, improve the high-temperature rutting parameter while worsening low-temperature performance, and beyond certain contents the mixtures fall outside binder specification limits (Bai et al., 2015). High filler loadings can also raise air voids, complicate compaction and dispersion, and increase cost, while nano-Al₂O₃ has been observed to impair fatigue tolerance at intermediate temperatures once its content exceeds a few percent even as it benefits high-temperature behaviour (Broering et al., 2024). Dispersion quality is itself a decisive variable, since agglomerated nanoparticles neither percolate efficiently nor reinforce uniformly; graphene and CNT modification improves conductivity to a real but limited degree

precisely because achieving ideal dispersion in a viscous bitumen is difficult (Yu, Zadshir, Yan, & Yin, 2022). Ageing behaviour is a further consideration, and here some fillers are benign: nano- Al_2O_3 blends physically with the binder and has been reported to inhibit the growth of ageing-related functional groups, so that thermal enhancement and durability need not be in conflict (Broering et al., 2024).

A related but distinct use of nanomaterials concerns the heat-transfer fluid rather than the solid mixture. In pavements that embed a network of pipes, the working fluid can itself be a nanofluid, a base liquid such as water or ethylene glycol carrying a suspension of conductive nanoparticles. Graphene, owing to its exceptional intrinsic conductivity, is regarded as the leading candidate for engineering such fluids, outperforming metal-oxide particles and carbon nanotubes on a conductivity basis, although its dispersion and stability require care (Pavía, Alajami, Estellé, Desforges, & Vigolo, 2021). Alumina nanofluids are the most extensively studied of the metal-oxide systems and provide well-characterised, moderate enhancements that scale with volume fraction and temperature and improve with smaller particle size (Sridhara & Satapathy, 2011). Hybrid formulations that combine graphene with alumina aim to marry the high conductivity of the former with the stability of the latter. By raising the conductivity of the circulating medium, such nanofluids increase the rate at which heat can be delivered to, or extracted from, the pavement in the embedded-pipe systems discussed next, closing the loop between material-scale nano-enhancement and system-scale thermal function.

Thermal-Functional Applications

Once a pavement is understood, and can be engineered, as a thermal system, a family of functional applications becomes available in which the road ceases to be a passive surface and

becomes an active thermal device. The most direct is energy harvesting. A pavement surface that reaches 60–70 °C under summer sun while the soil a short distance below stays near 27–33 °C presents a persistent vertical temperature gradient, and this gradient can be converted to electricity through the Seebeck effect using thermoelectric generators whose hot and cold junctions straddle the two thermal reservoirs (Zhu, Yu, & Li, 2019). Prototype road thermoelectric systems embed the generator in or beside the pavement, drawing the cold side from the subgrade, the ambient air, or flowing water, and produce modest but maintenance-free power suitable for sensors and lighting; because they contain no moving parts and can be sited outside the wheel path, they interfere little with traffic or resurfacing (Tahami, Gholikhani, Nasouri, Dessouky, & Papagiannakis, 2019). A complementary hydronic form of harvesting circulates a fluid through pipes in the asphalt to collect solar heat in summer for storage or use, effectively turning the road into a large solar collector (Pan, Wu, Xiao, & Liu, 2015). Figure 6.6 collects the principal thermal-functional applications, from heat-island mitigation and thermal regulation to heated pavements, energy efficiency and climate resilience, and Figure 6.7 points to the emerging directions, advanced nanomaterials, phase-change materials, and smart, self-regulating thermal systems, that are shaping the field.

The same hydronic infrastructure, run in reverse in winter, provides snow melting and de-icing. Warm fluid, potentially heated by stored solar or geothermal energy, is pumped through the embedded pipe network to raise the surface above freezing and prevent ice bonding, an approach reviewed extensively as a sustainable alternative to chemical de-icers, which are corrosive and environmentally damaging (Pan et al., 2015). The thermal performance of such systems is governed precisely by the heat-transfer principles of Section 6.2: melting time falls as the

circulating-fluid temperature rises, as the pipes are placed closer to the surface, and as the conductivity of the surface layer increases, though higher fluid temperatures also raise energy consumption, so design is an optimisation rather than a maximisation (Xu, Chen, Xiao, Zhu, & Wang, 2025). This is exactly where the conductive fillers and nanofluids of Section 6.3 pay off, because a more conductive mixture and a more conductive working fluid deliver heat to the surface faster and more efficiently. Electrical variants, which pass current through conductive asphalt or embedded cables to generate resistive heat, follow the same logic and likewise benefit from enhanced mixture conductivity (Xu et al., 2025).

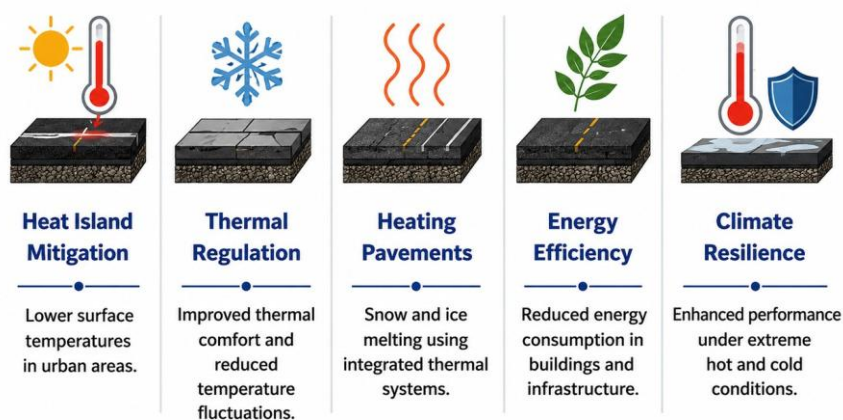


Figure 6.6. Thermal-functional applications of conductive and responsive pavements, heat-island mitigation, thermal regulation, heated pavements, energy efficiency and climate resilience.

A third application inverts the objective, seeking not to add heat but to reject it, in the interest of urban-heat-island mitigation. Conventional dark asphalt has low albedo and absorbs the great majority of incident solar radiation, driving up surface and near-surface air temperatures in cities. Cool, high-albedo pavements reflect more of that radiation and so run cooler; heat-reflective

coatings applied to asphalt have lowered surface temperatures by several degrees in controlled evaluations, with the benefit diminishing under wind and depending on coating formulation and location (Lu, Rahman, Moore, & Golrokh, 2022). Systematic review of field and laboratory studies confirms that heat-reflective asphalt pavements do reduce the heat-island effect, while cautioning that their effectiveness varies with pavement type, siting and material choice, and that reflected radiation can raise pedestrian-level thermal load, so albedo must be traded against other comfort criteria (Wong et al., 2024). Cool-pavement strategies thus act directly on the absorbed-solar term of the surface energy balance introduced earlier.

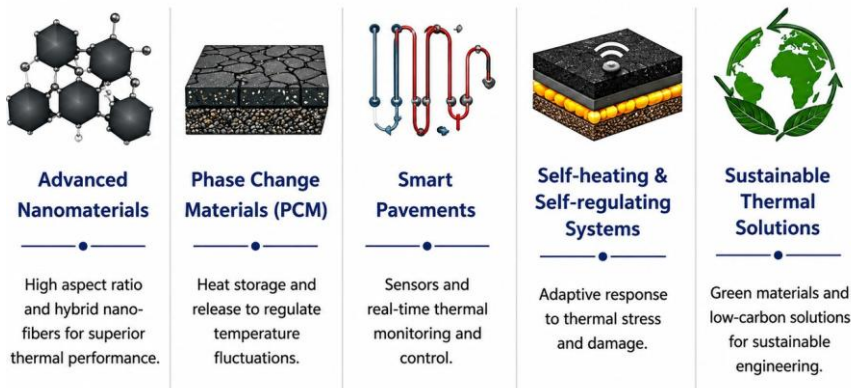


Figure 6.7. *Emerging directions in thermal-functional pavement materials, advanced nanomaterials, phase-change materials and smart, self-regulating thermal systems.*

Thermal and electromagnetic conductivity also enable self-healing, one of the most compelling functional uses of conductive and magnetic fillers. Bitumen heals microcracks when it is warmed enough to flow and re-wet the crack faces, and the difficulty is delivering that heat locally and on demand. Induction heating supplies it by exposing steel fibres or other electrically conductive

inclusions in the mixture to a high-frequency alternating field, which induces eddy currents that heat the particles and, through them, the surrounding mastic, closing incipient cracks before they propagate. Microwave heating achieves a similar end through dielectric and magnetic loss, and is greatly accelerated by ferromagnetic or high-loss fillers. Steel slag, rich in Fe_2O_3 and other metal oxides with favourable electromagnetic parameters, has been shown to enhance both induction heating and self-healing in recycled asphalt mixtures, coupling waste valorisation to functional performance (Yang, Wu, Xie, Amirkhanian, Liu, Zhang, Xiao, Zhao, Xu, & Li, 2022). Magnetite filler used as a replacement for mineral filler similarly improves microwave heating rate and healing efficiency, raising fracture toughness across repeated damage-heal cycles while also improving moisture resistance (Ameri & Sadeghiavaz, 2025). In each case the same raised thermal and electromagnetic conductivity that makes a pavement a good heat-harvester or snow-melter also makes it a good self-healer, so these functions reinforce one another rather than competing.

Finally, thermoregulation can be built into the material itself through phase-change materials (PCMs) and thermochromic coatings. A PCM incorporated into the mixture absorbs a large quantity of latent heat as it melts near a chosen transition temperature and releases it on freezing, so that it acts as a thermal buffer that clips the peaks and troughs of the diurnal cycle. Encapsulated PCMs have delayed the initial temperature rise of asphalt by several degrees and reduced peak pavement temperatures by a few degrees, directly attacking high-temperature rutting, and can be tuned with eutectic formulations to target specific transition temperatures, sometimes with an added conductivity enhancer to speed heat exchange (Zhang, Sani, Xu, Liu, & Gu, 2023). Because the same latent-heat mechanism moderates cold-side excursions, PCMs also offer benefits for low-temperature cracking and freeze-thaw durability,

and their capacity to lower surface temperature links them to heat-island mitigation as well (Pinheiro, Landi, Lima, Ribas, Hammes, Segundo, Homem, Castelo Branco, Freitas, Costa, & Carneiro, 2023). Thermochromic coatings extend the idea to the optical domain, changing colour and thus albedo with temperature so that the surface reflects more in the heat and absorbs more in the cold. Taken as a whole, these applications show that the thermal understanding developed through this chapter, from the measurement of a mixture's conductivity to the modelling of its temperature field and the nano-engineering of its conductive network, is what transforms a flexible pavement from an inert riding surface into a genuinely functional, and more sustainable, component of the built environment.

AUTHOR'S PERSPECTIVE

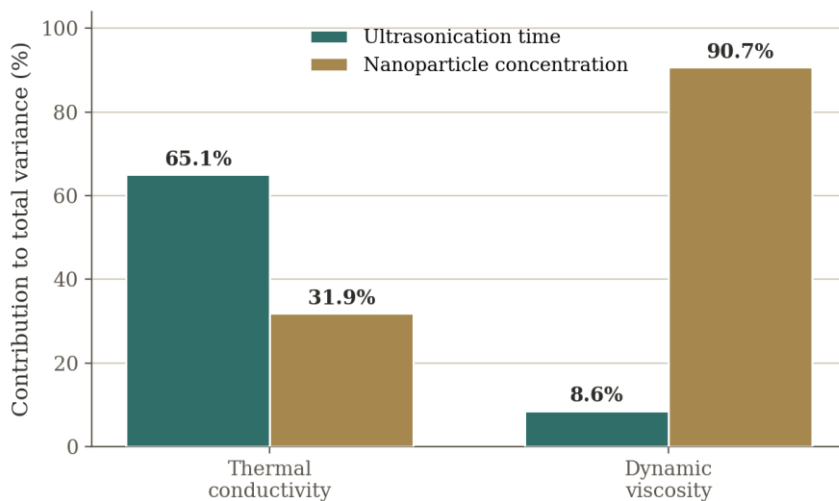
Thermal conductivity is the property I would measure first and trust least when it is borrowed from the literature. Because it depends so strongly on aggregate mineralogy, air voids and moisture, a value taken from another study is nearly useless for design, so I measure it directly on the actual mixture with a transient line-source probe such as the KD2 Pro. When conductivity must be raised, a few percent of graphene or nano-Al₂O₃ is far more effective per unit mass than metal-oxide micro-fillers, but only once the percolation threshold is crossed, which is why I design to the network rather than to the dose. The same conductive network that harvests energy or melts snow also enables induction self-healing, so thermal design is rarely about a single function.

Engineered Working Fluids for Hydronic Thermal-Functional Pavements: An Experimental Perspective

The thermal-functional applications of the preceding section share a common architecture. Many of them, energy-harvesting

pavement solar collectors, hydronic snow-melting and de-icing systems, and geothermally coupled pavements, operate by circulating a working fluid through a pipe network embedded in the asphalt (Pan et al., 2015). In such systems the rate at which heat is collected, stored or delivered is limited not only by the conductivity of the surrounding mixture, treated in Section 6.3, but equally by the thermophysical properties of the circulating fluid itself, so that a fluid which conducts heat poorly or stores little of it caps the performance of an otherwise well-designed collector. This section draws on the authors' own experimental programme on the thermophysical characterisation of heat-transfer fluids, carried out with the transient hot-wire (KD2 Pro) method introduced in Section 6.1, to show that the working fluid can be engineered as deliberately as the solid pavement, and that the same design principles govern both.

The simplest route is to disperse conductive nanoparticles in a conventional base fluid to form a nanofluid. Across several systems the authors have measured consistent, if moderate, gains in thermal conductivity. Silver-oxide (Ag_2O) nanoparticles in water raised the conductivity by as much as 27.2% at a loading of only 0.10 vol% once the dispersion was optimised (Ibrahim & Doruk, under review), while alumina (Al_2O_3) dispersed in an ionic-liquid base fluid improved the conductivity of the resulting ionanofluid by roughly 11% (Altun, Doruk, & Şara, 2023). These enhancements are obtained at very low solid fractions, echoing the low-dosage principle that governs nano-modification of the binder in Section 6.3, and they confirm that a nanofluid coolant can move heat to or from a pavement surface faster than the base fluid alone.



Analysis of variance for Ag₂O/water nanofluids (dispersion vs. dosage)

Figure 6.8. *Relative influence of ultrasonication time and nanoparticle concentration on the thermal conductivity and viscosity of Ag₂O/water nanofluids, showing that dispersion quality governs conductivity while particle loading governs viscosity.*

The decisive variable, however, is not the quantity of nanoparticle added but the quality and stability of its dispersion. An analysis of variance on the Ag₂O/water system separates the two effects cleanly. Ultrasonication time, a proxy for dispersion quality, accounted for about 65% of the variation in thermal conductivity, whereas nanoparticle concentration accounted for only about 32%; the picture inverts for viscosity, which was governed almost entirely, some 91%, by particle loading (Figure 6.8; Ibrahim & Doruk, under review). Complementary studies on surfactants reinforce the point, since the stability of Al₂O₃/water nanofluids depended sensitively on both surfactant dosage and particle concentration (Altun, Şara, & Doruk, 2022), and for TiO₂/water fluids the ionic character of the surfactant, anionic, cationic or non-ionic, controlled the dispersion state and hence the overall performance (Ali & Doruk, under

review). The lesson mirrors the binder-modification principle stated earlier in this chapter, that dispersion, not dosage, decides the outcome, and it argues for zeta-potential and stability screening as a condition of acceptance for any pavement working fluid.

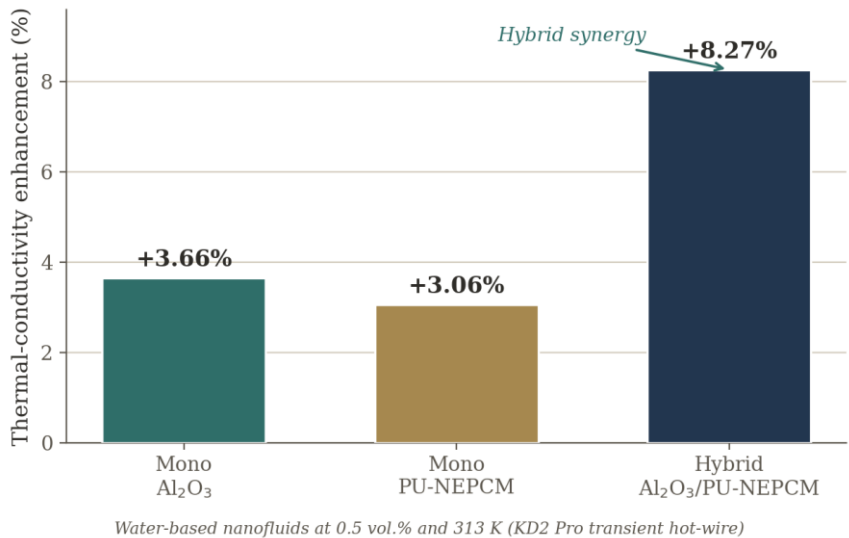


Figure 6.9. Thermal-conductivity enhancement of mono Al₂O₃, mono PU-NEPCM and their hybrid nanofluid at 0.5 vol% and 313 K, demonstrating the synergistic gain of the hybrid formulation.

Conductivity is only half of the thermal picture. Because a hydronic pavement must store as well as transport heat, a working fluid that also carries a large latent-heat capacity is especially valuable, and this is achieved by suspending nanoencapsulated phase-change material (NEPCM) in the base fluid. The authors encapsulated n-nonadecane, whose melting point lies conveniently near ambient pavement temperatures, within polymer shells and dispersed it to form latent functionally thermal fluids. Surface functionalisation of the capsules produced a highly stable suspension, with a zeta potential of -56.8 mV that maintained dispersion without any added surfactant, while simultaneously

raising both the thermal conductivity and the effective heat capacity of the fluid (Karaipekli, Erdoğan, & Barlak, 2019); an earlier NEPCM nanofluid raised the conductivity by about 13% at 5 vol% (Barlak, Sara, Karaipekli, & Yapıcı, 2016). Such a fluid buffers the diurnal temperature swing in the same way that a PCM embedded in the mixture does, but with the added advantage that the stored heat can be pumped to where it is needed.

The two strategies, conductive nanoparticle and latent nanocapsule, can be combined. A hybrid fluid pairing Al_2O_3 with polyurethane-encapsulated n-nonadecane outperformed either component alone: at 0.5 vol% and 313 K the hybrid raised thermal conductivity by 8.27%, against 3.66% and 3.06% for the corresponding mono-alumina and mono-NEPCM fluids, a clear synergistic gain, while retaining colloidal stability (Figure 6.9; Doruk, 2026). These bench-scale property gains translate to system performance, for when an NEPCM nanofluid was circulated through a double-pipe heat exchanger the overall heat-transfer coefficient improved by about 10% at the highest loading tested (Doruk, Şara, Karaipekli, & Yapıcı, 2017), showing that the measured enhancements survive integration into a flowing device.

Table 6.3. *Summary of the experimental thermophysical studies on nanofluids and NEPCM-based working fluids*

System / base fluid	Method	Key experimental result
Ag ₂ O-water nanofluid	KD2 Pro, Taguchi	+27.2% k at 0.10 vol%, 120 min; dispersion over dosage
Al ₂ O ₃ /PU-NEPCM hybrid	KD2 Pro, ANOVA	+8.27% k (hybrid) vs 3.66/3.06% mono; synergy
NEPCM (n-nonadecane) nanofluid	KD2 Pro	+13% k at 5 vol%; latent plus sensible heat
NEPCM in double-pipe exchanger	Device test	+10% overall heat-transfer coefficient at 1.68 vol%

System / base fluid	Method	Key experimental result
Surface-functionalized NEPCM (LFTF)	KD2 Pro, zeta	Zeta -56.8 mV, surfactant-free stability; higher k and cp
Al ₂ O ₃ -water + SDS	Stability, zeta	Stability governed by surfactant and particle loading
TiO ₂ -water + SDS/CTAB/Tween-80	KD2 Pro, PI	Surfactant character controls dispersion and performance
Al ₂ O ₃ /ionic-liquid (NEIL)	KD2 Pro	+11% k at 2.5 wt%

Table 6.3 summarises this body of experimental work. Read together, the results define a design template for the fluid side of thermal-functional pavements: a low-loaded, well-dispersed, electrostatically stable suspension that couples a conductive nanoparticle for sensible-heat transport with a nanoencapsulated PCM for latent storage offers the best balance of conductivity and heat capacity against the unavoidable viscosity and pumping penalty. Equally important is the methodological continuity, because the transient hot-wire (KD2 Pro) protocol, the dispersion and stability discipline, and the dosage-performance reasoning developed for these fluids are the same tools required to characterise and optimise the nano-modified binders and mixtures of Sections 6.1 and 6.3. The studies summarised here were conducted on the heat-transfer fluids themselves rather than on asphalt specimens, and their translation into field pavement collectors still demands attention to pipe integration, long-term fluid stability under thermal cycling, and pumping energy, which remain open engineering questions and a natural direction for coupling this thermophysical expertise to full pavement systems.

CHAPTER SUMMARY

Chapter 6 treated the pavement as a thermal system: it defined the thermal properties of bituminous materials and how to measure them, the heat-transfer processes that produce the temperature field, the nano-enhancement of thermal conductivity, and the thermal-functional applications this understanding enables.

Key findings

- ▶ Thermal conductivity of asphalt (about 0.7-2.0 W/m·K) depends strongly on aggregate mineralogy, air voids and moisture and is best measured by transient methods such as the KD2 Pro.
- ▶ The surface energy balance and the temperature field directly drive rutting and thermal cracking.
- ▶ Graphene and nano-Al₂O₃ raise conductivity efficiently, but only once the percolation threshold is crossed, and with mechanical trade-offs.

Design recommendations

- ▶ Measure conductivity on the actual mixture rather than borrowing literature values.
- ▶ Design conductive modification to the percolating network, checking low-temperature and fatigue penalties.
- ▶ Exploit the same conductive network for energy harvesting, snow melting and induction self-healing together.

Future research

- ▶ Dedicated standards for the thermal testing of road materials.
- ▶ Coupled thermo-mechanical, multifunctional pavement design and durable nanofluid systems.

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CHAPTER 7

Sustainability and Life-Cycle Assessment of Functional Pavement Materials

The transition toward sustainable flexible pavements cannot be evaluated on the basis of mechanical performance alone. A functional material that delivers superior rutting resistance, fatigue endurance, or self-healing capacity may nonetheless impose a substantial environmental burden if its manufacture is energy-intensive, if it depletes scarce virgin resources, or if it complicates end-of-life recovery. Conversely, a material that appears environmentally attractive at the production gate may prove disadvantageous over a full service life once maintenance frequency, durability, and use-phase interactions are accounted for. The central argument of this chapter is therefore that the sustainability of functional pavement materials must be judged holistically, across the entire life cycle and across the interlocking environmental, economic, and social dimensions of the "triple bottom line." This chapter develops the conceptual and methodological apparatus

required for such an evaluation. Section 7.1 introduces the indicators and rating frameworks used to operationalize sustainability in pavement engineering. Section 7.2 sets out the standardized life-cycle assessment (LCA) framework and its methodological subtleties. Section 7.3 extends the analysis to economic evaluation through life-cycle cost analysis (LCCA) and considers how environmental and economic metrics can be integrated. Section 7.4 synthesizes the preceding material through case studies and comparative analyses drawn from the recent literature on recycled, warm-mix, rubberized, plastic-modified, and alternative-binder pavements.

Sustainability Indicators in Pavement Engineering

Sustainability in pavement engineering is conventionally framed through the three interdependent pillars of environmental protection, economic viability, and social well-being. Translating this abstract framing into engineering practice requires measurable indicators, quantities that can be computed, compared across design alternatives, and ideally aggregated into decision-support metrics. The environmental pillar is typically expressed through indicators such as global warming potential (usually reported as kilograms of carbon dioxide equivalent), cumulative energy demand, acidification and eutrophication potential, particulate-matter formation, water consumption, and the depletion of abiotic resources. The economic pillar is captured by agency costs, user costs, and residual asset value, all discounted to present value over an analysis period. The social pillar, historically the least developed, encompasses considerations such as construction-related traffic disruption, worker health and safety, noise exposure, and equity of access (Styer, Tunstall, Landis, & Grenfell, 2024). A recurring observation in the recent literature is that the environmental and social dimensions have received disproportionate attention relative to the economic

dimension in formal rating instruments, a structural imbalance that complicates genuinely integrated decision-making (Mehraban, Tsantilis, Riviera, & Santagata, 2025). Figure 7.1 presents the three pillars, environmental, economic and social, whose intersection defines a sustainable pavement.

For flexible pavements specifically, several indicators carry particular engineering significance because they connect material properties to system-level environmental outcomes. The proportion of recycled content, most importantly reclaimed asphalt pavement (RAP), but also crumb rubber from end-of-life tires, waste plastics, and industrial by-products such as slag or bottom ash, serves as a proxy for both resource conservation and the avoidance of virgin binder and aggregate extraction. Production and compaction temperature is a second key indicator, because the energy required to heat and dry aggregates dominates the manufacturing footprint of hot-mix asphalt; warm-mix and cold technologies reduce this burden directly. Durability and expected service life form a third indicator class, since a longer-lasting pavement amortizes its embodied impacts over more years and fewer rehabilitation cycles. Functional surface characteristics, including smoothness (which governs pavement–vehicle interaction and hence vehicle fuel economy), noise emission, and solar reflectance, connect the material to use-phase impacts that can dwarf production impacts on high-volume roads (Xu, Akbarian, Gregory, & Kirchain, 2019). A comprehensive indicator framework must therefore span the material, the structure, and the road-user domains simultaneously.

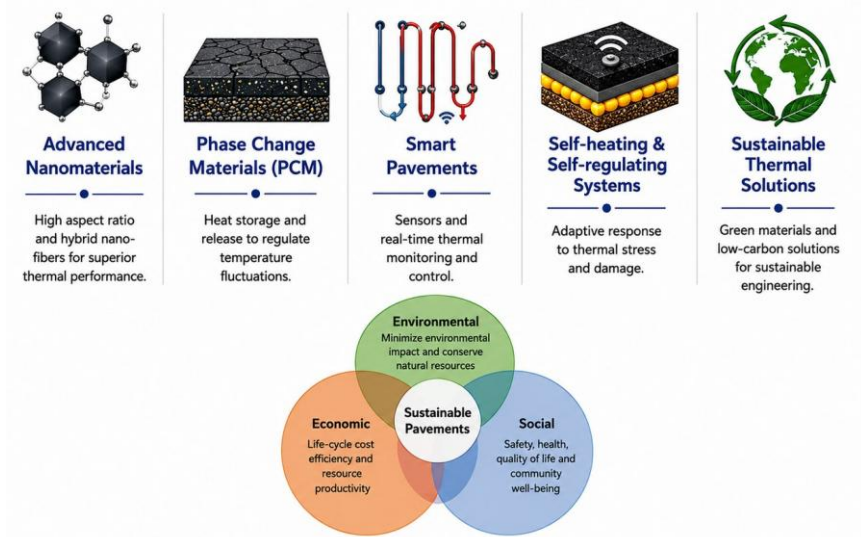


Figure 7.1. *The three pillars of sustainability, environmental, economic and social, whose intersection defines a sustainable pavement.*

Because engineers require guidance rather than an undifferentiated list of metrics, a family of sustainability rating systems has emerged to structure and weight these indicators. Systems such as Greenroads, GreenLITES, INVEST, I-LAST, BE2ST-in-Highways, CEEQUAL, GreenPave, and Envision assign credits for sustainable design and construction practices and, in several cases, permit third-party certification of projects (Mehraban et al., 2025). Greenroads, developed through research at the University of Washington, organizes credits into categories spanning environment and water, materials and resources, construction activities, access and equity, and pavement technologies, and it awards specific credits for low-noise surfaces measured by the on-board sound intensity method and for high solar-reflectance pavements that mitigate the urban heat-island effect. Envision, by contrast, adopts a broader whole-of-life-cycle and infrastructure-systems perspective. A comparative analysis of eight leading rating

systems found that they collectively emphasize environmental well-being (approximately 43% of credit weight) and social well-being (approximately 42%), while economic well-being receives markedly less emphasis (approximately 15%), and that alignment with international standards such as ISO, EN, and ASTM varies considerably among systems (Mehraban et al., 2025). This heterogeneity means that a project judged "sustainable" under one rating system is not necessarily rated equivalently under another, which underscores the value of transparent, physically grounded indicators derived from life-cycle analysis rather than reliance on any single scoring instrument.

Table 7.1. *Sustainability indicators in pavement engineering*

Dimension	Indicator	Example metric
Environmental	Energy and emissions	GWP (kg CO ₂ -eq), embodied energy
Resource	Material circularity	% recycled, reclaimed content
Economic	Life-cycle cost	Agency plus user cost (NPV)
Functional	Durability	Service life, maintenance interval
Social	Externalities	Noise, safety, congestion

A complementary and increasingly consequential mechanism for standardizing environmental indicators is the environmental product declaration (EPD). An EPD is a verified, standardized report of the quantified life-cycle environmental impacts of a specific product, functioning as an environmental "nutrition label" that enables comparison between products fulfilling the same function. For asphalt mixtures, EPDs are typically cradle-to-gate in scope, encompassing raw-material extraction, transport to the plant, and

plant operations up to the point at which the mixture leaves the facility. In North America, the National Asphalt Pavement Association's Emerald Eco-Label program provides a verified EPD tool developed in conformance with ISO 14025, ISO 21930, and the applicable product category rules for asphalt mixtures (Shacat, Willis, & Ciavola, 2024). The policy salience of EPDs has grown sharply: legislative initiatives and public procurement rules increasingly require verified declarations for materials supplied to state and federal projects, effectively embedding life-cycle thinking into everyday specification and purchasing decisions. The scientific credibility of EPD-based comparison depends, however, on consistent product category rules, representative plant-level data, and clearly defined system boundaries, issues that connect directly to the methodological questions addressed in the next section.

Underlying all of these indicators and instruments is the concept of the circular economy, which reframes waste streams as resources and elevates strategies of reuse, recycling, and material recovery. In pavement engineering, circularity is increasingly measured through mass-based and value-based circularity indicators that quantify the fraction of a pavement's material inputs derived from recovered sources and the fraction recoverable at end of life (Styer et al., 2024). RAP is the paradigmatic circular material, since asphalt is, in principle, fully and repeatedly recyclable; but circularity indicators also capture the reuse of crumb rubber, waste plastics, recycled aggregates, and reclaimed materials in unbound layers. The circular-economy framing is valuable because it discourages narrow optimization of a single impact category and instead directs attention to keeping materials in productive use at their highest value for as long as possible. Nevertheless, circularity indicators are complementary to, rather than substitutes for, full life-cycle assessment, because a high recycled content does not automatically guarantee a lower overall environmental impact once

processing energy, transport, additive use, and durability trade-offs are considered.

Life-Cycle Assessment (LCA) Framework and Methodology

Life-cycle assessment is the principal scientific method for quantifying the environmental impacts of pavement materials and systems across their full life span, and it is standardized internationally by ISO 14040 and ISO 14044. The methodology proceeds through four iterative phases: goal and scope definition; life-cycle inventory (LCI) analysis; life-cycle impact assessment (LCIA); and interpretation. In the goal-and-scope phase, the analyst fixes the intended application, the system boundary, the functional unit, and the analysis period. The inventory phase compiles all material and energy flows crossing the system boundary, together with associated emissions to air, water, and soil. The impact-assessment phase translates these flows into a smaller set of impact-category indicators, such as global warming potential, acidification, eutrophication, and human toxicity, using characterization factors. The interpretation phase evaluates the significance of results, tests their robustness through sensitivity and uncertainty analysis, and formulates conclusions and recommendations. For pavements specifically, the Federal Highway Administration published a dedicated Pavement Life Cycle Assessment Framework that operationalizes the ISO structure for road applications and that has since underpinned agency tools such as LCA Pave (Harvey, Meijer, Ozer, Al-Qadi, Saboori, & Kendall, 2016). Figure 7.2 sets out the four phases of the life-cycle assessment framework together with the life-cycle stages of a pavement, and Figure 7.3 summarises the principal environmental impact categories through which the inventory is interpreted.

The definition of the functional unit is the single most consequential methodological decision in a pavement LCA, because

it establishes the reference to which all inputs and outputs are normalized and thereby determines whether comparisons between alternatives are meaningful. A poorly specified functional unit, for example, one tonne of asphalt mixture at the plant gate, captures manufacturing differences but ignores the fact that competing mixtures may differ in durability, layer thickness, and maintenance demand. A robust functional unit must therefore specify the road segment, the traffic loading, the required structural and functional performance, and the analysis period over which that performance must be maintained (Suwanto, Parry, & Airey, 2024). Reviews of the pavement LCA literature repeatedly identify inconsistent functional-unit definitions, together with variation in the life-cycle phases included and in the assumed maintenance schedules, as the principal sources of incomparability across published studies (Suwanto et al., 2024; Alaloul, Altaf, Musarat, Javed, & Mosavi, 2021). Harmonizing these choices is a prerequisite for the aggregation of individual studies into defensible general conclusions.

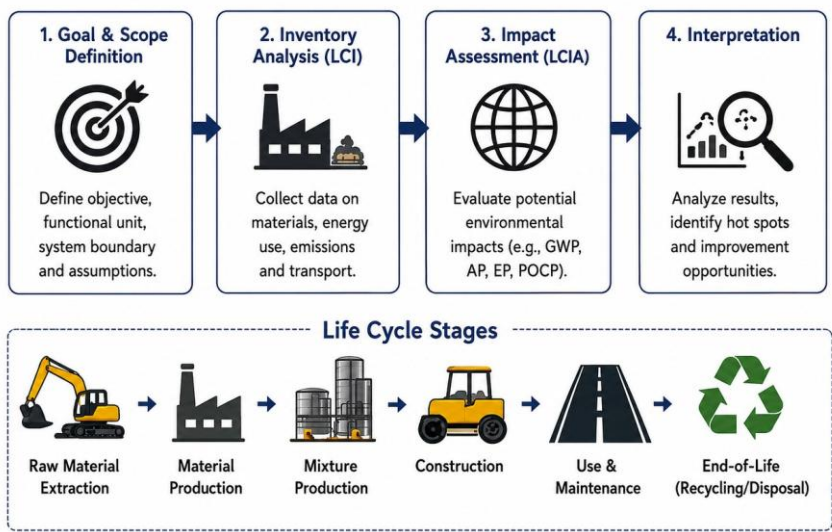


Figure 7.2. *The four-phase life-cycle assessment framework (goal and scope, inventory, impact assessment and interpretation) mapped onto the life-cycle stages of a pavement.*

The pavement life cycle is conventionally divided into distinct phases: materials production, construction, use, maintenance and rehabilitation, and end of life. Each carries its own inventory and its own characteristic uncertainties. The materials-production phase is dominated, for hot-mix asphalt, by the energy required to dry and heat aggregates and to produce and heat the bituminous binder; the construction phase captures equipment fuel use and on-site emissions; the use phase encompasses impacts occurring while the pavement is in service; the maintenance and rehabilitation phase captures the recurring impacts of overlays, milling, patching, and reconstruction; and the end-of-life phase addresses demolition, recovery, and either recycling or disposal. A distinguishing feature of pavement LCA relative to LCA in many other sectors is the potential dominance of the use phase. Because road surfaces interact with millions of vehicle passes, even small changes in surface roughness or structural stiffness alter fleet-wide fuel consumption through the mechanism known as pavement–vehicle interaction (PVI). Modeling by Xu et al. (2019) demonstrated that the use phase can contribute as much as 78% of a pavement's total life-cycle environmental impact and that PVI is the predominant use-phase element on high-volume roads; crucially, however, these contributions are highly context-sensitive to traffic volume, climate, and vehicle speed. The practical implication is that a comparative LCA restricted to cradle-to-gate boundaries may reach conclusions that are reversed once the use phase is included, and that the appropriate system boundary depends on the traffic context of the specific project.



Global Warming Potential (GWP)

- Contribution to climate change (kg CO₂-eq)



Acidification Potential (AP)

- Causes acid rain and ecosystem damage (kg SO₂-eq)



Eutrophication Potential (EP)

- Nutrient enrichment of water bodies (kg PO₃³⁻-eq)



Photochemical Ozone Creation (POCP)

- Formation of ground-level ozone (kg C₃H₈-eq)



Non-renewable Energy Use (NREU)

- Consumption of fossil energy (MJ-eq)

***Figure 7.3.** Principal environmental impact categories used in pavement life-cycle assessment, global warming, acidification, eutrophication, photochemical ozone creation and non-renewable energy use.*

The scope of an LCA is frequently described by the extent of the life cycle it encompasses. A cradle-to-gate study covers raw-material extraction through the point at which the product leaves the manufacturing facility and is the standard basis for asphalt-mixture EPDs. A cradle-to-laid or cradle-to-site study additionally

incorporates transport and construction. A cradle-to-grave study extends through the use, maintenance, and end-of-life phases, capturing the full service history. A cradle-to-cradle study closes the loop by crediting the recovery of materials for use in subsequent life cycles, an accounting that is particularly relevant to asphalt given its recyclability. The choice among these boundaries is not merely technical: it strongly conditions which materials appear advantageous. Warm-mix and high-RAP technologies, for instance, deliver their most conspicuous benefits in the production phase, so cradle-to-gate boundaries tend to flatter them; conversely, technologies that improve durability or smoothness deliver benefits chiefly in the use and maintenance phases and are best captured by cradle-to-grave boundaries (Suwanto et al., 2024; Rodríguez-Alloza & Garraín, 2026).

End-of-life modeling and the allocation of impacts between successive life cycles constitute a persistent methodological challenge with material consequences for functional pavements built from recycled content. When RAP is milled from an old pavement and incorporated into a new mixture, the analyst must decide how to allocate the environmental burdens of the original binder and aggregate and how to credit the avoided production of virgin materials. Different allocation conventions, cut-off, substitution, or economic allocation, can yield substantially different results for the same physical system, which is why transparent reporting of allocation choices is essential (Bizarro, Steinmann, Nieuwenhuijse, Keijzer, & Hauck, 2021). A related methodological frontier concerns temporal considerations, because emissions and material recovery occurring decades apart are not environmentally equivalent, and because the carbon intensity of background energy systems is expected to decline over the analysis period. Prospective and time-differentiated LCA approaches attempt to reflect these dynamics

rather than assuming a static present-day background (Gruber & Hofko, 2023).

Table 7.2. *Phases of life-cycle assessment (ISO 14040/44)*

Phase	Purpose
Goal and scope definition	Define function, system boundary and functional unit
Inventory analysis (LCI)	Quantify all inputs and outputs
Impact assessment (LCIA)	Translate flows into impact categories
Interpretation	Draw conclusions, test sensitivity, recommend

Finally, the credibility of any pavement LCA rests on explicit treatment of data quality and uncertainty. Inventory data may be primary, drawn from specific plants and projects, or secondary, drawn from generic databases; the representativeness of secondary data for a particular technology, region, and time period materially affects results. Because many of the parameters that drive pavement LCA, maintenance timing, service life, traffic growth, and the emission factors of future energy supply, are inherently uncertain, probabilistic and scenario-based methods are increasingly regarded as best practice rather than optional refinements. Xu et al. (2019) formulated the use phase probabilistically precisely because its dominant contribution is also its most uncertain, and systematic reviews recommend that comparative pavement LCAs report uncertainty explicitly and avoid drawing categorical conclusions from point estimates alone (Suwanto et al., 2024; Flores-Ruiz, Montoya-Alcaraz, García, Gutiérrez, & Calderón-Ramírez, 2025). Uncertainty quantification is not a concession of weakness but a source of decision-relevant insight: it identifies the parameters that genuinely govern the comparison and thereby directs both data-

collection effort and engineering attention to where they matter most.

Environmental and Economic Evaluation (Life-Cycle Cost Analysis)

Environmental preferability is a necessary but not a sufficient condition for the adoption of a functional pavement material; agencies operating under fiscal constraint must also be satisfied that a material is economically justifiable over its service life. Life-cycle cost analysis (LCCA) provides the complementary economic evaluation. Whereas LCA quantifies environmental flows, LCCA quantifies all significant costs incurred over a defined analysis period and discounts them to a common present value, enabling a like-for-like comparison of alternatives with different initial costs and different maintenance trajectories. The principal cost categories are agency costs, initial construction, periodic maintenance, rehabilitation, and reconstruction, net of any residual or salvage value at the end of the analysis period, and user costs, which include vehicle operating costs, delay costs during work zones, and, in more complete formulations, crash costs. The mathematics of discounting means that the timing of expenditures matters greatly: a material with a higher initial cost but a longer maintenance-free life can be economically superior to a cheaper alternative that requires frequent intervention, because deferred costs are discounted more heavily (Hasan, Whyte, & Al Jassmi, 2022; Rafiq et al., 2021). Figure 7.4 illustrates the circular life-cycle model that underlies this reasoning, and Figure 7.5 compares the life-cycle cost distribution of conventional and sustainable pavements across the initial-construction, use, maintenance and end-of-life phases.

A recurring methodological limitation of LCCA as commonly practiced is its narrow focus on agency costs to the exclusion of user costs and its frequent neglect of uncertainty.

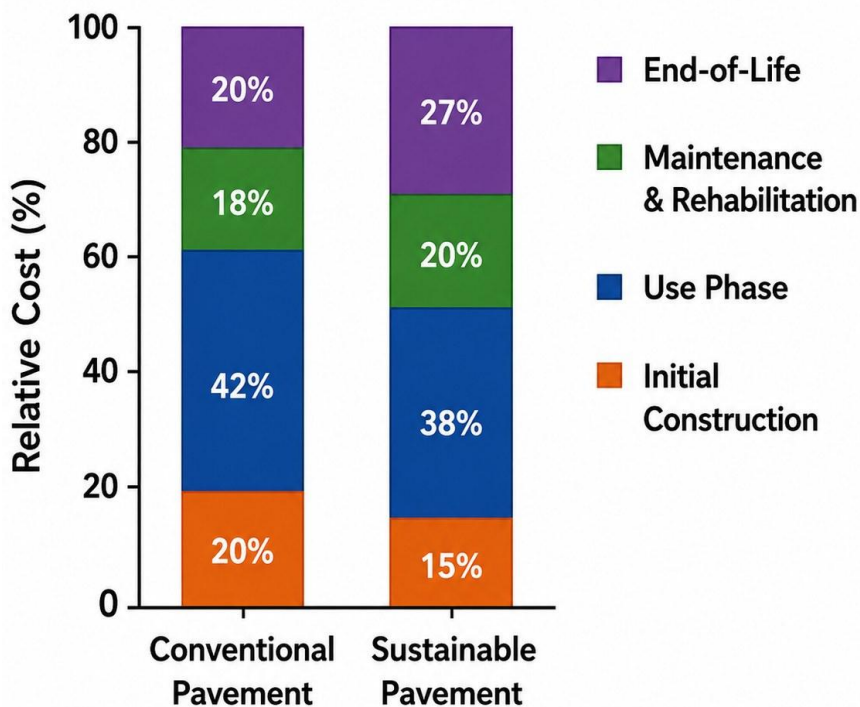
Reviews of the field note that LCCA is often applied only to the comparison of maintenance strategies, is largely restricted to agency expenditures, and typically ignores current or future uncertainty in prices, traffic, and performance (Suwanto et al., 2024). This is a significant shortcoming because user costs, particularly work-zone delay costs on high-volume corridors, can rival or exceed agency costs, and because the economic ranking of alternatives can be sensitive to the discount rate and to the assumed service lives. Consequently, contemporary best practice favors probabilistic LCCA, in which key inputs are represented by distributions rather than point values, and the analysis reports the probability that one alternative is less costly than another rather than a single deterministic ranking. The parallel to probabilistic LCA is deliberate: both environmental and economic evaluations are strengthened by explicit uncertainty treatment, and integrating the two under a consistent set of assumptions about service life and maintenance timing is essential to coherent decision-making (Jasim, Ali, & Al-Saadi, 2024).



Figure 7.4. Circular life-cycle model for sustainable pavement materials, from production with recycled content through use and maintenance to recovery and reuse.

The empirical literature consistently finds that materials incorporating recycled content can deliver simultaneous environmental and economic benefits, though the magnitude depends strongly on context. In a detailed LCCA of an urban highway section, Hasan et al. (2022) reported that the substitution of virgin materials with recycled construction waste and RAP across multiple asphalt courses reduced total life-cycle cost by approximately 14% relative to a conventional design, with the

savings arising chiefly from reduced virgin-material purchase and reduced haulage. A comparable case study comparing hot-mix asphalt with a reclaimed-asphalt alternative likewise identified a total life-cycle cost reduction on the order of 14% attributable to RAP substitution (Rafiq et al., 2021). Combined environmental-and-economic evaluations of recycled mixtures containing RAP together with bio-based or mineral additives have found reductions across all evaluated environmental impact categories alongside lower life-cycle costs, indicating that the environmental and economic objectives need not be in tension for this class of materials (da Costa, Mendes, Melo Neto, Lucena, & Lucena, 2025). These convergent findings help explain why recycling has become the default sustainability strategy in flexible pavement practice.



Sustainable solutions reduce long-term costs through durability and lower maintenance requirements.

Figure 7.5. *Life-cycle cost distribution of conventional and sustainable pavements across the initial-construction, use, maintenance and end-of-life phases.*

Nevertheless, the coupling of environmental and economic benefits is neither automatic nor unconditional, and several trade-offs warrant careful analysis. The variability of RAP properties, which depend on the origin and condition of the reclaimed material, can compromise the consistency and quality of recycled mixtures

and may necessitate additional testing, rejuvenators, or conservative binder-replacement limits, all of which carry cost and, in some cases, environmental penalties (Jasim et al., 2024). High-RAP mixtures may also raise durability questions if the aged binder is inadequately reactivated, and the literature on optimal RAP content reflects this tension, with several studies recommending that RAP be controlled within a range, frequently cited as roughly 30% to 50%, that preserves mechanical performance while still delivering meaningful emission reductions (Bizarro et al., 2021). Because durability directly governs maintenance frequency, and maintenance frequency governs both life-cycle cost and life-cycle environmental impact, any material innovation that trades a lower production footprint for a shorter service life must be evaluated over the full life cycle rather than at the plant gate. This is precisely the circumstance in which integrated LCA–LCCA is indispensable, and in which cradle-to-gate metrics or first-cost comparisons can be actively misleading.

The integration of environmental and economic evaluation is advancing along two complementary lines. The first is the harmonization of assumptions, so that the same functional unit, analysis period, maintenance schedule, and performance model underpin both the LCA and the LCCA of a given alternative; without such harmonization, the two analyses may implicitly describe different physical systems. The second is the development of decision-support frameworks that place environmental and economic indicators before decision-makers in a transparent, jointly interpretable form, whether through eco-efficiency ratios that express environmental benefit per unit cost, through multi-criteria decision analysis that weights indicators according to agency priorities, or through the internalization of environmental externalities via a social cost of carbon (Jasim et al., 2024; Flores-Ruiz et al., 2025). The monetization of carbon is a particularly active area, because it allows greenhouse-gas reductions to be expressed in

the same units as agency and user costs and thereby folds climate impact directly into the economic optimization. Each of these approaches carries its own value judgments, especially in the choice of weights and of the social cost of carbon, and transparency about those judgments is essential if the resulting recommendations are to command the confidence of the diverse stakeholders involved in pavement investment decisions.

Case Studies and Comparative Analysis

The methodological principles set out in the preceding sections acquire concrete meaning through comparative case studies of specific functional materials. Warm-mix asphalt (WMA) provides an instructive first example because its environmental rationale is transparent: by lowering mixing and compaction temperatures relative to hot-mix asphalt (HMA), WMA reduces the fuel required to dry and heat aggregates and thereby cuts production-phase emissions and energy demand. Life-cycle studies quantifying this effect report reductions in greenhouse-gas emissions that vary with the temperature differential and the WMA technology employed; comparisons of HMA produced near 160 °C with WMA produced near 110 °C have shown greenhouse-gas reductions on the order of 27%, while other analyses report reductions closer to 20% (Belc, Ciutina, Buzatu, et al., 2021; Flores-Ruiz et al., 2025). Systematic reviews of carbon-dioxide mitigation strategies conclude that the greatest environmental leverage lies in early-stage interventions, reducing mixing temperature, incorporating recycled inputs, and substituting alternative binders, and that combinations of recycled materials with warm-mix technologies can reduce total emissions by roughly 15% to 45% depending on the specific configuration (Flores-Ruiz et al., 2025). These findings position WMA not as a standalone solution but as an enabling technology that compounds the benefits of recycling, since lower temperatures facilitate the

incorporation of higher RAP contents. Figure 7.6 draws these threads together in a multi-criteria framework for sustainable material selection that balances environmental and technical performance, economic feasibility, social impact and resource efficiency.

Reclaimed asphalt pavement is the most extensively studied functional-material case and illustrates both the promise and the nuance of recycling-based sustainability. Because RAP contains aged but recoverable binder and sound aggregate, its incorporation into new mixtures avoids the upstream impacts of virgin binder production and aggregate extraction, which are among the largest contributors to the asphalt production footprint. Empirical LCA results consistently confirm meaningful reductions: a mixture containing roughly 30% RAP has been reported to use approximately 16% less energy and to emit approximately 20% less carbon than an equivalent virgin hot-mix, and aggressive high-RAP innovations can achieve far larger reductions (Gruber & Hofko, 2023). In a forward-looking LCA of best-available and near-future technologies, Bizarro et al. (2021) estimated a carbon-footprint reduction of between 55% and 64% for one tonne of asphalt containing 93% RAP produced at 105 °C relative to a 0% RAP mixture, though achieving such contents requires technology advances in binder reactivation and mixture design. These results must be interpreted against the durability and variability caveats discussed in Section 7.3: the environmental benefit of high-RAP mixtures is realized only if performance and service life are preserved, and end-of-life allocation conventions materially affect the credited magnitude of the benefit (Gruber & Hofko, 2023). The case of RAP therefore exemplifies the general principle that recycled content is a powerful but conditional sustainability lever whose net benefit is established only through full life-cycle analysis.

Rubberized asphalt incorporating crumb rubber from end-of-life tires offers a second recycling case with a distinctive dual-benefit

structure, since it simultaneously diverts a problematic waste stream from landfill and enhances pavement performance. Life-cycle analyses of the tire-recycling pathway itself have reported that converting waste tires into crumb rubber can reduce carbon-dioxide emissions by roughly 72% relative to landfilling or incineration, establishing a strong upstream case for the material (Wang, Wang, Tseng, Huang, & Li, 2020). At the pavement scale, cradle-to-grave analyses that combine recycled tire rubber with warm-mix additives have reported reductions in life-cycle environmental impacts of approximately 45% to 60% across impact categories relative to conventional pavement, with the magnitude depending on the impact category and the assumed service-life scenario (Rodríguez-Alloza & Garraín, 2026). These improvements arise not only from waste diversion and reduced production temperature but also from the performance benefits of rubber modification, which include improved cracking and fatigue resistance, reduced traffic noise, and extended service life, performance gains that reduce maintenance frequency and thereby lower both life-cycle cost and life-cycle impact. The rubberized-asphalt case is instructive because it shows how the durability and functional-surface indicators introduced in Section 7.1 feed back into the life-cycle result: a longer-lived, lower-noise surface delivers environmental value that a cradle-to-gate analysis would entirely miss (Wang et al., 2020; Rodríguez-Alloza & Garraín, 2026).



Figure 7.6. Multi-criteria framework for sustainable material selection, balancing environmental and technical performance, economic feasibility, social impact and resource efficiency.

Waste-plastic-modified asphalt represents a rapidly growing but more contested case, in which the sustainability calculus is less settled than for RAP or crumb rubber. On the benefit side, incorporating waste plastics such as polyethylene and polyethylene terephthalate into bituminous mixtures diverts persistent waste from

landfill and can improve rutting resistance, fatigue life, and moisture durability, thereby contributing to circular-economy objectives (Styer et al., 2024). A comparative LCA of a novel pavement system incorporating recycled PET from bottles together with carbonated aggregate, produced at reduced temperature, reported reductions of approximately 40% to 60% in climate-change impact and smaller but appreciable reductions in eutrophication categories relative to conventional mixtures (Rispoli & Ajibade, 2024). Eco-economic analyses combining LCA and LCCA for pavements modified with recycled devulcanized rubber and low-density polyethylene have similarly reported substantial greenhouse-gas reductions relative to both unmodified and polymer-modified reference mixtures (Ibrahim et al., 2024). On the caution side, the environmental risk profile of waste-plastic modification is not fully characterized, and concerns regarding the release of volatile organic compounds during production, potential microplastic generation over the service life, and end-of-life recyclability temper the enthusiasm evident in first-cost or production-phase comparisons. The waste-plastic case therefore reinforces the methodological argument of Section 7.2 that the choice of impact categories and system boundary is decisive: an assessment restricted to global warming potential and cradle-to-gate boundaries may present a materially incomplete picture of a technology whose principal uncertainties lie in toxicity and end-of-life fate.

Beyond bituminous systems, alternative binders such as alkali-activated and geopolymer materials extend the sustainability discussion to the chemistry of the binder itself, most directly in rigid and semi-rigid applications and in stabilized layers relevant to flexible pavement structures. The environmental appeal of alkali-activated binders derives from their avoidance of the high-temperature decarbonation of limestone that makes ordinary Portland cement production so carbon-intensive; life-cycle studies

report carbon-emission reductions on the order of 40% or more when such binders substitute for Portland cement (Alhassan, Alkhawaldeh, Betoush, Alkhawaldeh, Huseien, Amaireh, & Elrefae, 2023). Yet the same studies caution that the benefit is contingent and geographically variable, because the alkaline activators, principally sodium silicate and sodium hydroxide, carry their own significant production impacts, such that even modest increases in activator dosage can erode or reverse the net advantage, and because the industrial by-products that serve as precursors are finite and increasingly contested among competing valorization pathways (Alhassan et al., 2023). This case illustrates a general and important lesson for functional-material sustainability: a headline reduction in one impact category, achieved by displacing a conventional high-impact input, may be partially offset by the impacts of the substituting inputs, and only a complete inventory across all relevant flows can establish the true net effect.

Taken together, these case studies support several cross-cutting conclusions that recur throughout the sustainability literature on functional pavement materials. First, the largest and most reliable environmental gains derive from early-life-cycle interventions, recycling to displace virgin binder and aggregate, and temperature reduction to cut production energy, and these interventions are most powerful in combination, as when warm-mix technology enables higher RAP or rubber contents (Flores-Ruiz et al., 2025; Rodríguez-Alloza & Garraín, 2026). Second, durability and functional performance are not separate from sustainability but are among its principal determinants, because service life and maintenance frequency govern how embodied impacts and costs are amortized, and because surface characteristics govern use-phase impacts that can dominate the life cycle on high-volume roads (Xu et al., 2019). Third, the direction and magnitude of a comparative result depend heavily on methodological choices, functional unit, system

boundary, allocation convention, impact categories, and treatment of uncertainty, so that transparent and harmonized methodology is a precondition for credible comparison (Suwanto et al., 2024; Alaloul et al., 2021). Fourth, environmental and economic benefits frequently, though not invariably, coincide for recycled and warm-mix materials, which explains their rapid uptake, but the coincidence must be demonstrated for each context rather than assumed (Hasan et al., 2022; da Costa et al., 2025). The overarching message of this chapter is that the sustainability of a functional pavement material is a property not of the material in isolation but of the material embedded within a specific pavement structure, traffic context, and maintenance regime, and that only an integrated life-cycle assessment and life-cycle cost analysis, conducted with harmonized assumptions and explicit uncertainty, can render a defensible judgment. As functional materials proliferate and as procurement increasingly mandates environmental declarations, the discipline's capacity to conduct such integrated, transparent evaluations will determine whether the promise of sustainable flexible pavements is realized in practice or merely asserted in principle.

AUTHOR'S PERSPECTIVE

In sustainability work the result is decided before the calculation begins, by the choice of system boundary and impact categories. A cradle-to-gate, global-warming-only comparison will flatter almost any recycled-content mixture, yet it can hide toxicity, durability and end-of-life burdens that dominate the full picture. I would not accept a green claim that omits the use phase and a durability-adjusted functional unit, because a material that is greener to make but shorter-lived can be worse over the life of the road.

CHAPTER SUMMARY

Chapter 7 framed sustainability through measurable indicators, the ISO life-cycle-assessment methodology, environmental and economic (life-cycle-cost) evaluation, and comparative case studies of recycled and functional materials.

Key findings

- ▶ Sustainability must be expressed through quantifiable environmental, economic, resource, functional and social indicators.
- ▶ LCA conclusions hinge on the system boundary, functional unit and impact categories chosen.
- ▶ High recycled content does not guarantee a lower life-cycle impact once processing, durability and end-of-life are counted.

Design recommendations

- ▶ Define a durability-adjusted functional unit and include the use phase.
- ▶ Report multiple impact categories, not global warming potential alone.
- ▶ Combine LCA with life-cycle cost analysis to avoid single-metric optimisation.

Future research

- ▶ Harmonised, transparent LCA datasets and boundaries for pavements.
- ▶ Integrated social and toxicity indicators for emerging waste and nano materials.

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CHAPTER 8

Challenges, Emerging Trends and Future Perspectives

The preceding chapters have established that advanced functional materials, nanomodifiers, bio-derived binders, recycled constituents, encapsulated healing agents, conductive fillers and photocatalytic coatings, can measurably improve the mechanical performance, durability and environmental profile of flexible pavements. Yet the trajectory from a promising laboratory formulation to a durable, cost-competitive, standardized and widely deployed pavement technology is neither short nor linear. Many of the materials discussed in this book remain at low-to-intermediate technology-readiness levels, constrained by manufacturing economics, quality-control difficulties, an incomplete regulatory framework and a persistent gap between accelerated laboratory testing and long-term field behaviour. This concluding chapter synthesizes those constraints and looks forward. Section 8.1 examines the technical and economic barriers, scalability, cost and dispersion, that most directly govern whether a functional material can move beyond the bench. Section 8.2 addresses the institutional

dimension: standardization, specification writing and the practicalities of field implementation. Section 8.3 surveys the most compelling emerging directions, from smart and self-healing systems to genuinely multifunctional pavements. Section 8.4 offers concluding remarks and a research outlook intended to orient the next decade of work.

Technical and Economic Challenges (scalability, cost, dispersion)

Figure 8.1 traces the historical evolution of flexible-pavement technology, from conventional asphalt through polymer-, fibre- and nano-modified systems to smart, self-healing and net-zero pavements, while Figure 8.2 maps the principal technical and economic challenges against the corresponding future opportunities.

The most immediate obstacle confronting advanced functional pavement materials is that laboratory success rarely translates directly into industrial practice, because the conditions that make a nanomaterial or bio-additive perform well at the milligram-to-gram scale are difficult and expensive to reproduce at the tonnage scale of a working asphalt plant. Among nanomodified binders this problem is most acute. Comprehensive reviews of nanomaterials in asphalt mixes consistently identify three intertwined difficulties: ensuring uniform dispersion, avoiding particle agglomeration, and controlling the cost of both the nanomaterial and the specialized processing it demands (Debbarma et al., 2022). Because nanoparticles possess extremely high specific surface areas and surface energies, they tend to re-aggregate through van der Waals attraction once introduced into the viscous, chemically heterogeneous bitumen matrix. Where dispersion is incomplete, the very property enhancements that motivate nanomodification, stiffening, improved rutting resistance, enhanced ageing resistance, become spatially non-uniform and unreliable, and in the worst case

agglomerates act as stress concentrators that initiate rather than resist cracking (Afshin & Behnood, 2025). The dispersion problem is therefore not a peripheral processing nuisance but a first-order determinant of whether the claimed benefits are realized at all.

Table 8.1. *Key challenges and mitigation strategies*

Challenge	Description	Mitigation strategy
Cost	High price of nano-, advanced modifiers	Low optimum dosage, waste synergies
Dispersion	Agglomeration at production scale	Surface functionalisation, plant mixing
Scalability	Lab-to-field transfer	Pilot sections, plant trials
Standardization	Lack of specifications, protocols	Performance-based specifications
Durability data	Limited long-term field evidence	Accelerated testing plus LTPP monitoring
Environment, health	Nanoparticle, microplastic release	Life-cycle, ecotoxicity assessment

Achieving adequate dispersion typically requires high-shear mechanical mixing, ultrasonic treatment, or chemical surface functionalization of the particles, and each of these adds cost, energy and complexity. Reviews of the viscosity characteristics of nanomodified asphalt document that mixing temperature, shear rate, shear duration and nanomaterial loading must all be jointly optimized, and that the optimum differs from one nanomaterial to another, so that no single processing recipe can be transferred across the family of candidate modifiers (Huang et al., 2024). This sensitivity is problematic for scale-up because industrial asphalt plants are engineered for throughput and thermal efficiency, not for the fine control of shear history that a nanocomposite demands. Surface functionalization can improve compatibility and reduce re-agglomeration, but it introduces additional chemical processing steps whose cost and environmental burden must themselves be

justified. The net consequence is that many nanomodifiers that perform impressively in the laboratory have not been demonstrated at plant scale, and the literature repeatedly flags the absence of full-scale trials, life-cycle cost analyses and standardized mixing protocols as the decisive gaps separating research from practice (Debbarma et al., 2022; Afshin & Behnood, 2025).

Cost is inseparable from these technical questions and frequently constitutes the binding constraint. Engineered nanomaterials such as carbon nanotubes, graphene derivatives and nano-silica remain expensive relative to conventional polymer modifiers, and pavements are unusually cost-sensitive because they are commodity infrastructure procured in enormous quantities and let, in most jurisdictions, to the lowest responsive bidder. A material that raises binder cost by even a modest fraction can be rendered uncompetitive unless the added cost is offset by demonstrable and specification-creditable gains in service life or reduced maintenance. State-of-the-practice assessments of the asphalt binder supply note that the industry is simultaneously grappling with the declining quality and rising price of conventional bitumen, a consequence of deeper refining and shifting crude slates, which paradoxically strengthens the long-term economic case for alternative and modified binders even as short-term procurement rules penalize their higher first cost (Malluru et al., 2025). The economic argument for advanced materials, in other words, is fundamentally a life-cycle argument, and it cannot be won within a first-cost procurement paradigm.

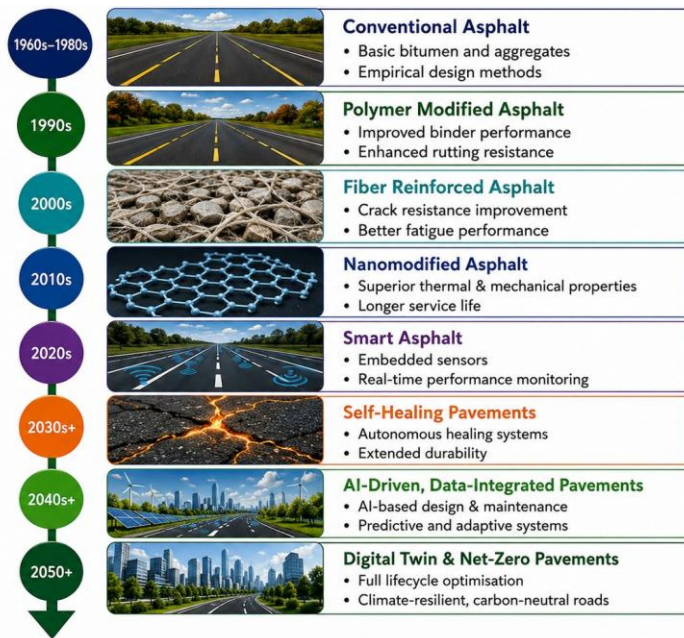


Figure 8.1. *Historical evolution of flexible-pavement technology, from conventional asphalt through polymer-, fibre- and nano-modified systems toward smart, self-healing and net-zero pavements.*

Bio-derived binders and extenders illustrate the same tension from a different angle. Materials such as lignin, bio-oils and bio-chars are attractive because they are renewable, potentially inexpensive as industrial by-products, and capable of partially displacing fossil bitumen. State-of-the-art reviews of bio-based paving binders emphasize that biomass feedstocks, including vegetal and animal wastes and waste cooking oils, can be converted through thermochemical routes into bio-oils and bio-chars with useful rheological effects, but that performance is highly feedstock-dependent and often asymmetric: bio-char generally increases viscosity, stiffness and rutting resistance, whereas bio-oils tend to soften the binder, improving low-temperature behaviour but

impairing high-temperature stability (Musco et al., 2024). This variability is itself a scalability problem, because a paving industry that depends on predictable, reproducible binder grades cannot easily accommodate a feedstock whose properties fluctuate with agricultural season, geographic origin and processing conditions. Lignin, the most abundant natural aromatic polymer and a by-product of the pulp and biofuel industries, has attracted particular attention as a partial bitumen replacement and antioxidant, yet reviews of its use caution that dosage, lignin type and ageing interactions strongly govern outcomes, and that the balance between improved stiffness and ageing resistance on the one hand and possible losses in cracking tolerance on the other must be managed carefully (Gaudenzi et al., 2023). Supply consistency, compatibility with existing binders, and the absence of agreed acceptance criteria therefore constrain bio-materials just as dispersion and cost constrain nanomaterials.

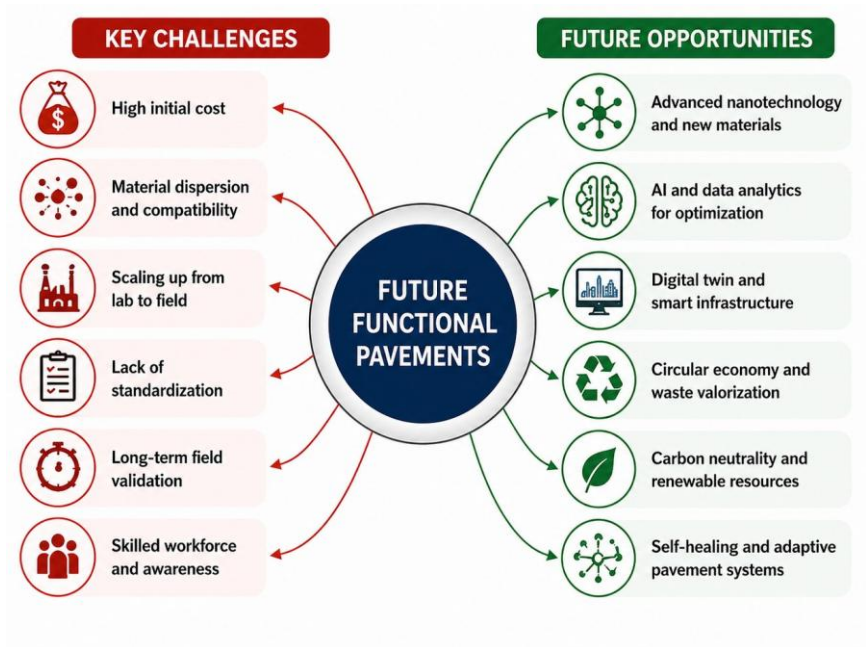


Figure 8.2. *Key technical and economic challenges facing functional pavement materials, set against the corresponding future opportunities.*

Recycled materials occupy a comparable position. Reclaimed asphalt pavement (RAP) is the most widely reused construction material by mass, and increasing RAP content is among the most direct routes to reducing the cost and environmental footprint of asphalt production. Analyses of very high and 100 percent RAP mixtures demonstrate that the technologies to produce them already exist, but that the aged, oxidized and stiff binder contained in RAP introduces variability and brittleness that must be counteracted with rejuvenators and careful mix design (Zaumanis et al., 2014). The central technical challenge is heterogeneity: RAP stockpiles differ in gradation, binder content and degree of ageing, and this variability propagates into the recycled mixture unless it is characterized and controlled (Tarsi et al., 2020). Crumb-rubber modification, another established recycling pathway that diverts waste tyres from landfill, similarly depends on process choices, wet, dry or terminal-blend, that materially affect both performance and environmental burden, so that the sustainability claim attached to a recycled material is contingent on the specific processing route rather than intrinsic to the material itself. In every case the recurring theme is that the raw material's variability, not its average performance, is what limits confident large-scale deployment.

A further, often underappreciated, technical-economic challenge concerns the compatibility of functional additives with the thermal and mechanical realities of pavement production and service. Warm-mix asphalt (WMA) technologies, which lower production and compaction temperatures by roughly 20 to 40 degrees Celsius relative to hot-mix asphalt, are frequently invoked as the natural carrier for temperature-sensitive functional additives such as bio-binders, rejuvenators and encapsulated healing agents,

because they reduce the risk of thermal degradation and can cut energy consumption and emissions substantially (Rubio et al., 2012; Milad et al., 2022). Yet lowering production temperature can compromise aggregate drying, binder-aggregate adhesion and long-term moisture resistance if not managed, illustrating how the introduction of one functional benefit can create a second-order technical liability that must itself be engineered around. Self-healing systems face the analogous constraint that the very mechanisms enabling healing, diffusion and flow of binder across microcracks, thermally or inductively activated, depend on the binder remaining mobile enough to heal yet stiff enough to resist deformation, a balance that becomes harder to strike as binders are stiffened by ageing, recycling or nanomodification (García, 2012). Taken together, these considerations show that the technical and economic barriers are not independent line items but a coupled system: dispersion drives cost, cost drives the demand for life-cycle justification, variability undermines the reproducibility on which specifications depend, and each functional enhancement interacts with the production process and with the other constituents of the mixture. Overcoming them requires not merely better materials but better process control, robust supply chains, and an economic accounting framework capable of valuing durability and sustainability rather than first cost alone.

Standardization, Specifications and Field Implementation

Figure 8.3 depicts an integrated smart-pavement ecosystem in which embedded sensing, connected vehicles, aerial inspection and a cloud data platform support real-time monitoring.

If Section 8.1 concerned whether advanced materials can be made reliably and affordably, this section concerns whether the institutions that build and regulate roads can adopt them with confidence. The transition from a validated material to a routinely

specified one is mediated by standards, test methods and specifications, and it is here that many otherwise promising technologies stall. The fundamental difficulty is that conventional pavement specifications were written for conventional materials. They rely heavily on volumetric mix-design criteria and on empirical or index-based binder tests that were calibrated against decades of experience with unmodified or lightly modified bitumen. Advanced functional materials, by design, alter the microstructure, chemistry and time-dependent behaviour of the binder and mixture in ways that these legacy tests may not capture, so that a material can pass or fail a specification test for reasons that bear little relation to its actual field performance. The result is a regulatory mismatch that penalizes innovation twice: novel materials may be excluded because they fail an irrelevant criterion, and inferior materials may be accepted because the criterion is insensitive to the property that matters.

Recycled materials furnish the clearest example of how specification structure governs deployment. Despite abundant evidence that mixtures containing high proportions of reclaimed asphalt can perform comparably to virgin mixtures when properly engineered, many highway agencies continue to cap allowable RAP content at conservative levels, often 15 to 30 percent, precisely because the traditional volumetric design framework does not reliably account for the effect of the aged RAP binder on mixture performance (Tarsi et al., 2020; Zaumanis et al., 2014). The conservatism is rational given the tools available, but it forgoes substantial economic and environmental benefit. Progress on this front is coming from two directions. The first is the development of simple, rapid indicative tests that allow the variability of a RAP source to be characterized and classified, so that allowable content limits can be set on the basis of the material's measured characteristics rather than a blanket administrative ceiling; frameworks based on fragmentation and cohesion indices, for

example, have been proposed to establish source-specific allowable RAP limits and thereby put high-RAP mixtures on a defensible technical footing (Guduru & Kuna, 2023). The second is the broader migration from purely volumetric acceptance toward performance-related and performance-engineered specifications, in which mixtures are evaluated by direct tests of rutting, cracking and moisture resistance rather than solely by their component proportions. This shift is essential for advanced materials generally, because it creates a mechanism by which the durability benefits that justify their added cost can actually be measured and credited within the procurement process.

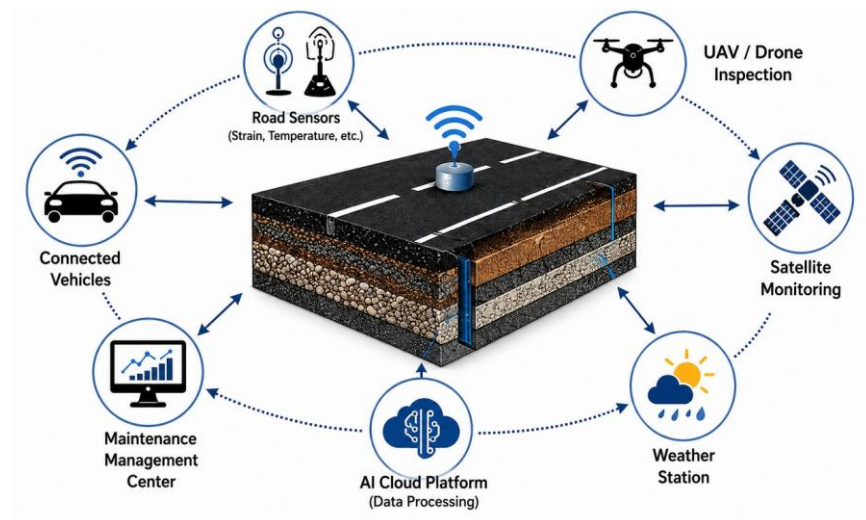


Figure 8.3. *Integrated smart-pavement ecosystem in which embedded sensing, connected vehicles, aerial inspection and a cloud data platform enable real-time monitoring.*

The standardization challenge is compounded for functional pavements whose value lies in properties that fall entirely outside conventional structural specifications. Photocatalytic pavements designed to degrade vehicular pollutants are a case in point. Their intended benefit, reduction of nitrogen oxides and other exhaust

species through titanium-dioxide-catalysed reactions at the pavement surface, is quantified not by any structural test but by air-purification protocols, and even here the measured efficiency depends strongly on humidity, light intensity, traffic-borne soiling and the method of applying the catalyst (Li et al., 2023). Reviews of photocatalytic asphalt note that surface-coated systems achieve far greater pollutant-degradation efficiency than systems in which the catalyst is dispersed through the binder, but that surface coatings suffer from limited service life under traffic abrasion, so that a laboratory efficiency figure measured on a pristine specimen may badly overstate field performance over time (Li et al., 2023). Without standardized, field-representative durability protocols, accounting for abrasion, contamination and weathering, such functional claims cannot be reliably specified or procured, and agencies are understandably reluctant to pay for a benefit they cannot verify or enforce. The same observation applies to self-healing, energy-harvesting and self-sensing functionalities: each introduces a performance dimension for which no mature, agreed test method or acceptance criterion yet exists.

Field implementation raises a further set of issues that laboratory work systematically underrepresents. Chief among these is the gulf between accelerated laboratory conditioning and the multi-decade, multi-factor reality of in-service pavement, in which oxidative ageing, thermal cycling, moisture, traffic loading and de-icing chemicals act simultaneously and interactively. A binder modification that resists ageing in a pressure-ageing-vessel protocol may behave differently under the coupled action of ultraviolet exposure, moisture and mechanical fatigue in the field, and the sustainability benefits attributed to a material at the laboratory scale may be eroded or reversed once realistic construction and maintenance activities are included. Life-cycle assessments of recycled-content pavements demonstrate this sensitivity vividly: the

calculated greenhouse-gas savings from incorporating reclaimed asphalt or recycled rubber depend heavily on the system boundary chosen, the allocation method adopted, and whether the use and maintenance phases are included, with the consequence that studies of nominally similar technologies report widely divergent environmental outcomes (Gruber & Hofko, 2023). This lack of methodological harmonization is itself a standardization problem, because it prevents agencies from making consistent, comparable environmental judgments about competing materials. Until life-cycle assessment methods, functional units and system boundaries are standardized for pavement applications, environmental claims will remain difficult to audit and therefore difficult to reward through green procurement.

Construction practice adds its own constraints. Asphalt paving is a mature, high-throughput industry with established equipment, workforce competencies and quality-control routines, and any new material must integrate into that reality without imposing impractical demands. Additives that require unusual mixing energy, narrow temperature windows, extended storage stability or specialized handling face adoption resistance quite apart from their technical merit. Warm-mix technologies have diffused comparatively rapidly precisely because they align with, rather than disrupt, existing plant operations while offering tangible energy, emissions and workability benefits, and because a body of comparative environmental and economic evidence has accumulated to support them (Milad et al., 2022; Rubio et al., 2012). By contrast, technologies that demand new plant capital, new field procedures or new inspection methods encounter a higher adoption threshold, and the absence of trained personnel and validated construction guidance can undermine even a technically sound material. Reviews of the binder supply chain further emphasize that meaningful transition toward sustainable alternatives will require not only new

specifications but coordinated action across producers, contractors, agencies and standards bodies, a systemic realignment rather than an isolated technical fix (Malluru et al., 2025). Bio-based binders again illustrate the point: their deployment is limited less by any single performance deficiency than by the absence of standardized production, characterization and acceptance frameworks capable of accommodating feedstock variability (Musco et al., 2024). The overarching lesson of this section is that standardization and field implementation are not downstream formalities to be addressed once the material science is settled; they are integral engineering problems that must be pursued in parallel with material development if advanced functional pavements are to move from demonstration to practice.

Emerging Directions (smart/self-healing materials, multifunctional pavements)

Figure 8.4 sets out a digital-twin workflow for pavement systems, from data acquisition through modelling, prediction and optimisation to decision and action.

Against the backdrop of these challenges, the most intellectually vibrant frontier in pavement engineering is the reconceptualization of the road surface from a passive load-bearing layer into an active, responsive and multifunctional system. Three convergent directions define this frontier: materials that repair themselves, materials that sense their own condition, and pavements that harvest energy or deliver environmental services in addition to carrying traffic. What unites them is the ambition to embed functionality directly into the pavement material, so that maintenance, monitoring and even energy generation become intrinsic properties of the infrastructure rather than external interventions.

Self-healing asphalt is the most mature of these directions and the one with the clearest economic rationale, because the dominant cost of a pavement over its life is not construction but repeated repair of fatigue and thermal cracking. The physical basis for self-healing is that bitumen is a viscoelastic material capable, under favourable conditions of temperature and rest, of flowing across and re-bonding microcracks before they coalesce into macroscopic damage; foundational work demonstrated that open cracks in asphalt mastic can partially close and recover strength through this intrinsic capillary and diffusion-driven flow when the binder is sufficiently mobile (García, 2012). Methodological reviews now organize the field around the mechanisms used to accelerate or trigger this latent capacity, distinguishing intrinsic healing from extrinsic strategies that add external agents or energy (Anupam et al., 2022). Extrinsic approaches fall broadly into two families. The first uses externally supplied energy, electromagnetic induction heating or microwave irradiation, to raise the binder temperature locally and thereby mobilize healing on demand, which requires that the normally insulating asphalt be made electrically or magnetically responsive through the addition of conductive fibres or magnetic particles (Wan et al., 2023). The second embeds encapsulated rejuvenators within the mixture: microcapsules or hollow fibres rupture as cracks propagate, releasing oils that soften and restore the aged binder at the crack tip (Sun et al., 2017). Studies of encapsulated systems report substantial recovery of mechanical properties, with healing efficiencies spanning a wide range depending on capsule survival during mixing, release timing and the spatial distribution of capsules within the matrix (Sun et al., 2017; Wan et al., 2023). Hybrid concepts that combine induction heating with rejuvenator capsules are attractive because the two mechanisms are complementary, heating restores flow while the released oil chemically reverses ageing, but they also compound the

manufacturing and dispersion challenges discussed earlier, and the durability of the healing function over many damage-repair cycles remains insufficiently characterized under realistic field conditions (Anupam et al., 2022).

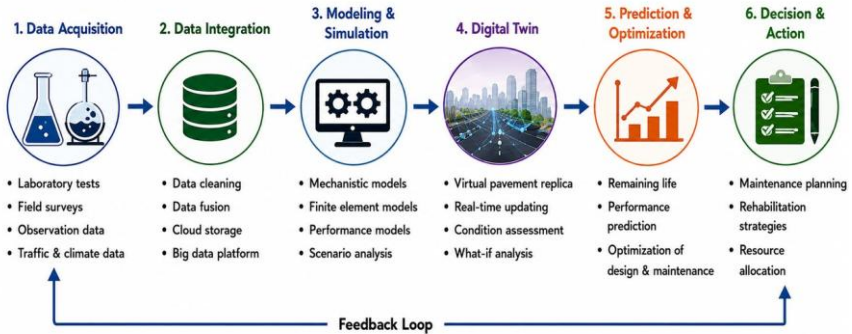


Figure 8.4. *Digital-twin workflow for pavement systems, from data acquisition through modelling, prediction and optimisation to decision and action.*

The second emerging direction turns the pavement into a distributed sensor. Self-sensing asphalt exploits the fact that incorporating conductive carbon-based fillers, carbon nanotubes, graphene nanoplatelets, carbon fibres or carbon black, renders the normally insulating mixture electrically conductive, and that its electrical resistance then changes measurably in response to strain, damage and temperature (Gulisano et al., 2024). This piezoresistive behaviour allows the pavement itself to report on traffic loading, structural strain and the initiation of internal damage, opening the prospect of continuous structural health monitoring without the discrete, fragile embedded gauges that current practice relies upon. Reviews of the field emphasize that fibrous conductive additives are generally more effective than particulate ones at forming the percolating conductive network required for sensing, because their

high aspect ratio creates longer continuous conductive paths at lower filler loadings, thereby limiting the mechanical and economic penalty of the additive (Gulisano et al., 2024). The same conductive-network principle underlies the coupling between self-sensing and self-healing: the conductive additives that enable strain sensing are frequently the very additives that enable induction heating, so a single functionalized material can in principle both diagnose and treat its own damage. The practical obstacles are the durability and stability of the electrical response under moisture, temperature cycling and repeated loading, the calibration of resistance change against meaningful engineering quantities, and the integration of the sensing signal into pavement-management data systems.

The third and most ambitious direction is the genuinely multifunctional pavement that delivers services beyond structural support. Energy harvesting is the flagship of this category. Because road networks are vast, continuously loaded and exposed to solar radiation and thermal gradients, they represent an enormous untapped energy resource, and technologies to convert traffic-induced mechanical deformation, thermal gradients or incident solar energy into usable electricity have advanced considerably. Piezoelectric harvesting, in which transducers embedded in or beneath the pavement convert the strain energy of passing vehicles into electrical power, has been reviewed in detail from the perspectives of transducer structure, packaging, energy-management circuitry and field durability (Mou et al., 2025). The consensus emerging from this work is sober but constructive: the poor durability of piezoelectric elements under repeated heavy loading, the stiffness mismatch between the transducers and the surrounding asphalt, and the modest power densities achievable mean that the near-term value of these systems lies less in bulk grid-scale generation than in powering localized, low-consumption functions such as embedded sensors, wireless communication nodes, roadside

lighting and signage (Mou et al., 2025). Viewed this way, energy harvesting and self-sensing become synergistic: a pavement that generates small amounts of local power can supply the very sensors that monitor its condition, moving toward a self-powered, self-reporting road. Photocatalytic surfaces that degrade vehicle exhaust, discussed earlier as a standardization challenge, belong to the same multifunctional family, as do pavements engineered for solar reflectance to mitigate the urban heat-island effect and permeable systems designed for stormwater management. The defining research question for all of them is how to combine multiple functions within a single durable material without the functions degrading one another or the structural performance of the pavement.

Cutting across all three directions is the accelerating role of computational and data-driven methods, which are increasingly indispensable to the design and management of functional pavements. Machine-learning techniques are now applied across the pavement life cycle, optimizing mix design, predicting the performance of complex modified and recycled mixtures, characterizing materials, and detecting surface distress, precisely because the multi-component, multi-scale systems created by advanced functional materials are too complex for the empirical correlations of traditional practice to capture (Dadaei et al., 2025). Data-driven surrogate models can explore vast compositional design spaces far faster than laboratory testing, helping to identify optimal nanomaterial dosages or rejuvenator contents and thereby directly addressing the dispersion-and-dosage optimization problems of Section 8.1 (Huang et al., 2024; Dadaei et al., 2025). When coupled with the real-time condition data generated by self-sensing pavements, such models point toward a future of predictive, digitally managed infrastructure in which material behaviour, structural health and maintenance scheduling are continuously and

intelligently linked. The principal reservation, echoing the theme of standardization, is that machine-learning models are only as trustworthy as the data and physical understanding underpinning them; the field is now emphasizing interpretability, uncertainty quantification and field validation as prerequisites for using these tools in high-consequence infrastructure decisions (Dadaei et al., 2025). The emerging pavement, in short, is one in which advanced materials, embedded functionality and computational intelligence are designed together rather than in isolation.

Concluding Remarks and Research Outlook

Figure 8.5 presents a consolidated roadmap of emerging trends and future perspectives, and Figure 8.6 envisions the net-zero, intelligent pavement infrastructure of 2050 toward which these developments converge.

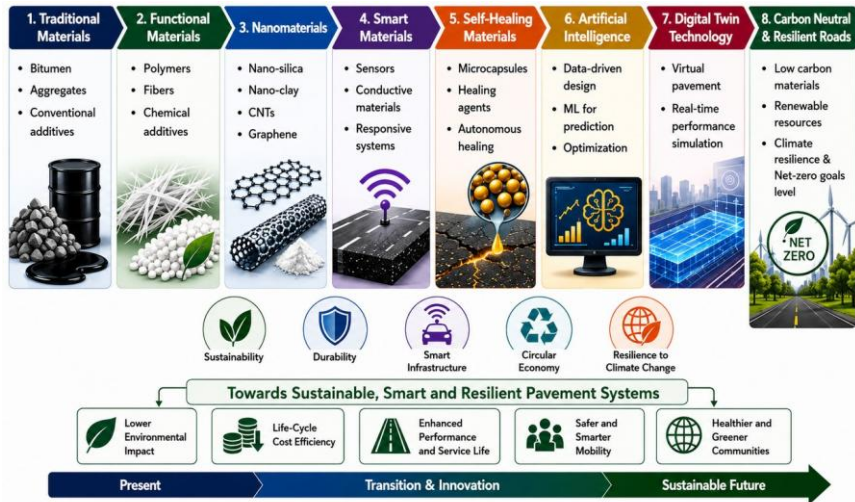


Figure 8.5. Consolidated roadmap of the emerging trends and future perspectives shaping functional pavement materials.

The material presented throughout this book, and synthesized in this chapter, supports a clear overall assessment: advanced functional materials offer a credible and increasingly demonstrated path toward flexible pavements that are more durable, more sustainable and more intelligent than those built with conventional technology, but the realization of that promise depends as much on process engineering, economics, standardization and institutional change as on materials science itself. The technical enhancements are real, nanomodification can improve stiffness, rutting and ageing resistance; bio-derived and recycled constituents can displace fossil bitumen and virgin aggregate; encapsulated and induction-activated systems can restore cracked binder; conductive fillers can turn pavements into sensors; and harvesting and photocatalytic technologies can extract value and environmental service from the road surface. Yet each of these advances is presently gated by a recurring set of obstacles: the difficulty of achieving uniform dispersion and reproducible behaviour at industrial scale, the first-cost penalty that a life-cycle accounting framework is needed to offset, the variability of recycled and bio-based feedstocks, the mismatch between legacy specifications and novel material behaviour, and the absence of standardized, field-representative test methods for the new functional properties.

Several priorities for future research follow directly from this diagnosis. First, the community should elevate scale-up, process control and reproducibility to the status of primary research objectives rather than treating them as engineering afterthoughts; a functional material that cannot be dispersed reliably in a working plant is not yet a pavement technology, however impressive its laboratory data. Second, there is an urgent need for harmonized, transparent life-cycle assessment and life-cycle cost methodologies specific to pavement applications, with agreed functional units, system boundaries and allocation rules, so that the environmental

and economic claims attached to competing materials can be compared, audited and rewarded through procurement (Gruber & Hofko, 2023). Third, the migration from volumetric toward performance-related and performance-engineered specifications must continue and must be extended to encompass the new functional dimensions, healing capacity, sensing stability, pollutant-degradation durability, harvested-energy reliability, for which acceptance criteria do not yet exist (Guduru & Kuna, 2023; Li et al., 2023). Fourth, long-term field validation under real traffic and climate, sustained over years rather than the weeks of accelerated laboratory conditioning, is indispensable, because the coupled action of ageing, moisture, thermal cycling and loading cannot be faithfully reproduced in the laboratory and because durability, not peak performance, is the true measure of a functional material's worth (Malluru et al., 2025).



Figure 8.6. *Vision of the net-zero, intelligent pavement infrastructure of 2050 toward which current developments converge.*

Looking further ahead, the most consequential opportunity lies in convergence. The individual functionalities surveyed here, self-healing, self-sensing, energy harvesting and environmental remediation, are increasingly seen not as competing alternatives but as complementary capabilities that share underlying materials and mechanisms, most notably the conductive and functional filler networks that simultaneously enable heating, sensing and, in some configurations, energy conversion (Gulisano et al., 2024; Wan et al., 2023; Mou et al., 2025). A pavement that senses its own strain, powers that sensing from harvested traffic energy, heals incipient cracks by induction before they propagate, and cleans the air above it is no longer merely a structural element but an item of active, self-maintaining, service-providing infrastructure. Realizing such a vision will require deep interdisciplinary collaboration spanning materials chemistry, structural and pavement engineering, electrical engineering, data science and public policy, together with the computational tools now maturing to manage the resulting complexity (Dadaei et al., 2025). It will also require that the sustainability imperative, reducing the substantial energy, emissions and resource footprint of the world's road networks, remain the organizing purpose of the enterprise, ensuring that added functionality is pursued in service of, and not at the expense of, environmental performance (Rubio et al., 2012; Musco et al., 2024). The challenges catalogued in this chapter are formidable, but they are challenges of implementation, integration and institution-building rather than of fundamental feasibility. The scientific foundations for sustainable, functional, intelligent flexible pavements are now substantially in place; the work of the coming decade is to make them scalable, standardized, durable and, above all, ordinary.

AUTHOR'S PERSPECTIVE

If I had to rank the barriers between these materials and the field, cost and scalability would come first and novelty last. The laboratory has already produced more functional chemistries than the industry can specify or reproduce at plant scale, so the decisive work now is standardisation, pilot sections and honest long-term monitoring. The real prize is multifunctionality that pays for itself, a single system that resists rutting, heals, harvests heat and reuses waste, and reaching it is an engineering and policy problem at least as much as a materials one.

CHAPTER SUMMARY

Chapter 8 synthesised the book, weighing the technical and economic barriers, the standardisation and field-implementation gap, the emerging smart and multifunctional directions, and the research outlook for functional, sustainable pavements.

Key findings

- ▶ Cost, dispersion and scalability, not laboratory novelty, are the binding constraints on adoption.
- ▶ Performance-based specifications and field validation are prerequisites for deployment.
- ▶ Self-healing, energy-harvesting, sensing and multifunctional pavements are the most promising frontiers.

Design recommendations

- ▶ Prioritise low-dosage, waste-synergistic formulations that are plant-reproducible.
- ▶ Validate through instrumented pilot sections and long-term monitoring.
- ▶ Design for several functions at once where the mechanisms reinforce rather than conflict.

Future research

- ▶ Standardisation, accelerated-plus-field durability evidence and life-cycle accountability.
- ▶ Self-sufficient, multifunctional pavements that resist, heal, harvest and reuse.

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